

RUSSIAN MARITIME REGISTER OF SHIPPING

RULES
FOR THE CLASSIFICATION
AND CONSTRUCTION
OF SEA-GOING SHIPS

Part XVII

DISTINGUISHING MARKS
AND DESCRIPTIVE NOTATIONS
IN THE CLASS NOTATION SPECIFYING
STRUCTURAL AND OPERATIONAL
PARTICULARS OF SHIPS



Saint-Petersburg
Edition 2018

Rules for the Classification and Construction of Sea-Going Ships of Russian Maritime Register of Shipping have been approved in accordance with the established approval procedure and come into force on 1 January 2018.

The present edition of the Rules is based on the edition 2017 taking into account the amendments developed immediately before publication.

The unified requirements, interpretations and recommendations of the International Association of Classification Societies (IACS) and the relevant resolutions of the International Maritime Organization (IMO) have been taken into consideration.

The Rules are published in the following parts:

Part I "Classification";

Part II "Hull";

Part III "Equipment, Arrangements and Outfit";

Part IV "Stability";

Part V "Subdivision";

Part VI "Fire Protection";

Part VII "Machinery Installations";

Part VIII "Systems and Piping";

Part IX "Machinery";

Part X "Boilers, Heat Exchangers and Pressure Vessels";

Part XI "Electrical Equipment";

Part XII "Refrigerating Plants";

Part XIII "Materials";

Part XIV "Welding";

Part XV "Automation";

Part XVI "Hull Structure and Strength of Glass-Reinforced Plastic Ships and Boats";

Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships";

Part XVIII "Common Structural Rules for Bulk Carriers and Oil Tankers". The text of the Part is identical to that of the IACS Common Structural Rules;

Part XIX "Additional Requirements for Structures of Container Ships and Ships, Dedicated Primarily to Carry their Load in Containers". The text of the Part is identical to IACS UR S11A "Longitudinal Strength Standard for Container Ships" (June 2015) and S34 "Functional Requirements on Load Cases for Strength Assessment of Container Ships by Finite Element Analysis" (May 2015).

Parts I to XVII are published in electronic format and hard copy in Russian and English. In case of discrepancies between the Russian and English versions, the Russian version shall prevail.

Parts XVIII to XIX are published in English and in electronic format only.

As compared to the 2017 edition, the present edition of the Rules contains the following amendments.

RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS

PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

1. Paras 3.6.4.1, 4.2.1.1, 5.6.2, 5.8.1.1.1, 7.1.1.3.1, 7.2.4 (existing), 10.6.1: the requirements have been specified to avoid ambiguous phrase "subject to special agreement with the Register".
2. Paras 3.2.4, 3.5.2.3, 3.6.2.3, 4.2.1.4, 4.2.3.5, 6.2.9.4, 7.2.3 have been deleted to avoid ambiguous phrase "subject to special agreement with the Register";
paras 4.2.1.5 — 4.2.1.7 have been renumbered as paras 4.2.1.4 — 4.2.1.6 accordingly;
paras 4.2.3.6 — 4.2.3.12 have been renumbered as 4.2.3.5 — 4.2.3.11 accordingly;
para 6.2.9.5 has been renumbered as 6.2.9.4 accordingly;
paras 7.2.4 — 7.2.6 have been renumbered as 7.2.3 — 7.2.5 accordingly.
3. Chapter 1.1 has been completely amended considering UR IACS II (Rev.2 Apr 2016).
4. Chapter 1.2 has been completely amended considering UR IACS 12 (Rev.3 Apr 2016).
5. Chapter 3.1: in para 3.1.1.1 the requirement has been specified;
para 3.1.1.3 has been deleted;
in para 3.1.2 the definition "Ballast water" has been deleted.
6. Chapter 3.2: Table 3.2.2 has been amended.
7. Chapter 3.3: in Table 3.3.2 the reference to IMO resolution MEPC.184(59) has been replaced by the reference to IMO resolution MEPC.259(68).
8. Chapter 3.5: paras 3.5.1.1 and 3.5.2.2.6 have been amended;
para 3.5.2.2.7 has been deleted;
paras 3.5.2.2.8 — 3.5.2.2.11 have been renumbered as 3.5.2.2.7 — 3.5.2.2.10 accordingly;
in para 3.5.2.2.11 (existing) the reference to IMO resolution MEPC.184(59) has been replaced by the reference to IMO resolution MEPC.259(68).
9. Chapter 3.6: paras 3.6.1.1, 3.6.2.1.2, 3.6.2.2.4, 2.6.3.3.8, 3.6.3.10.2 and 3.6.3.10.3 have been amended;
para 3.6.2.2.5 has been deleted;
subsequent paras have been renumbered accordingly;
the Chapter has been supplemented with paras 3.6.3.2.5 and 3.6.3.10.4.
10. Chapter 4.1: para 4.1.3.1.6 has been deleted.
11. Chapter 4.2: in para 4.2.3.3 the requirements have been specified;
new paras 4.2.1.2 and 4.2.5.1.8 have been introduced;
para 4.2.3.7 has been amended.
12. Chapter 4.3: paras 4.3.1 and 4.3.2 have been amended.
13. Chapter 6.5: para 6.5.1.1 has been amended;
Para 6.5.1.15 has been deleted (the requirements have been transferred to para 6.5.1.1);
para 6.5.1.3 has been amended.
14. Chapter 7.1: the definition "Design ambient temperature (DAT)" has been specified;
the definition "Test temperature" has been deleted;
in paras 7.1.3.1.3 and 7.1.3.2.4 the requirements have been specified.
15. Chapter 7.2: para 7.2.2 has been amended.
16. Chapter 7.3: paras 7.3.1, 7.3.2, 7.3.3 and 7.3.4 have been amended.
17. Chapter 7.4: para 7.4.6.1 has been amended.
18. Chapter 7.6: in para 7.6.2 the requirements for fuel storage and supply to ensure that machinery are brought into operation from the dead ship condition have been specified.
19. Chapter 7.7: in para 7.7.1.1 the requirements for materials used for manufacture of fittings, expansion joints and formed components of pipelines to be installed on the open decks, as well as in the open unheated spaces have been specified.
20. Chapter 7.9: in paras 7.9.2.1.9, 7.9.2.1.13, 7.9.3.1.4, 7.9.4.1.5, 7.9.5.1.3 and 7.11.1.4 the requirements have been specified.
21. Chapter 7.12: in para 7.12.6 the requirement has been specified.

22. Chapter 7.13: in para 7.13.1 the requirement has been specified considering the experience of technical supervision;

para 7.13.2 has been deleted.

23. Section 9 has been completely amended considering IMO resolution MSC.391(95).

24. Chapter 10.1: para 10.1.1 has been amended.

25. New Section 11 "Requirements for LNG bunkering ships" has been introduced.

26. New Section 12 "Requirements for ships for compliance with the distinguishing mark **IWS** in the class notation" has been introduced.

27. New Section 13 "Requirements for offshore service vessels" has been introduced.

28. New Section 14 "Requirements for ships prepared for conversion for the use of gas fuel" has been introduced.

29. Editorial amendments have been made.

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PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

1 REQUIREMENTS FOR POLAR CLASS SHIPS

1.1 POLAR CLASS DESCRIPTIONS AND APPLICATION

1.1.1 Application.

1.1.1.1 The requirements for polar class ships apply to ships constructed of steel and intended for independent navigation in ice-infested polar waters.

The requirements of this Section apply to ships contracted for construction on or after 1 July 2017.

Note. The "contracted for construction" date means the date on which the contract to build the ship is signed between the prospective owner and the shipbuilder. For further details regarding the date of "contracted for construction", refer to 1.1.2, Part I "Classification".

1.1.1.2 Ships that comply with the requirements of 1.2 and 1.3 can be considered for a polar class notation specified in Table 1.1.1.2. These requirements are additional to the RS requirements for ships without ice class assigned. If the hull and machinery are constructed such as to comply with the requirements of different polar classes, then both the hull and machinery shall be assigned the lower of these classes in the Certificate of Classification. Compliance of the hull or machinery with the requirements of a higher polar class shall also be indicated in the Certificate of Classification in column "Other characteristics".

1.1.1.3 Ships which are assigned a polar class notation and complying with the relevant requirements of 1.2 and 1.3 may be given an ice class mark **Icebreaker**.

"Icebreaker" refers to any ship having an operational profile that includes escort or ice management functions, having powering and dimensions that allow it to undertake aggressive operations in ice-covered waters.

1.1.1.4 For ships which are assigned a polar class notation, the hull form and propulsion power plant shall be such that the ship can operate independently and at continuous speed in a representative ice condition, as defined in Table 1.1.1.2 for the corresponding polar class.

For ships and ship-shaped floating facilities which are intentionally not designed to operate independently in ice, such operational intent or limitations shall be explicitly stated in the Certificate of Classification.

1.1.1.5 For ships which are assigned a polar class notation **PCI** to **PC5**, bows with vertical sides, and bulbous bows generally shall be avoided. Bow angles shall in general be within the range specified in 1.2.3.1.5.

1.1.1.6 For ships which are assigned a polar class notation **PC6** and **PC7**, and are designed with a bow with vertical sides or bulbous bows, operational limitations (restricted from intentional ramming) in design conditions shall be stated in the Certificate of Classification.

1.1.2 Polar Classes.

1.1.2.1 The polar class (**PC**) notations and descriptions are specified in Table 1.1.1.2. It is the responsibility of the shipowner to select an appropriate polar class. The descriptions in Table 1.1.1.2 are intended to guide shipowners, designers and Administrations in selecting an appropriate polar class to comply with the requirements for the ship in intended voyage or service areas.

1.1.2.2 The polar class notation is used throughout this Section to convey the differences between classes with respect to operational capability and strength.

1.1.3 Upper and Lower Ice Waterlines.

1.1.3.1 The upper and lower ice waterlines upon which the design of the ship has been based shall be indicated in the Certificate of Classification. The upper ice waterline (**UIWL**) shall be defined by the maximum draughts fore, amidships and aft. The lower ice waterline (**LIWL**) shall be defined by the minimum draughts fore, amidships and aft.

1.1.3.2 The lower ice waterline is to be determined with due regard to the ship's ice-going capability in the ballast loading conditions. The propeller shall be fully submerged at the lower ice waterline.

1.2 STRUCTURAL REQUIREMENTS FOR POLAR CLASS SHIPS

1.2.1 Application.

1.2.1.1 The requirements of this Section apply to polar class ships in compliance with 1.1.

Table 1.1.1.2

Polar class descriptions	
Polar class	Ice description (based on WMO Sea Ice Nomenclature)
PCI	Year-round operation in all polar waters
PC2	Year-round operation in moderate multi-year ice conditions
PC3	Year-round operation in second-year ice which may include multi-year ice inclusions
PC4	Year-round operation in thick first-year ice which may include old ice inclusions
PC5	Year-round operation in medium first-year ice which may include old ice inclusions
PC6	Summer/autumn operation in medium first-year ice which may include old ice inclusions
PC7	Summer/autumn operation in thin first-year ice which may include old ice inclusions

1.2.2 Hull areas.

1.2.2.1 The hull of all polar class ships is divided into areas reflecting the magnitude of the loads that are expected to act upon them. In the longitudinal direction, there are four regions: bow (*B*), bow intermediate (*BI*), midbody (*M*) and stern (*S*). Besides, the bow intermediate, midbody and stern regions are further divided in the vertical direction into the bottom (*b*), lower (*l*) and ice belt regions. The extension of ice strengthening region shall be determined in compliance with Fig.1.2.2.1.

1.2.2.2 The UIWL and LIWL are as defined in 1.1.3.

1.2.2.3 Fig. 1.2.2.1 notwithstanding, at no time shall the boundary between the bow and bow intermediate regions be forward of the intersection point of the line of the stem and the ship baseline.

1.2.2.4 Fig. 1.2.2.1 notwithstanding, the aft boundary of the bow region need not be more than $0,45L$ aft of the forward perpendicular (*FP*).

1.2.2.5 The boundary between the bottom and lower regions shall be taken at the point where the shell is inclined 7° from horizontal.

1.2.2.6 If a ship is intended to operate astern in ice regions, the aft section of the ship shall be designed using the bow and bow intermediate hull ice belt requirements.

1.2.2.7 If the ship is assigned the ice class mark **Icebreaker**, the forward boundary of the stern region shall be at least $0,04L$ forward of the section where the parallel ship side at the UIWL ends.

1.2.3 Design ice loads.

1.2.3.1 General.

1.2.3.1.1 A glancing impact on the bow is the design scenario for determining the scantlings required to resist ice loads.

1.2.3.1.2 The design ice load is characterized by an average pressure P_{avg} uniformly distributed over a rectangular load patch of height b and width w .

1.2.3.1.3 Within the bow area of all polar classes, and within the bow intermediate ice belt area of polar classes **PC6** and **PC7**, the ice load parameters are functions of the actual bow shape. To determine the ice load parameters P_{avg} , b and w , it is required to calculate the following ice load characteristics for sub-regions of the bow area; shape coefficient f_a , total glancing impact force F_i , line load Q_i and pressure P_i .

1.2.3.1.4 In other ice-strengthened areas, the ice load parameters P_{avg} , b_{NonBow} and w_{NonBow} are determined independently of the hull shape and based on a fixed load patch aspect ratio, $AR = 3,6$.

1.2.3.1.5 Design ice forces calculated according to 1.2.3.2.1.1 are applicable for bow forms where the buttock angle γ at the stern is positive and γ less than 80° and the normal frame angle β' at the centre of the foremost sub-region, as defined in 1.2.3.2.1, is greater than 10° .

1.2.3.1.6 Design ice forces calculated according to 1.2.3.2.1.2 are applicable for ships which are assigned the polar class **PC6** or **PC7** and have a bow form with vertical sides. The requirements of 1.2.3.2.1.2 shall apply where the

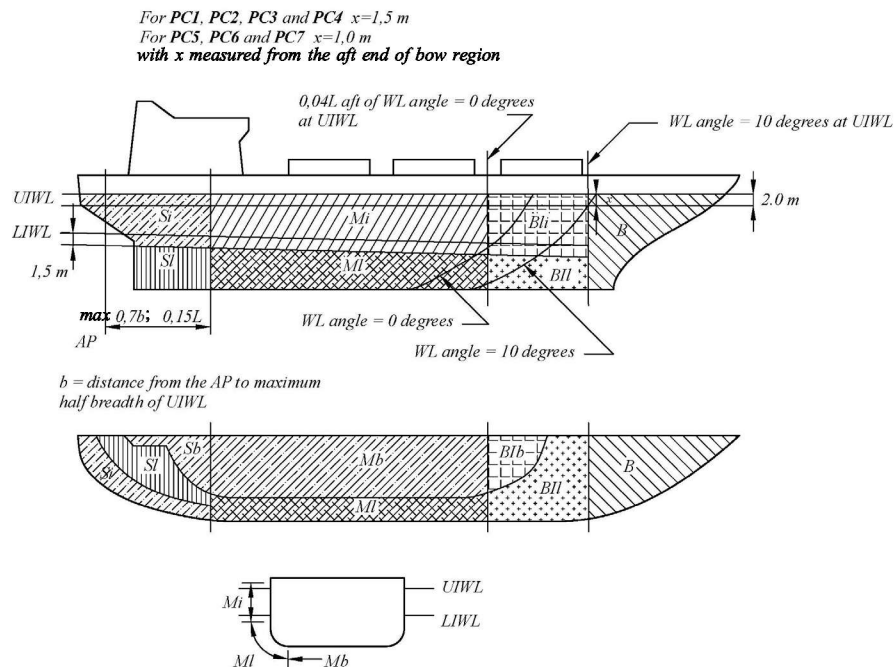


Fig. 1.2.2.1
Hull area extents

normal frame angles β' at the considered sub-regions, as defined in 1.2.3.2.1, are between 0 and 10 deg.

1.2.3.1.7 For ships which are assigned the polar class **PC6** or **PC7**, and equipped with bulbous bows, the design ice forces on the bow shall be determined according to 1.2.3.2.1.2. In addition, the design forces shall not be taken less than those specified in 1.2.3.2.1.1, assuming $f_a = 0,6$ and $AR = 1,3$.

1.2.3.1.8 For ships with bow forms other than those defined in 1.2.3.1.5 to 1.2.3.1.7, design forces shall be determined according to the procedures approved by the Register.

1.2.3.1.9 Ship structures that are not directly subjected to ice loads may still experience inertial loads of stowed cargo and equipment resulting from ship/ice interaction. These inertial loads, based on accelerations determined according to the procedure approved by the Register, shall be considered in the design of these structures.

1.2.3.2 Glancing impact load characteristics.

The parameters defining the glancing impact load characteristics are reflected in the class factors listed in Tables 1.2.3.2-1 and 1.2.3.2-2.

1.2.3.2.1 Bow area.

In the bow area, the force F , line load Q , pressure P and load patch aspect ratio AR associated with the glancing impact load scenario are functions of the hull angles measured at the UIWL. The influence of the hull angles is captured through calculation of a bow shape coefficient f_a . The hull angles are defined in Fig. 1.2.3.2.1.

The waterline length of the bow region shall generally be divided into 4 sub-regions of equal length. The force F , line load Q , pressure P and load patch aspect ratio AR shall be calculated with respect to the mid-length position of each sub-region (each maximum of F , Q and P shall be used in the calculation of the ice load parameters P_{avg} , b and w).

1.2.3.2.1.1 The bow area load characteristics are determined as follows:

shape coefficient f_{a_i} :

$$f_{a_i} = \min(f_{a_{i1}}, f_{a_{i2}}, f_{a_{i3}}) \quad (1.2.3.2.1-1)$$

$$f_{a_{i1}} = (0,097 - 0,68(x/L - 0,15)^2) \cdot \alpha_i / (\beta_i')^{0,5};$$

$$f_{a_{i2}} = 1,2CF_F / (\sin(\beta_i') \cdot CF_C \cdot D^{0,64});$$

$$f_{a_{i3}} = 0,60;$$

force F , in MN:

$$F_i = f_{a_i} \cdot CF_C \cdot D^{0,64}; \quad (1.2.3.2.1-2)$$

load patch aspect ratio AR :

$$AR = 7,46 \cdot \sin(\beta_i') \geq 1,3; \quad (1.2.3.2.1-3)$$

line load Q , in MN/m:

$$Q_i = F_i^{0,61} CF_D / AR_i^{0,35}; \quad (1.2.3.2.1-4)$$

pressure P , in MPa:

$$P_i = F_i^{0,22} CF_D^2 AR_i^{0,3} \quad (1.2.3.2.1-5)$$

where i = sub-region considered;

L = ship length as defined in 1.1.3, Part II "Hull", but measured on the UIWL, in m;

x = distance from the forward perpendicular FP to station under consideration, in m;

α = waterline angle, in deg. (refer to Fig. 1.2.3.2.1);

β' = normal frame angle, in deg., measured as per normal to the outer shell (refer to Fig. 1.2.3.2.1);

D = ship displacement, in kt, but not less than 5 kt;

CF_C = crushing failure class factor according to Table 1.2.3.2-1;

CF_F = Flexural failure Class Factor according to Table 1.2.3.2-1;

CF_D = load patch dimensions class factor according to Table 1.2.3.2-1.

1.2.3.2.1.2 The bow area load characteristics for bow forms defined in 1.2.3.1.6 shall be determined according to the following formulae:

shape coefficient, f_{a_i} :

$$f_{a_i} = \alpha_i / 30; \quad (1.2.3.2.1.2-1)$$

Table 1.2.3.2-1

Class factors to be used for calculations according to 1.2.3.2.1.1

Polar class	Crushing failure class factor CF_C	Flexural failure class factor CF_F	Load patch dimensions class factor CF_D	Displacement class factor CF_{DIS}	Longitudinal strength class factor CF_L
PC1	17,69	68,60	2,01	250	7,46
PC2	9,89	46,80	1,75	210	5,46
PC3	6,06	21,17	1,53	180	4,17
PC4	4,50	13,48	1,42	130	3,15
PC5	3,10	9,00	1,31	70	2,50
PC6	2,40	5,49	1,17	40	2,37
PC7	1,80	4,06	1,11	22	1,81

Table 1.2.3.2-2

Class factors to be used for calculations according to 1.2.3.2.1.2

Polar class	Crushing failure class factor CF_C	Line load class factor CF_{QV}	Pressure class factor CF_{PV}
PC6	3,43	2,82	0,65
PC7	2,60	2,33	0,65

force F , in kN:

$$F_i = f a_i C F_{CV} D^{0,47}; \quad (1.2.3.2.1.2-2)$$

line load Q , in MN/m:

$$Q_i = F_i^{0,22} C F_{QV}; \quad (1.2.3.2.1.2-3)$$

pressure P , in kPa:

$$P_i = F_i^{0,56} C F_{PV} \quad (1.2.3.2.1.2-4)$$

where i = sub-region considered;

a = waterline angle, deg. (refer to Fig. 1.2.3.2.1);

D = ship displacement, in kt, but not less than 5 kt;

$C F_{CV}$ = crushing failure class factor according to Table 1.2.3.2-2;

$C F_{QV}$ = line load class factor according to Table 1.2.3.2-2;

$C F_{PV}$ = pressure class factor according to Table 1.2.3.2-2.

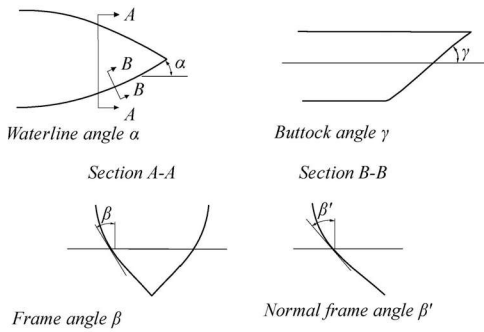


Fig. 1.2.3.2.1

Definition of hull angles

Notes: β' = normal frame angle at upper ice waterline, in deg.;

α = upper ice waterline angle, in deg.;

γ = buttock angle at upper ice waterline (angle of buttock line measured from horizontal), in deg.;

$\text{tg} \beta = \text{tg} \alpha / \text{tg} \gamma$;

$\text{tg} \beta' = \text{tg} \beta \cdot \cos \alpha$.

1.2.3.2.2 Hull areas other than the bow.

In the hull areas other than the bow, the force F_{NonBow} , in MN, and line load Q_{NonBow} , in MN/m, used in the determination of the load patch dimensions b_{NonBow} , w_{NonBow} and design pressure P_{avg} are determined according to the following formulae:

$$F_{NonBow} = 0,36 C F_C D F; \quad (1.2.3.2.2.2-1)$$

$$Q_{NonBow} = 0,639 F_{NonBow}^{0,61} C F_D \quad (1.2.3.2.2.2-2)$$

where $C F_C$ = crushing failure class factor according to Table 1.2.3.2-1;

$D F$ = ship displacement factor:

$D F = D^{0,64}$ if $D \leq C F_{DIS}$;

$D F = C F_{DIS}^{0,64} + 0,10(D - C F_{DIS})$ if $D > C F_{DIS}$;

D = ship displacement, in kt, but not less than 10 kt;

$C F_{DIS}$ = displacement class factor according to Table 1.2.3.2-1.

1.2.3.3 Design load patch.

In the bow area, and the bow intermediate ice belt area for ships with class notation **PC6** and **PC7**, the design load patch has dimensions of width w_{Bow} , in m, and height, b_{Bow} , in m, shall be determined according to the following formulae:

$$w_{Bow} = F_{Bow} / Q_{Bow}; \quad (1.2.3.3-1)$$

$$b_{Bow} = Q_{Bow} / P_{Bow} \quad (1.2.3.3-2)$$

where F_{Bow} = maximum force F_i , in kN, in the bow area according to 1.2.3.2.1;

Q_{Bow} = maximum line load Q_i , in MN/m, in the bow area according to 1.2.3.2.1;

P_{Bow} = maximum pressure P_i , in MPa, in the bow area according to 1.2.3.2.1.

In other hull areas, the design load patch has dimensions of width, w_{NonBow} , in m, and height, b_{NonBow} in m, shall be determined according to the following formulae:

$$w_{NonBow} = F_{NonBow} / Q_{NonBow};$$

$$b_{NonBow} = w_{NonBow} / 3,6$$

where F_{NonBow} = force, in kN, according to 1.2.3.2.2;

Q_{NonBow} = line load, in MN/m, according to 1.2.3.2.2.

1.2.3.3.2 In hull areas other than those covered by 1.2.3.3.1, the design load patch has dimensions of width w_{NonBow} and height b_{NonBow} in m, determined as follows:

$$w_{NonBow} = F_{NonBow} / Q_{NonBow}; \quad (1.2.3.3.2-1)$$

$$b_{NonBow} = w_{NonBow} / 3,6 \quad (1.2.3.3.2-2)$$

where F_{NonBow} = force determined by Formula (1.2.3.2.2.1.1), in MN;

Q_{NonBow} = line load determined by Formula (1.2.3.2.2.1.2), in MN/m.

1.2.3.4 Pressure within the design load patch.

1.2.3.4.1 The average pressure P_{avg} , in MPa, within a design load patch is determined as follows:

$$P_{avg} = F / (b \cdot w) \quad (1.2.3.4.1)$$

where F = F_{Bow} or F_{NonBow} as appropriate for the hull area under consideration, in MN;

b = b_{Bow} or b_{NonBow} as appropriate for the hull area under consideration, in m;

w = w_{Bow} or w_{NonBow} as appropriate for the hull area under consideration, in m.

1.2.3.4.2 Areas of higher, concentrated pressure exist within the load patch. In general, smaller areas have higher local pressures. Accordingly, the peak pressure factors listed in Table 1.2.3.4.2 are used to account for the pressure concentration on localized structural members.

1.2.3.5 Hull area factors.

Associated with each hull ice-strengthened areas is an area factor that reflects the relative magnitude of the load expected in that area. The area factors AF for each hull area are specified in Table 1.2.3.5-1.

In the event that a structural member spans across the boundary of a hull area, the largest hull area factor shall be used in the scantling determination of the member.

The values of hull area factors of stern ice belt S_i and stern lower S_l of ships having propulsion arrangements with azimuth thrusters are specified in Table 1.2.3.5-2.

For ships assigned the ice class mark **Icebreaker**, the area factor AF , for each hull area is specified in Table 1.2.3.5-3.

Table 1.2.3.4.2

Peak pressure factors

Structural member		Peak pressure factor PPF_i
Plating	Transversely-framed	$PPF_p = (1,8 - s) \geq 1,2$
	Longitudinally-framed	$PPF_p = (2,2 - 1,2 s) \geq 1,5$
Frames in transverse	With load distributing stringers	$PPF_t = (1,6 - s) \geq 1,0$
	With no load distributing stringers	$PPF_t = (1,8 - s) \geq 1,2$
Frames in bottom structures		$PPF_s = (1,6 - s) \geq 1,0$
Load carrying stringers Side and bottom longitudinals Web frames		$PPF_s = 1,0$ at $S_w \geq 0,5w$; $PPF_s = 2,0 - 2,0 \cdot S_w/w$ if $S_w < 0,5w$
where s = frame or longitudinal spacing, in m; S_w = web frame spacing, in m; w = ice load patch width, in m.		

Table 1.2.3.5-1

Hull area factors AF .

Hull area		Area	Polar class						
			PC1	PC2	PC3	PC4	PC5	PC6	PC7
Bow (B)	All	B	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Bow Intermediate (BI)	Ice belt	BI_i	0,90	0,85	0,85	0,80	0,80	1,00 ¹	1,00 ¹
	Lower	BI_l	0,70	0,65	0,65	0,60	0,55	0,55	0,50
	Bottom	BI_b	0,55	0,50	0,45	0,40	0,35	0,30	0,25
Midbody (M)	Ice belt	M_i	0,70	0,65	0,55	0,55	0,50	0,45	0,45
	Lower	M_l	0,50	0,45	0,40	0,35	0,30	0,25	0,25
	Bottom	M_b	0,30	0,30	0,25	²	²	²	²
Stern (S)	Ice belt	S_i	0,75	0,70	0,65	0,60	0,50	0,40	0,35
	Lower	S_l	0,45	0,40	0,35	0,30	0,25	0,25	0,25
	Bottom	S_b	0,35	0,30	0,30	0,25	0,15	²	²
¹ Refer to 1.2.3.1.3.									
² Ice strengthening is not required.									

Table 1.2.3.5-2

Hull area		Area	Polar class						
			PC1	PC2	PC3	PC4	PC5	PC6	PC7
Stern (S)	Ice belt	S_i	0,90	0,85	0,80	0,75	0,65	0,55	0,50
	Lower	S_l	0,60	0,55	0,50	0,45	0,40	0,40	0,40
	Bottom	S_b	0,5	0,30	0,30	0,25	0,15	¹	¹
¹ Ice strengthening is not required.									

1.2.4 Shell plate requirements.

1.2.4.1 The required minimum shell plate thickness t , in mm, is determined by the formula

$$t = t_{net} + t_s \quad (1.2.4.1)$$

where t_{net} = plate thickness required to resist ice loads according to 1.2.4.2, in mm;

t_s = corrosion and abrasion allowance according to 1.2.11, in mm.

1.2.4.2 The thickness of shell plating required to resist the design ice load t_{net} , in mm, depends on the orientation of the framing.

In the case of transversely-framed plating ($\Omega \geq 70$ deg.), including all bottom plating, i.e. in hull areas BI_b , M_b and S_b , the net thickness shall be determined by formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/(\sigma_y))^{0,5}/(1 + s/2b) \quad (1.2.4.2-1)$$

Table 1.2.3.5-3

Hull area		Area	Polar class						
			PC1	PC2	PC3	PC4	PC5	PC6	PC7
Bow (<i>B</i>)	All	<i>B</i>	1,00	1,00	1,00	1,00	1,00	1,00	1,00
Bow Intermediate (<i>BI</i>)	Ice belt	<i>BI_i</i>	0,90	0,85	0,85	0,85	0,85	1,00	1,00
	Lower	<i>BI_l</i>	0,70	0,65	0,65	0,65	0,65	0,65	0,65
	Bottom	<i>BI_b</i>	0,55	0,50	0,45	0,45	0,45	0,45	0,45
Midbody (<i>M</i>)	Ice belt	<i>M_i</i>	0,70	0,65	0,55	0,55	0,55	0,55	0,55
	Lower	<i>M_l</i>	0,50	0,45	0,40	0,40	0,40	0,40	0,40
	Bottom	<i>M_b</i>	0,30	0,30	0,25	0,25	0,25	0,25	0,25
Stern (<i>S</i>)	Ice belt	<i>S_i</i>	0,95	0,90	0,80	0,80	0,80	0,80	0,80
	Lower	<i>S_l</i>	0,55	0,50	0,45	0,45	0,45	0,45	0,45
	Bottom	<i>S_b</i>	0,35	0,30	0,30	0,30	0,30	0,30	0,30

In the case of longitudinally-framed plating ($\Omega \leq 20$ deg.), when $b \geq s$, the net thickness shall be determined by formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/\sigma_y)^{0,5}/(1 + s/2l). \quad (1.2.4.2-2)$$

In the case of longitudinally-framed plating ($\Omega \leq 20$ deg.), when $b < s$, the net thickness shall be determined by formula

$$t_{net} = 500s((AF \cdot PPF_p \cdot P_{avg})/\sigma_y)^{0,5} \cdot (2b/s - (b/s)^2)^{0,5}/(1 + s/2l). \quad (1.2.4.2-3)$$

where Ω = smallest angle between the chord of the waterline and the line of the main framing according to Fig. 1.2.4.2, in deg.;
 s = transverse frame spacing in transversely-framed ships or longitudinal frame spacing in longitudinally-framed ships, in m;
 AF = hull area factor from Table 1.2.3.5.1;
 PPF_p = peak pressure factor from Table 1.2.3.4.2;
 P_{avg} = average patch pressure according to Formula (1.2.3.4.1), in MPa;
 σ_y = minimum upper yield stress of the material, in N/mm²;
 b = height of design load patch, in m, where $b \geq (l-s/4)$ in the case determined by Formula (1.2.4.2-1);
 l = distance between frame supports, i.e. equal to the frame span as given in 1.2.5.5, but not reduced for any fitted end brackets, in m. When a load-distributing stringer is fitted, the length l need not be taken larger than the distance from the stringer to the most distant frame support.

When $20^\circ < \Omega < 70^\circ$, net thickness of the shell plating shall be determined by linear interpolation.

1.2.5 Framing. General.

1.2.5.1 Framing members of polar class ships shall be designed to withstand the ice loads defined in 1.2.3.

1.2.5.2 The term "framing member" refers to transverse and longitudinal local frames, load-carrying stringers and web frames in the hull strengthening regions (refer to Fig. 1.2.2.1).

1.2.5.3 The strength of a framing member is dependent upon the fixity that is provided at its supports. Fixity can be assumed where framing members are either continuous through the support or attached to a supporting section with a connection bracket. In other

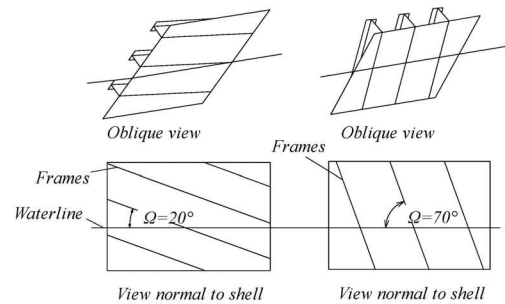


Fig. 1.2.4.2
Shell framing angle Ω

cases, simple support shall be assumed unless the connection can be demonstrated to provide significant rotational restraint. Fixity shall be ensured at the support of any framing which terminates within an ice-strengthened area.

1.2.5.4 The intersections of framing members with plate structures shall be executed in accordance with 3.10.2.4.5, Part II "Hull". The details for securing the ends of framing members at supporting sections, shall comply with 1.7.2.2 and 2.5.5, Part II "Hull".

1.2.5.5 The effective span of a framing member shall be determined on the basis of its moulded length. If end brackets are fitted, the effective span may be reduced in accordance with 3.10.2.2.3, Part II "Hull". Brackets shall be configured to ensure stability in the elastic and post-yield response regions.

1.2.5.6 When calculating the section modulus and shear area of a framing member, net thicknesses of the web, flange and attached shell plating shall be used. The shear area of a framing member may include that material contained over the full depth of the member, i.e. web area including portion of flange, if fitted, but excluding attached shell plating.

1.2.5.7 The actual net effective shear area A_w , in cm^2 , of a transverse or longitudinal local frame shall be determined by formula

$$A_w = ht_{wn}\sin\varphi_w/100 \quad (1.2.5.7)$$

where h = height of stiffener, in mm, refer to Fig. 1.2.5.7;

t_{wn} = net web thickness, in mm;

$t_{wn} = t_w - t_c$;

t_w = as built web thickness, in mm (refer to Fig. 1.2.5.7);

t_c = corrosion deduction, in mm, to be subtracted from the web and flange thickness (according to 3.10.4.1, Part II "Hull", but not less than t_s as required by 1.2.11.3);

φ_w = smallest angle between shell plate and stiffener web, measured at the midspan of the stiffener (refer to Fig. 1.2.5.7). The angle φ_w may be taken as 90 deg., provided the smallest angle is not less than 75 deg.

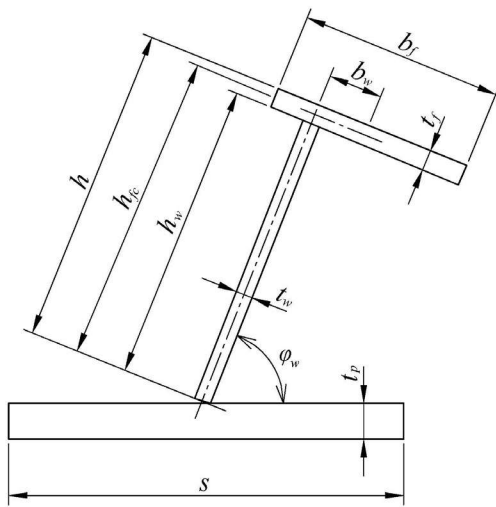


Fig. 1.2.5.7
Stiffener geometry

1.2.5.8 When the cross-sectional area of the attached plate flange exceeds the cross-sectional area of the local frame, the actual net effective plastic section modulus Z_p , in cm^3 , of a transverse or longitudinal frame shall be determined by formula

$$Z_p = A_{pn}t_{pn}/20 + \frac{h_w^2 t_{wn} \sin\varphi_w}{2000} + A_{fn}(h_{fc} \sin\varphi_w - b_w \cos\varphi_w)/10 \quad (1.2.5.8-1)$$

where h , t_{wn} , t_c , and φ_w are as given in 1.2.5.7 and s as given in 1.2.4.2;

A_{pn} = net cross-sectional area of the local frame, in cm^2 ;

t_{pn} = fitted net shell plate thickness, in mm, complying with t_{net} as required by 1.2.4.2;

h_w = height of local frame web, in mm (refer to Fig. 1.2.5.7);

A_{fn} = net cross-sectional area of local frame flange, in cm^2 ;

h_{fc} = height of local frame measured to centre of the flange area, in mm (refer to Fig. 1.2.5.7);

b_w = distance from mid thickness plane of local frame web to the centre of the flange area, in mm (refer to Fig. 1.2.5.7).

When the cross-sectional area of the local frame exceeds the cross-sectional area of the attached plate flange, the plastic neutral axis is located a distance z_{na} ,

in mm, above the attached shell plate, and when the cross-sectional area of the attached plate flange exceeds the cross-sectional area of the local frame, the actual net effective plastic section modulus, Z_p , in cm^3 , of a transverse or longitudinal frame is given by:

$$z_{na} = (100A_{fn} + ht_{wn} - 1000t_{pn}s)/2t_{wn} \quad (1.2.5.8-2)$$

$$Z_p = t_{pn}s(z_{na} + t_{pn}/2)\sin\varphi_w + \left(\frac{((h_w - z_{na})^2 + z_{na}^2)t_{wn}\sin\varphi_w}{2000} + A_{fn}((h_{fc} - z_{na})\sin\varphi_w - b_w\cos\varphi_w)/10 \right) \quad (1.2.5.8-3)$$

1.2.5.9 In case, when $20^\circ < \Omega < 70^\circ$, where Ω is defined as specified in 1.2.4.2, linear interpolation shall be used.

1.2.6 Framing. Local frames in bottom structures and transverse local frames in side structures.

1.2.6.1 The local frames in bottom structures (i.e. hull regions B_{fb} , M_b and S_b) and transverse local frames in side structures shall be dimensioned such that the combined effects of shear and bending do not exceed the plastic strength of the member. The plastic strength is defined by the magnitude of midspan load that causes the development of a plastic collapse mechanism. For bottom structure the patch load shall be applied with the dimension b parallel with the frame direction.

1.2.6.2 The actual net effective shear area of the frame A_w , in cm^2 , as defined in 1.2.5.7, shall comply with the following condition: $A_w \geq A_t$, where

$$A_t = (100^2 \cdot 0.5LL \cdot s(AF \cdot PPF_t \cdot P_{avg})) / (0.577\sigma_y) \quad (1.2.6.2)$$

where LL = length of loaded portion of span = lesser of a and b , in m;

a = frame span as defined in 1.2.5.5, in m;

b = height of design ice load patch as defined in 1.2.3.3;

s = transverse frame spacing, in m;

AF = hull area factor according to 1.2.3.5;

PPF_t = peak pressure factor PPF_t or PPF_s as appropriate according to Table 1.2.3.4.2;

P_{avg} = average pressure within load patch as defined in 1.2.3.4;

σ_y = minimum upper yield stress of the material, in N/mm^2 .

1.2.6.3 The actual net effective plastic section modulus of the plate/stiffener combination Z_p as defined in 1.2.5.8, shall comply with the following condition: $Z_p \geq Z_{pt}$, where Z_{pt} , in cm^3 , shall be the greater calculated on the basis of two load conditions: ice load acting at the midspan of the transverse frame; and the ice load acting near a support.

$$Z_{pt} = 100^3 LL \cdot Y \cdot s(AF \cdot PPF_t \cdot P_{avg})a \cdot A_1 / (4\sigma_y) \quad (1.2.6.3)$$

where AF , PPF_t , P_{avg} , LL , b , s , a and σ_y are as given in 1.2.6.2;

$Y = 1 - 0.5(LL/a)$;

A_1 = maximum of:

$A_{1A} = 1/(1 + j/2 + k_w j/2[(1 - a_1^2)^{0.5} - 1])$;

$A_{1B} = (1 - 1/(2a_1 \cdot Y))/(0.275 + 1.44k_w^2)$;

$j = 1$ for framing with one simple support outside the ice-strengthened areas;

$j = 2$ for framing without any simple supports;

$a_1 = A_t / A_w$;

A_t = minimum shear area of transverse frame as given in 1.2.6.2, in cm^2 ;

A_w = effective net shear area of transverse frame (calculated according to 1.2.5.7), in cm^2 ;

$k_w = 1/(1 + 2A_{fn}/A_w)$, with A_{fn} as given in 1.2.5.8;

$k_z = z_p/Z_p$, in general;
 $k_z = 0,0$, when the frame is arranged with end bracket;
 z_p = sum of individual plastic section moduli of flange and shell plate as fitted, in cm^3 ;
 $z_p = (b_f t_{fn}^2/4 + b_{eff} t_{pn}^2/4)/1000$;
 b_f = flange breadth, in mm, refer to Fig. 1.2.5.7;
 t_{fn} = net flange thickness, in mm;
 $t_{fn} = t_f - t_c$ (t_c as given in 1.2.5.7);
 t_f = as-built flange thickness, in mm, refer to Fig. 1.2.5.7;
 t_{pn} = the fitted net shell plate thickness, in mm (not to be less than t_{net} as given in 1.2.4);
 b_{eff} = effective width of shell plate flange, in mm;
 $b_{eff} = 500$ s;
 Z_p = net effective plastic section modulus of transverse frame (calculated according to 1.2.5.8), in cm^3 .

1.2.6.4 The scantlings of the frame shall meet the structural stability requirements of 1.2.9.

1.2.7 Framing. Longitudinal local frames in side structures.

1.2.7.1 Longitudinal local frames in side structures shall be dimensioned such that the combined effects of shear and bending do not exceed the plastic strength of the member. The plastic strength is defined by the magnitude of midspan load that causes the development of a plastic collapse mechanism.

1.2.7.2 The actual net effective shear area of the frame A_w as defined in 1.2.5.7, shall comply with the following condition: $A_w \geq A_L$, where

$$A_L = 100^2 (AF \cdot PPF_s \cdot P_{avg}) \cdot 0,5 b_1 a / (0,577 \sigma_y), \text{ in } \text{cm}^2 \quad (1.2.7.2)$$

where AF = hull area factor according to 1.2.3.5;

PPF_s = refer to Table 1.2.3.4.2;

P_{avg} = average pressure within load patch according to 1.2.3.4;

$b_1 = k_0 b_2$, in m;

$k_0 = 1 - 0,3/b'$;

$b' = b/s$;

b = height of design ice load patch according to 1.2.3.3;

s = spacing of longitudinal frames, in m;

$b_2 = b(1 - 0,25b')$, in m, if $b' < 2$;

$b_2 = s$, in m, if $b' \geq 2$;

a = effective span of longitudinal local frame according to 1.2.5.5;

σ_y = minimum upper yield stress of the material, in N/mm^2 .

1.2.7.3 The actual net effective plastic section modulus of the plate/stiffener combination Z_p as defined in 1.2.5.8, shall comply with the following condition: $Z_p \geq Z_{pL}$, where

$$Z_{pL} = 100^3 (AF \cdot PPF_s \cdot P_{avg}) b_1 a^2 A_4 / 8 \sigma_y, \text{ in } \text{cm}^3, \quad (1.2.7.3)$$

where AF , PPF_s , P_{avg} , b_1 , a and σ_y are as given in 1.2.7.2;

$A_4 = 1/(2 + k_{wl}[(1 - a_4^2)^{0,5} - 1])$;

$a_4 = A_L/A_w$;

A_L = minimum shear area for longitudinal as given in 1.2.7.2, in cm^2 ;

A_w = net effective shear area of longitudinal (calculated according to 1.2.5.7), in cm^2 ;

$k_{wl} = 1/(1 + 2A_{fn}/A_w)$ with A_{fn} as given in 1.2.5.8.

1.2.7.4 The scantlings of the longitudinals shall meet the structural stability requirements of 1.2.9.

1.2.8 Framing. Web frame and load-carrying stringers.

1.2.8.1 Web frames and load-carrying stringers shall be designed to withstand the ice load patch as defined in 1.2.3. The load patch shall be applied at locations where

the capacity of these members under the combined effects of bending and shear is minimised.

1.2.8.2 Web frames and load-carrying stringers shall be dimensioned such that the combined effects of shear and bending do not exceed the plastic strength of the member. The plastic strength is defined by the magnitude of midspan load that causes the development of a plastic collapse mechanism. Where the structural configuration is such that members do not form part of a grillage system, the appropriate peak pressure factor (PPF) from Table 1.2.3.4.2 shall be used. Lightening holes and cutouts shall be accordance with 3.10.2.4.8, Part II "Hull".

1.2.8.3 For determination of scantlings of load-carrying stringers, web frames supporting local frames, or web frames supporting load-carrying stringers forming part of a structural grillage system, appropriate methods as outlined in 1.2.17 shall normally be used.

1.2.8.4 The scantlings of web frames and load-carrying stringers shall meet the structural stability requirements of 1.2.9.

1.2.9 Framing. Structural stability.

1.2.9.1 To prevent local buckling in the web, the ratio of web height h_w to net web thickness t_{wn} of any framing member shall not exceed:

for flat bar sections:

$$h_w / t_{wn} \leq 282 / \sigma_y^{0,5}; \quad (1.2.9.1-1)$$

for bulb, tee and angle sections:

$$h_w / t_{wn} \leq 805 / \sigma_y^{0,5} \quad (1.2.9.1-2)$$

where h_w = web height;

t_{wn} = net web thickness;

σ_y = minimum upper yield stress of the material, in N/mm^2 .

1.2.9.2 Framing members for which it is not practicable to meet the requirements of 1.2.9.1 (e.g. load-carrying stringers or deep web frames) are required to have their webs effectively stiffened. The scantlings of the web stiffeners shall ensure the structural stability of the framing member. The minimum net web thickness for these framing members shall not be less than determined according the following formula:

$$t_{wn} = 2,63 \cdot 10^{-3} c_1 \sqrt{\frac{\sigma_y}{5,34 + 4(c_1/c_2)^2}} \quad (1.2.9.2)$$

where $c_1 = h_w - 0,8h$, in mm;

h_w = web height of stringer/web frame, in mm (refer to Fig. 1.2.9.2);

h = height of framing member penetrating the member under consideration (0 if no such framing member), in mm (refer to Fig. 1.2.9.2);

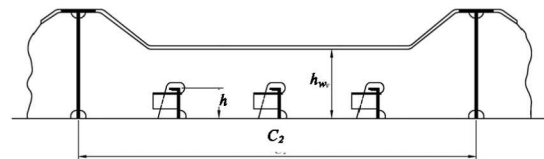


Fig. 1.2.9.2
Parameter definition for web stiffening

c_2 = spacing between supporting structure oriented perpendicular to the member under consideration, in mm (refer to Fig. 1.2.9.2);
 σ_y = minimum upper yield stress of the material, in N/mm².

1.2.9.3 In addition, the following shall be satisfied:

$$t_{wn} \geq 0,35 t_{pn} (\sigma_y / 235)^{0,5} \quad (1.2.9.3)$$

where σ_y = minimum upper yield stress of the material, in N/mm²;
 t_{wn} = net thickness of the web, in mm;
 t_{pn} = net thickness of the shell plate in way the framing member, in mm.

1.2.9.4 To prevent local flange buckling of welded profiles, the following shall be satisfied:

.1 the flange width b_f in mm, shall not be less than five times the net thickness of the web t_{wn} ;

.2 the flange outstand b_{out} in mm, shall meet the following requirement:

$$b_{out} / t_{fn} \leq 155 / \sigma_y^{0,5} \quad (1.2.9.4.2)$$

where t_{fn} = net thickness of flange, in mm;
 σ_y = minimum upper yield stress of the material, in N/mm².

1.2.10 Plated structures.

1.2.10.1 Plated structures are those stiffened plate elements in contact with the hull and subject to ice loads. These requirements are applicable to an inboard extent which is the lesser of:

.1 web height of adjacent parallel web frame or stringer; or

.2 2,5 times the depth of framing that intersects the plated structure.

1.2.10.2 The thickness of the plating and the scantlings of attached stiffeners shall be such that the degree of end fixity necessary for the shell framing is ensured.

1.2.10.3 The stability of the plated structure shall adequately withstand the ice loads defined in 1.2.3.

1.2.11 Corrosion/abrasion additions and steel renewal.

1.2.11.1 Effective protection against corrosion and ice-induced abrasion is recommended for all external surfaces of the shell plating for Polar Class ships.

1.2.11.2 The values of corrosion/abrasion additions, t_s , in mm, to be used in determining the shell plate thickness are listed in Table 1.2.11.2.

Table 1.2.11.2
Corrosion/abrasion additions for shell plating

Hull area	t_s , in mm					
	With effective protection			Without effective protection		
	PC1 to PC3	PC4 and PC5	PC6 and PC7	PC1 to PC3	PC4 and PC5	PC6 and PC7
B, BI_i	3,5	2,5	2,0	7,0	5,0	4,0
BI_b, M_b, S_i	2,5	2,0	2,0	5,0	4,0	3,0
M_b, S_b, BI_b, M_b, S_b	2,0	2,0	2,0	4,0	3,0	2,5

1.2.11.3 Polar class ships shall have a minimum corrosion/abrasion addition of $t_s = 1,0$ mm applied to all internal structures within the ice-strengthened hull areas, including plated members adjacent to the shell, as well as stiffener webs and flanges.

1.2.11.4 Steel renewal for ice strengthened structures is required when the gauged thickness is less than $t_{net} + 0,5$ mm.

1.2.12 Materials.

1.2.12.1 Steel grades of plating for hull structures shall be determined according to Table 1.2.12.4 and 1.2.12.5 based on the as-built thickness, the polar class and the material class of structural members according to 1.2.12.2.

1.2.12.2 Material classes specified in Table 1.2.3.7-1, Part II "Hull" are applicable to polar class ships regardless of the ship's length. In addition, material classes for weather and sea exposed structural members and for members attached to the weather and sea exposed plating are specified in Table 1.2.12.2. Where the material classes in Table 1.2.3.7-1, Part II "Hull" and in Table 1.2.12.2 differ, the higher material class shall be applied.

1.2.12.3 Regardless of polar class, steel grades for all shell plates situated below the level of 0,3 m below the lower waterline (refer to Fig. 1.2.12.3) and attached framing of hull structures and appendages shall be obtained from Table 1.2.3.7-2, Part II "Hull" for structural members specified in Table 1.2.12.2.

Table 1.2.12.2

Material classes for structural members of polar ships

Structural members	Material class
Shell plating within the bow and bow intermediate ice belt hull areas (B, BI_i)	II
All weather and sea exposed secondary and primary (as defined in Table 1.2.3.7-1, Part II "Hull") structural members outside 0,4L amidships	I
Plating materials for stem and stern frames, rudder horn, rudder, propeller nozzle, shaft brackets, ice skeg, ice knife and other appendages subject to ice impact loads	II
All inboard framing members attached to the weather and sea-exposed plating including any contiguous inboard member within 600 mm of the shell plating	I
Weather-exposed plating and attached framing in cargo holds of ships which by nature of their trade have their cargo hold hatches open during cold weather operations	I
All weather and sea exposed special (as defined in Table 1.2.3.7-1, Part II "Hull") structural members within 0,2L from FP	II

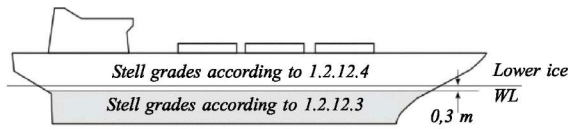


Fig. 1.2.12.3
Steel grade requirements for submerged
and weather exposed shell plating

with vertical or bulbous bows. Hence the longitudinal strength requirements specified in 1.2.13 shall not be considered for ships with stem angle γ_{stem} equal to or larger than 80 deg.

1.2.13.1.3 When determine design loads, ice loads shall only be combined with still water loads. The combined stress state shall be evaluated against permissible bending and shear stresses at different sections

Table 1.2.12.4

Steel grades for weather exposed plating

Thickness t , in mm	Material Class I				Material Class II				Material Class III					
	PC1 to PC5		PC6 and PC7		PC1 to PC5		PC6 and PC7		PC1 to PC3		PC4 and PC5		PC6 and PC7	
	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT	MS	HT
$t \leq 10$	B	AH	B	AH	B	AH	B	AH	E	EH	E	EH	B	AH
$10 < t \leq 15$	B	AH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$15 < t \leq 20$	D	DH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$20 < t \leq 25$	D	DH	B	AH	D	DH	B	AH	E	EH	E	EH	D	DH
$25 < t \leq 30$	D	DH	B	AH	E	EH2	D	DH	E	EH	E	EH	E	EH
$30 < t \leq 35$	D	DH	B	AH	E	EH	D	DH	E	EH	E	EH	E	EH
$35 < t \leq 40$	D	DH	D	DH	E	EH	D	DH	F	FH	E	EH	E	EH
$40 < t \leq 45$	E	EH	D	DH	E	EH	D	DH	F	FH	E	EH	E	EH
$45 < t \leq 50$	E	EH	D	DH	E	EH	D	DH	F	FH	F	FH	E	EH

Notes: 1. Includes weather-exposed plating of hull structures and appendages, as well as their outboard framing members, situated above a level of 0,3 m below the lowest ice waterline.
2. Grades D, DH are allowed for a single strake of side shell plating not more than 1,8 m wide from 0,3 m below the lowest ice waterline.

1.2.12.4 Steel grades for shell plates in the region of alternating waterlines and above according to Fig. 1.2.12.3, and attached framing of hull structures and appendages shall be obtained from Table 1.2.12.4.

1.2.12.5 Materials of castings shall comply with the requirements of Part XIII "Materials" for specified design temperature.

1.2.13 Longitudinal strength.

1.2.13.1 Application.

1.2.13.1.1 A ramming impact on the bow is the design scenario for the evaluation of the longitudinal strength of the hull.

1.2.13.1.2 Intentional ramming shall not be considered as a design scenario for ships which are designed

along the ship's length. In addition, sufficient buckling strength shall also be verified.

1.2.13.2 Design vertical ice force at the bow.

1.2.13.2.1 The design vertical ice force at the bow F_{IB} , MN, shall be taken as:

$$F_{IB} = \min(F_{IB,1}; F_{IB,2}) \quad (1.2.13.2.1-1)$$

$$\text{where } F_{IB,1} = 0,534 K_1^{0,15} \sin^{0,2}(\gamma_{stem}) (DK_h)^{0,5} CF_L; \quad (1.2.13.2.1-2)$$

$$F_{IB,2} = 1,20 CF_L; \quad (1.2.13.2.1-3)$$

K_1 = indentation parameter = K_f / K_h ;

.1 for the case of a blunt bow form:

$$K_f = (2C \cdot B^{1-e_b} / (1 + e_b))^{0,9} \lg(\gamma_{stem})^{-0,9(1+e_b)};$$

.2 for the case of wedge bow form ($\alpha_{stem} < 80^\circ$), $e_b = 1$ and the above simplifies to:

$$K_f = (\lg(\alpha_{stem}) / \lg^2(\gamma_{stem}))^{0,9};$$

$$K_h = 0,01 A_{wp}, \text{ in MN/m};$$

CF_L = longitudinal strength class factor from Table 1.2.3.2.1;

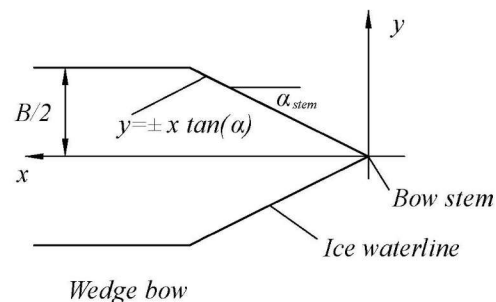
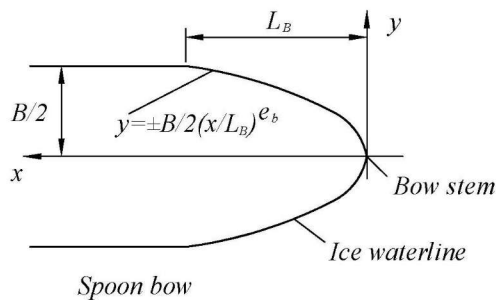


Fig. 1.2.13.2.1-1
Bow shape definition

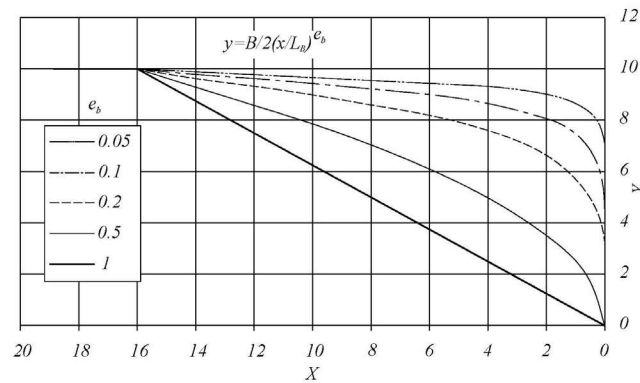


Fig. 1.2.13.2.1-2

Illustration of e_b effect on the bow shape for $B = 20$ and $L_B = 16$

e_b = bow shape exponent which best describes the waterplane (refer to Figs. 1.2.13.2.1-1 and 1.2.13.2.1-2);

$e_b = 1,0$ for a simple wedge bow form;

$e_b = 0,4$ to $0,6$ for a spoon bow form;

$e_b = 0$ for a landing craft bow form;

an approximate e_b determined by a simple fit is acceptable;

γ_{stem} = stem angle to be measured between the horizontal axis and the stem tangent at the upper ice waterline, deg. (buttock angle as per Fig. 1.2.3.2.1.1.1 measured on the centreline);

α_{stem} = waterline angle measured in way of the stem at the upper ice waterline (UIWL), in deg. (refer to Figure 1.2.13.2.1-1);

$C = 1/(2(L_B/B)^{e_b})$;

B = ship moulded breadth, in m;

L_B = bow length used in the equation $y = B/2(x/L_B)^{e_b}$, in m (refer to Figs. 1.2.13.2.1-1 and 1.2.13.2.1-2);

D = ship displacement, in kt, not to be taken less than 10 kt;

A_{wp} = ship waterplane area, in m^2 ;

CF_F = flexural failure class factor from Table 1.2.3.2.1.

Where applicable, draught dependent quantities shall be determined at the waterline corresponding to the loading condition under consideration.

1.2.13.3 Design vertical shear force.

1.2.13.3.1 The design vertical ice shear force F_I , in MN, along the hull girder shall be determined by formula

$$F_I = C_f F_{IB} \quad (1.2.13.3.1)$$

where C_f = longitudinal distribution factor to be taken as follows:

for positive shear force:

$C_f = 0,0$ in sections $0,0 \leq x/L \leq 0,6$;

$C_f = 1,0$ in sections $0,9 \leq x/L \leq 1,0$;

for negative shear force:

$C_f = 0,0$ in section $x/L = 0,0$;

$C_f = -0,25 x/L$ in sections $0,0 < x/L < 0,2$;

$C_f = -0,5$ in sections $0,2 \leq x/L \leq 0,6$;

$C_f = 2,5 x/L - 2$ in sections $0,6 < x/L < 0,8$;

$C_f = 0,0$ in sections $0,8 \leq x/L \leq 1,0$;

x = distance from of the design section to the aft perpendicular, in m;

L = ship length measured on the UIWL according to 1.1.3, Part II "Hull".

1.2.13.3.2 The applied vertical shear stresses shall be determined according to 1.6.5.1, Part II "Hull" by substituting the design vertical ice shear force N_w , in kN, for the design vertical wave shear force F_b , in kN.

1.2.13.4 Design vertical ice bending moment.

1.2.13.4.1 The design vertical ice bending moment M_I shall be determined by formula

$$M_I = 0,1 C_m L \sin^{-0,2}(\gamma_{stem}) F_{IB} \quad (1.2.13.4.1)$$

where L = ship length measured on UIWL according to 1.1.3, Part II "Hull";

γ_{stem} = according to 1.2.13.2.1;

F_{IB} = design vertical ice force at the bow, in MN;

C_m = longitudinal distribution factor for design vertical ice bending moment to be taken as follows:

$C_m = 0,0$ in section $x/L = 0,0$;

$C_m = 2,0 x/L$ in sections $0,0 < x/L < 0,5$;

$C_m = 1,0$ in sections $0,5 \leq x/L \leq 0,7$;

$C_m = 2,96 - 2,8 x/L$ in sections $0,7 < x/L < 0,95$;

$C_m = 0,3$ in section $x/L = 0,95$;

$C_m = 6,0 - 6,0 x/L$ in sections $0,95 < x/L < 1,0$;

$C_m = 0,0$ in section $x/L = 1,0$;

x = distance from the design section to the aft perpendicular, in m.

Where applicable, draught dependent quantities shall be determined at the waterline corresponding to the loading condition under consideration.

1.2.13.4.2 The applied vertical bending stress σ_a shall be determined according to 1.6.5.1, Part II "Hull" by substituting the design vertical ice bending moment M_w , in kN, for the design vertical wave bending moment. The ship still water bending moment shall be taken as the maximum sagging moment.

1.2.13.5 Longitudinal strength criteria.

1.2.13.5.1 The strength criteria provided in Table 1.2.13.5.1 shall be satisfied. The design stress is not to exceed the permissible stress.

1.2.14 Stem and sternframe construction.

1.2.14.1 Polar class ships shall have a solid section stem made of steel. The stems and sternframes of polar class ships and icebreakers of PC1 and PC, as well as the sternframes of polar class PC1, PC2, PC3, PC4 and PC5 ships, shall be made of forged or cast steel. Stems and sternframes welded of cast or forged parts are admissible.

1.2.14.2 In PC3, PC4, PC5, PC6, PC7 polar class ships and polar class icebreakers less than PC4, a stem

Table 1.2.13.5.1

Longitudinal strength criteria

Failure mode	Applied stress	Permissible stress when $\sigma_y/\sigma_u \leq 0,7$	Permissible stress when $\sigma_y/\sigma_u > 0,7$
Tension	σ_a	$\eta \sigma_y$	$\eta 0,41(\sigma_u + \sigma_y)$
Shear	τ_a	$\eta \sigma_y / 3^{0,5}$	$\eta 0,41(\sigma_u + \sigma_y) / 3^{0,5}$
Buckling	σ_a	σ_c for plating and for web plating of stiffeners $\sigma_c / 1,1$ for stiffeners	
	τ_a	τ_c	

where σ_a = applied vertical bending stress, in N/mm²;
 τ_a = applied vertical shear stress, in N/mm²;
 σ_y = minimum upper yield stress of the material, in N/mm²;
 σ_u = ultimate tensile strength of material, in N/mm²;
 σ_c = critical buckling stress in compression, according to 1.6.5.3, Part II "Hull", in N/mm²;
 τ_c = critical buckling stress in shear, according to 1.6.5.3, Part II "Hull", in N/mm²;
 $\eta = 0,8$.
 $\eta = 0,6$ for ships with ice class mark Icebreaker.

of combined structure (a bar with thickened plates welded thereto) or plate structure may be used. Welding seams of the combined or plated structure stems shall be made with full penetration in compliance with the requirements of Part XIV "Welding".

In PC6 and PC7 polar class ships stemframes of combined structure or plate structure may be used.

1.2.14.3 In PC3, PC4, PC5, PC6, PC7 polar class ships, the stem shall be strengthened by a centre line web having its section depth equal to h_p at least (refer to Table 1.2.14.3) with a face plate along its free edge or a longitudinal bulkhead fitted on the ship centreline, on the entire stem length from the keel plate to the nearest deck or platform situated above the area B (refer to Fig. 1.2.2.1) The thickness of this plate shall not be less than that of the brackets according to 1.2.14.4. In all polar class icebreakers and PC1, PC2 polar class ships, a longitudinal bulkhead may be substituted for the centre line web.

Table 1.2.14.3

h_p , in m				
PC7	PC6	PC5	PC4	PC3
0,6	0,6	1,0	1,3	1,5

1.2.14.4 Within the vertical extent defined in 1.2.14.3, the stem shall be strengthened by horizontal webs at least 0,6 m in depth and spaced not more than 0,6 m apart. Where in line with side stringers, the webs shall be attached to them. In stems of combined or plate type, the webs shall be extended beyond the welded butts of the stem and shell plating.

Above the deck or platform located higher than the upper boundary of region B, the spacing of horizontal webs may gradually increase to 1,2 m in polar class icebreakers and PC1, PC2, PC3 polar class ships, and to 1,5 m in ships of other polar class.

The web thickness shall be adopted not less than half the stem plate thickness according to 1.2.4.7. The free

edges of webs shall be strengthened with face plates welded to the frames at their ends. The side stringers of the fore peak shall be connected to the webs fitted in line with them.

In case of a full bow, vertical stiffeners may be required additionally to be fitted to the stem plates.

1.2.14.5 Where the stern frame has an appendage (ice knife), the clearance between the latter and the rudder plate shall not exceed 100 mm. The appendage shall be reliably connected to the stern frame. Securing the appendage to plate structures is not permitted.

1.2.14.6 In icebreakers, the lower edge of solepiece shall be constructed with a slope of 1:8 beginning from the propeller post.

1.2.14.7 Cross-sectional area of the stem A_{st} , in cm², irrespective of configuration shall not be less than determined by formula

$$A_{st} = c_t c_k f(D) \quad (1.2.14.7-1)$$

where c_k = coefficient according to Table 1.2.14.7;

$$f(D) = 31D + 137 \text{ if } D < 5 \text{ kt;}$$

$$f(D) = 100D^{2/3} \text{ if } D \geq 5 \text{ kt;}$$

D = displacement of the ship, in kt;

c_t = coefficient equal to 1,0 for polar class ships; 1,4 for icebreakers.

c_k = coefficient according to Table 1.2.14.7.

Table 1.2.14.3

c_k						
PC7	PC6	PC5	PC4	PC3	PC2	PC1
0,54	0,54	0,66	1,02	1,25	1,40	1,55

Section modulus Z_{st} , in cm³, of the stem cross-sectional area to the axis perpendicular to the centreline, shall be not less than determined by formula

$$Z_{st} = 1,2 Q_{Bow} \quad (1.2.14.7-2)$$

where Q_{Bow} = line load according to 1.2.3.2.1, in kN/m.

To be included in the design cross-sectional area of a combined or plate stem are areas of shell plates and

centreline girder or of longitudinal bulkhead on the centreline on a breadth not exceeding ten times the thickness of relevant plates.

The plate thickness of stem plate t_{net}^{stem} , in mm, of combined or plate stem, shall be not less than determined by formula

$$t_{net}^{stem} = 1,2 t_{net} a_b / s \sqrt{\sigma_y / \sigma_{y1}} \quad (1.2.14.7-3)$$

t_{net} = net thickness of outer shell according to 1.2.4.2;

s = transverse frame spacing, in m;

a_b = distance between the brackets, in m;

σ_y = minimum upper yield stress of outer shell material, in N/mm²;

σ_{y1} = minimum upper yield stress of stem material, in N/mm².

1.2.15 Appendages.

1.2.15.1 All appendages shall be designed to withstand forces appropriate for the location of their attachment to the hull structure or their position within a hull area.

1.2.15.2 Load definition and response criteria shall be determined by the Register.

1.2.16 Local details.

1.2.16.1 For the purpose of transferring ice-induced loads to supporting structure (bending moments and shear forces), local design details shall comply with the Register requirements.

1.2.16.2 The loads carried by a member in way of cut-outs shall not cause instability. Where necessary, the structure shall be stiffened.

1.2.17 Direct calculations.

1.2.17.1 Application.

Direct calculations shall be used for load carrying stringers and web frames forming part of a grillage system and shall not be utilised as an alternative to the analytical procedures prescribed for the shell plating and local frame requirements specified in 1.2.4, 1.2.6 and 1.2.7.

Direct calculations shall be made by the finite element method in the static nonlinear elastoplastic design. While calculating, the nonlinear dependence between the stresses and deformations shall be considered, if the yield stress reached.

The tensile diagram with linear hardening shall be used to describe the material properties.

1.2.17.2 Requirements for finite element model (FEM).

3-D finite element model shall be used for calculations. The model dimensions shall be specified so that to include web frames forming part of a grillage system in the ice reinforcement area as given in 1.2.2, and to comply with the minimum requirements to the finite element model as specified in Table 1.2.17.2-1.

The FEM model shall represent the geometry of the hull form.

Boundary conditions for FEM model shall comply with the requirements given in Table 1.2.17.2-2.

Structures to be modelled shall include side shell, web frames, stringers, local frames, inner skin and attached local frames, web stiffeners and brackets.

Table 1.2.17.2-1
Minimum requirements for finite element model dimensions

Boundary	Type of side structure	
	Double side structure	Single side structure
Fore	Transverse bulkhead	
Aft	Transverse bulkhead	
Upper	Upper deck	Deck, platform or double bottom, located above icebelt region
Lower	Double bottom	Deck, platform or double bottom, located above icebelt region

Table 1.2.17.2-2

Boundary conditions

Location of finite element model boundaries	Translational			Rotational		
	δ_x	δ_y	δ_z	θ_x	θ_y	θ_z
Top and bottom boundaries	—	×	×	×	×	×
Fore and aft boundaries	×	×	—	×	×	×
Note. × — fixed.						

Structural idealization shall reasonably represent the non-linear behavior of the structure with the following minimum requirements to be satisfied:

shell elements shall be used for representing the side shell, inner skin, web frames, stringers, and local frames web and flange;

beam elements shall be used for representing local frames outside ice belt region;

rod elements shall be used for representing web stiffeners.

Mesh size shall be selected such that the modelled structures reasonably represent the non-linear behavior of the structures with the following minimum requirements to be satisfied:

it is preferable to use quadrilateral elements that are nearly square in shape, the aspect ratio of the elements shall be kept below 1/3;

triangular elements shall be avoided as much as practical;

web of the web frames shall be divided into at least five elements;

web of the local frames shall be divided into at least three elements;

areas where high local stress or large deflections are expected could be modeled with finer mesh, while the areas outside ice belt region could be modelled with coarser mesh.

Finite elements thickness shall be equal to the net thickness of the structure.

1.2.17.3 Acceptance criteria.

The direct calculation shall demonstrate that ultimate structural capacity of the grillage structure, P_{ult} , in MPa,

is not less than the design ice pressure within the hull area under consideration, as specified in 1.2.3.4. The criteria shall be satisfied for representative locations of the design load patch, as specified in 1.2.17.4.

The ultimate structural capacity of the grillage structure shall be calculated in accordance with 1.2.17.5.

1.2.17.4 Load patch.

The design load patch specified in 1.2.3.3 shall be applied, without being combined with any other load.

The design load patch shall be applied normal to the side shell plating.

The load patch shall be located where the bending and shear capacity of the web frame or load carrying stringer is minimized. The minimum required locations of the design load patch are as follows:

top edge of the load patch is in line with top boundary of the ice belt, at the central web frame of the grillage;

bottom edge of the load patch is in line with the bottom boundary of the ice belt, at the central web frame of the grillage;

load patch centroid is located at the midspan of the central web frame of the grillage;

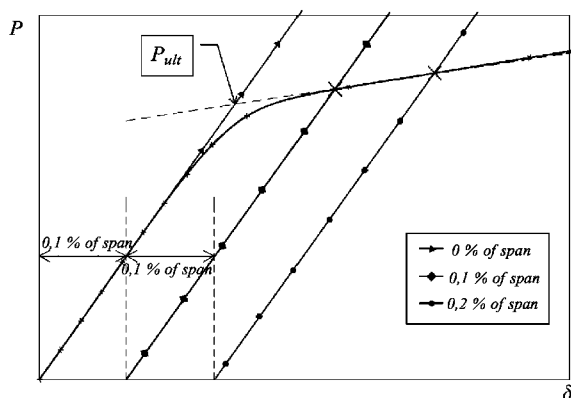
load patch centroid is located at the midspan of the central load carrying stringer of the grillage.

1.2.17.5 Ultimate structural capacity.

The ultimate structural capacity of the grillage shall be based on a non-linear static FEM analysis with the gradually increasing loads. The load increment shall be sufficiently fine to ensure the accuracy of the curve (P - δ).

The analysis shall reliably capture buckling of the elements by the method agreed with the Register.

Ultimate structural capacity P_{ult} shall be based on pressure-deflection (P - δ) curve using modified tangent intersection method according to Fig. 1.2.17.5.



Note. P — pressure applied to the grillage structure;
 δ — maximum deflection of the web frame or load-carrying stringer in the grillage structure.

Fig.1.2.17.5

Ultimate structural capacity calculation using tangent intersection method

1.2.17.6 Requirements for software.

FEM computation program shall be able to address the aspects of non-linear material behavior, structural idealization, meshing, load application and elasto-plastic calculations according to the requirements specified in 1.2.17.1 to 1.2.17.5. In addition, applicable software shall be able to address all possible computational errors.

1.2.18 Welding.

1.2.18.1 All welding within ice-strengthened areas shall be of the double continuous type.

1.2.18.2 Continuity of strength shall be ensured at all structural connections.

1.3 MACHINERY REQUIREMENTS FOR POLAR CLASS SHIPS

1.3.1 Application.

The requirements of this Chapter apply to main propulsion, steering gear, emergency and essential auxiliary systems essential for the safety of the ship and the survivability of the crew.

1.3.2 General.

1.3.2.1 Drawings and particulars to be submitted:

.1 details of the environmental conditions and the required ice class for the machinery, if different from ship's ice class;

.2 detailed drawings of the main propulsion machinery. Description of the main propulsion, steering, emergency and essential auxiliaries shall include operational limitations. Information on essential main propulsion load control functions;

.3 description detailing how main, emergency and auxiliary systems are located and protected to prevent problems from freezing, ice and snow and evidence of their capability to operate in intended environmental conditions;

.4 calculations and documentation indicating compliance with the requirements of this Chapter.

1.3.2.2 System design.

1.3.2.2.1 Machinery and supporting auxiliary systems shall be designed, constructed and maintained to comply with the requirements of periodically unmanned machinery spaces with respect to fire safety. Any automation plant (i.e. control, alarm, safety and indication systems) for essential systems installed shall be maintained to the same standard.

1.3.2.2.2 Systems, subject to damage by freezing, shall be drainable.

1.3.2.2.3 Single screw vessels classed PC1 to PC5 inclusive shall have means provided to ensure sufficient ship operation in the case of propeller damage including CP-mechanism.

1.3.3 Materials.

1.3.3.1 Materials exposed to sea water.

Materials exposed to sea water, such as propeller blades, propeller hub and blade bolts shall have an

elongation not less than 15 per cent on a test piece the length of which is five times the diameter.

Charpy V-notch impact test (determination of impact energy KV for sharply-notched specimen) shall be carried out for other than bronze and austenitic steel materials. Test pieces taken from the propeller castings shall be representative of the thickest section of the blade. An average impact energy KV value of 20 J taken from three Charpy V-notch tests shall be obtained at minus 10 °C.

1.3.3.2 Materials exposed to sea water temperature.

Materials exposed to sea water temperature shall be of steel or other approved ductile material. An average impact energy KV value of 20 J taken from three tests shall be obtained at minus 10 °C.

1.3.3.3 Material exposed to low air temperature.

Materials of essential components exposed to low air temperature shall be of steel or other approved ductile material.

An average impact energy KV value of 20 J taken from three Charpy V-notch tests shall be obtained at 10 °C below the lowest design temperature.

1.3.4 Ice interaction load.

1.3.4.1 Propeller ice interaction.

The present requirements cover open and ducted type propellers situated at the stern of a ship having controllable pitch or fixed pitch blades. Ice loads on bow propellers and pulling type propellers shall receive special consideration by the Register.

The given loads are expected, single occurrence, maximum values for the whole ships service life for normal operational conditions.

These loads do not cover off-design operational conditions, for example when a stopped propeller is dragged through ice.

The present requirements considering loads due to propeller ice interaction apply also for azimuthing (geared and podded) thrusters. However, ice loads due to ice impacts on the body of azimuthing thrusters are not covered by the present Section.

The loads given in 1.3.4 are total loads (unless otherwise stated) during ice interaction and shall be applied separately (unless otherwise stated) and are intended for component strength calculations only. The different loads given here shall be applied separately.

F_b is a force bending a propeller blade backwards when the propeller mills an ice block while rotating ahead.

F_f is a force bending a propeller blade forwards when a propeller interacts with an ice block while rotating ahead.

1.3.4.2 Ice class factors.

The Table 1.3.4.2 below lists the design ice thickness and ice strength index to be used for estimation of the propeller ice loads.

Table 1.3.4.2

Ice class	H_{ice} in m	S_{ice}	S_{qice}
PC1	4,0	1,2	1,15
PC2	3,5	1,1	1,15
PC3	3,0	1,1	1,15
PC4	2,5	1,1	1,15
PC5	2,0	1,1	1,15
PC6	1,75	1	1
PC7	1,5	1	1

where H_{ice} = ice thickness for machinery strength design;
 S_{ice} = ice strength index for blade ice force;
 S_{qice} = ice strength index for blade ice torque.

1.3.4.3 Design ice loads for open propeller.

1.3.4.3.1 Maximum backward blade force F_b , in kN:

when $D < D_{limit}$:

$$F_b = -27S_{ice}[nD]^{0,7}[EAR/Z]^{0,3}[D]^2; \quad (1.3.4.3.1-1)$$

when $D \geq D_{limit}$:

$$F_b = -23S_{ice}[nD]^{0,7}[EAR/Z]^{0,3}(H_{ice})^{1,4}[D]^2 \quad (1.3.4.3.1-2)$$

where $D_{limit} = 0,85(H_{ice})^{1,4}$;

n = nominal rotational speed (at MCR free running condition) for CP-propeller and 85 per cent of the nominal rotational speed (at MCR free running condition) for a FP-propeller (regardless driving engine type).

F_b shall be applied as a uniform pressure distribution to an area on the back (suction) side of the blade for the following load cases:

.1 load case 1: from 0,6R to the tip and from the blade leading edge to a value of 0,2 chord length;

.2 load case 2: a load equal to 50 per cent of the F_b shall be applied on the propeller tip area outside of 0,9R;

.3 load case 5: for reversible propellers a load equal to 60 per cent of the F_b shall be applied from 0,6R to the tip and from the blade trailing edge to a value of 0,2 chord length.

Refer to load cases 1, 2 and 5 in Table 1 of the Appendix.

1.3.4.3.2 Maximum forward blade force F_f , in kN:

when $D < D_{limit}$:

$$F_f = 250[EAR/Z][D]^2; \quad (1.3.4.3.2-1)$$

when $D \geq D_{limit}$:

$$F_f = 500 \frac{1}{(1 - \frac{d}{D})} H_{ice}[EAR/Z][D]^2 \quad (1.3.4.3.2-2)$$

where

$$D_{limit} = \frac{2}{(1 - \frac{d}{D})} H_{ice}; \quad (1.3.4.3.2-3)$$

d = propeller hub diameter, in m;

D = propeller diameter, in m;

EAR = expanded blade area ratio;

Z = number of propeller blades.

F_f shall be applied as a uniform pressure distribution to an area on the face (pressure) side of the blade for the following loads cases:

.1 load case 3: from $0,6R$ to the tip and from the blade leading edge to a value of $0,2$ chord length;

.2 load case 4: a load equal to 50 per cent of the F_f shall be applied on the propeller tip area outside of $0,9R$;

.3 load case 5: for reversible propellers a load equal to 60 per cent F_f shall be applied from $0,6R$ to the tip and from the blade trailing edge to a value of $0,2$ chord length.

Load cases 3, 4 and 5 — refer to Table 1 of the Appendix.

1.3.4.3.3 Maximum blade spindle torque Q_{Smax}

Spindle torque Q_{Smax} , in kNm, around the spindle axis of the blade fitting shall be calculated both for the load cases described in 1.3.4.3.1 and 1.3.4.3.2 for F_b and F_f . If these spindle torque values are less than the default value given below, the default minimum value shall be used. Default value:

$$Q_{Smax} = 0,25F_{c0,7} \quad (1.3.4.3.3)$$

where $c_{0,7}$ = length of the blade chord at $0,7R$ radius, in m;
 F is either F_b or F_f which ever has the greater absolute value.

1.3.4.3.4 Maximum propeller ice torque applied to the propeller Q_{max} , in kNm:

when $D < D_{limit}$:

$$Q_{max} = 105(1 - d/D)S_{qice}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^3; \quad (1.3.4.3.4-1)$$

when $D \geq D_{limit}$:

$$Q_{max} = 202(1 - d/D)S_{qice}H_{ice}^{1,1}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^{1,9} \quad (1.3.4.3.4-2)$$

where $D_{limit} = 1,8H_{ice}$;

S_{qice} = ice strength index for blade ice torque;

$P_{0,7}$ = propeller pitch at $0,7R$, in m;

$t_{0,7}$ = max thickness at $0,7R$, in m;

n is the rotational propeller speed, in rps, at bollard condition.

If not known, n shall be taken according to Table 1.3.4.3.4.

Table 1.3.4.3.4

Propeller type	n
CP propellers	n_n
FP propellers driven by turbine or electric motor	n_n
FP propellers driven by diesel engine	$0,85n_n$
where n_n = nominal rotational speed at MCR, free running condition.	

For CP propellers, propeller pitch $P_{0,7}$ shall correspond to MCR in bollard condition. If not known, $P_{0,7}$ shall be taken as $0,7P_{0,7n}$, where $P_{0,7n}$ is propeller pitch at MCR free running condition.

1.3.4.3.5 Maximum propeller ice thrust (applied to the shaft at the location of the propeller).

Maximum forward propeller ice thrust:

$$T_f = 1,1F_f; \quad (1.3.4.3.5-1)$$

Maximum backward propeller ice thrust:

$$T_b = 1,1F_b. \quad (1.3.4.3.5-2)$$

1.3.4.4 Design ice loads for ducted propeller.

1.3.4.4.1 Maximum backward blade force F_b :

where $D < D_{limit}$:

$$F_b = -9,5S_{ice}(EAR/Z)^{0,3}(nD)^{0,7}D^2; \quad (1.3.4.4.1-1)$$

where $D \geq D_{limit}$:

$$F_b = -66S_{ice}(EAR/Z)^{0,3}(nD)^{0,7}(H_{ice})^{1,4}D^{0,6} \quad (1.3.4.4.1-2)$$

where $D_{limit} = 4H_{ice}$;

n shall be taken as in 1.3.4.3.1.

F_b shall be applied as a uniform pressure distribution to an area on the back side for the following load cases (refer to Table 2 of the Appendix):

.1 load case 1: on the back of the blade from $0,6R$ to the tip and from the blade leading edge to a value of $0,2$ chord length;

.2 load case 5: for reversible rotation propellers a load equal to 60 per cent of F_b is applied on the blade face from $0,6R$ to the tip and from the blade trailing edge to a value of $0,2$ chord length.

1.3.4.4.2 Maximum forward blade force F_f , in kN:

when $D < D_{limit}$:

$$F_f = 250(EAR/Z)D^2; \quad (1.3.4.4.2-1)$$

when $D \geq D_{limit}$:

$$F_f = 500 \frac{1}{(1 - \frac{d}{D})} H_{ice} [EAR/Z] [D]^2 \quad (1.3.4.4.2-2)$$

$$\text{where } D_{limit} = \frac{2}{(1 - \frac{d}{D})} H_{ice}, \text{ in m.} \quad (1.3.4.4.2-3)$$

F_f shall be applied as a uniform pressure distribution to an area on the face (pressure) side for the following load case (refer to Table 2 of the Appendix):

.1 load case 3: on the blade face from $0,6R$ to the tip and from the blade leading edge to a value of $0,5$ chord length;

.2 load case 5: a load equal to 60 per cent F_f shall be applied from $0,6R$ to the tip and from the blade leading edge to a value of $0,2$ chord length.

1.3.4.4.3 Maximum propeller ice torque applied to the propeller Q_{max} , in kNm, is the maximum torque on a propeller due to ice-propeller interaction:

when $D \leq D_{limit}$:

$$Q_{max} = 74(1 - d/D)S_{qice}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^3; \quad (1.3.4.4.3-1)$$

when $D \geq D_{limit}$:

$$Q_{max} = 141(1 - d/D)S_{qice}H_{ice}^{1,1}(P_{0,7}/D)^{0,16}(t_{0,7}/D)^{0,6}(nD)^{0,17}D^{1,9} \quad (1.3.4.4.3-2)$$

where $D_{limit} = 1,8H_{ice}$, in m;

n = rotational propeller speed, in rps, at bollard condition.

If not known, n shall be taken according to Table 1.3.4.4.3.

Таблица 1.3.4.4.3

Propeller type	n
CP propellers	n_n
FP propellers driven by turbine or electric motor	n_n
FP propellers driven by diesel engine	$0,85n_n$
where n_n = nominal rotational speed at MCR, free running condition.	

For CP propellers, propeller pitch $P_{0,7}$ shall correspond to MCR in bollard condition. If not known, $P_{0,7}$ shall be taken as $0,7P_{0,7n}$, where $P_{0,7n}$ is propeller pitch at MCR free running condition.

1.3.4.4.4 Maximum blade spindle torque for CP-mechanism design Q_{smax} .

Spindle torque Q_{smax} , in kNm, around the spindle axis of the blade fitting shall be calculated for the load case described in 1.3.4.1. If these spindle torque values are less than the default value given below, the default value shall be used.

Default value:

$$Q_{smax} = 0,25Fc_{0,7} \quad (1.3.4.4.4)$$

where $c_{0,7}$ = length of the blade section at $0,7R$ radius;
 F = either F_b or F_f whichever has the greater absolute value.

1.3.4.4.5 Maximum propeller ice thrust (applied to the shaft at the location of the propeller).

Maximum forward propeller ice thrust:

$$T_f = 1,1F_f. \quad (1.3.4.4.5-1)$$

Maximum backward propeller ice thrust:

$$T_b = 1,1F_b. \quad (1.3.4.4.5-2)$$

1.3.4.5 Reserved.

1.3.4.6 Design loads on propulsion line.

1.3.4.6.1 Torque.

The propeller ice torque excitation for shaft line dynamic analysis shall be described by a sequence of blade impacts which are of half sine shape and occur at the blade. The torque due to a single blade ice impact as a function of the propeller rotation angle is then:

$$Q(\varphi) = C_q Q_{max} \sin(\varphi(180/\alpha_i)) \text{ when } \varphi = 0 \dots \alpha_i;$$

$$Q(\varphi) = 0 \text{ when } \varphi = \alpha_i \dots 360. \quad (1.3.4.6.1-1)$$

C_q and α_i parameters are given in Table 1.3.4.6.1.

Table 1.3.4.6.1

Torque excitation	Propeller-ice interaction	C_q	α_i
Case 1	Single ice block	0,5	45
Case 2	Single ice block	0,75	90
Case 3	Single ice block	1,0	135
Case 4	Two ice blocks with 45 degree phase in rotation angle	0,5	45

The total ice torque is obtained by summing the torque of single blades taking into account the phase shift 360 deg/Z. The number of propeller revolutions during a milling sequence shall be determined by the formula

$$N_Q = 2H_{ice}. \quad (1.3.4.6.1-2)$$

The number of impacts is ZN_Q (refer to Fig. 1 in the Appendix).

Milling torque sequence duration is not valid for pulling bow propellers, which are subject to special consideration by the Register in each particular case.

The response torque at any shaft component shall be analysed considering excitation torque $Q(\varphi)$ at the propeller, actual engine torque Q_e and mass elastic system.

Q_e = actual maximum engine torque at considered speed.

Design torque along propeller shaft line.

The design torque Q_r of the shaft component shall be determined by means of torsional vibration analysis of the propulsion line. Calculations shall be carried out for all excitation cases given above and the response shall be applied on top of the mean hydrodynamic torque in bollard condition at considered propeller rotational speed.

1.3.4.6.2 Maximum response thrust (maximum thrust along the propeller shaft line).

Maximum thrust along the propeller shaft line shall be calculated with the formulae below. The factors 2,2 and 1,5 take into account the dynamic magnification due to axial vibration. Alternatively the propeller thrust magnification factor may be calculated by dynamic analysis.

Maximum shaft thrust forwards, in kN:

$$T_r = T_n + 2,2T_f. \quad (1.3.4.6.2-1)$$

Maximum shaft thrust backwards, in kN:

$$T_r = 1,5T_b \quad (1.3.4.6.2-2)$$

where T_n = propeller bollard thrust, in kN;

T_f = maximum forward propeller ice thrust, in kN;

T_b = maximum backward propeller ice thrust, in kN.

If hydrodynamic bollard thrust T_n is not known, T_n shall be taken according to Table 1.3.4.6.2.

Table 1.3.4.6.2

Propeller type	T_n
CP propellers (open)	1,25T
CP propellers (ducted)	1,1T
FP propellers driven by turbine or electric motor	T
FP propellers driven by diesel engine (open)	0,85T
FP propellers driven by diesel engine (ducted)	0,75T
where T = nominal propeller thrust at MCR at free running open water conditions.	

1.3.4.6.3 Blade failure load for both open and nozzle propeller.

The force is acting at $0,8R$ in the weakest direction of the blade and at a spindle arm of $2/3$ of the distance of

axis of blade rotation of leading and trailing edge which ever is the greatest.

The blade failure load F_{ex} , in kN, is determined by formula

$$F_{ex} = \frac{0,3ct^2\sigma_{ref}}{0,8D-2r} \cdot 10^3 \quad (1.3.4.6.3)$$

where $\sigma_{ref} = 0,6\sigma_{0,2} + 0,4\sigma_u$;
 σ_u and $\sigma_{0,2}$ are representative values for the blade material;
 c , t and r are respectively the actual chord length, thickness and radius of the cylindrical root section of the blade at the weakest section outside root fillet, and typically will be at the termination of the fillet into the blade profile.

1.3.5 Design.

1.3.5.1 Design principle.

The strength of the propulsion line shall be designed: for maximum loads in 1.3.4;

such that the plastic bending of a propeller blade shall not cause damages in other propulsion line components; with sufficient fatigue strength.

1.3.5.2 Azimuthing main propulsors.

In addition to the above requirements special consideration shall be given to the loading cases which are extraordinary for propulsion units when compared with conventional propellers. Estimation of the loading cases shall reflect the operational realities of the ship and the thrusters. In this respect, for example, the loads caused by impacts of ice blocks on the propeller hub of a pulling propeller shall be considered. Also loads due to thrusters operating in an oblique angle to the flow shall be considered. The steering mechanism, the fitting of the unit and the body of the thruster shall be designed to withstand the loss of a blade without damage. The plastic bending of a blade shall be considered in the propeller blade position, which causes the maximum load on the studied component.

Azimuth thrusters shall also be designed for estimated loads due to thruster body/ice interaction as per 1.2.15.

1.3.5.3 Blade design.

1.3.5.3.1 Maximum blade stresses.

Blade stresses shall be calculated using the backward and forward loads given in section 1.3.4.3 and 1.3.4.4. The stresses shall be calculated with recognised and well-documented FE-analysis or other acceptable alternative method.

The stresses on the blade shall not exceed the allowable stresses σ_{all} for the blade material given below.

Calculated blade stress for maximum ice load shall comply with the following:

$$\sigma_{calc} < \sigma_{all} = \sigma_{ref}/S \quad (1.3.5.3.1-1)$$

where $S = 1,5$;

σ_{ref} = reference stress, defined as:

$$\sigma_{ref} = 0,7\sigma_u; \text{ or} \quad (1.3.5.3.1-2)$$

$$\sigma_{ref} = 0,6\sigma_{0,2} + 0,4\sigma_u, \text{ whichever is less,} \quad (1.3.5.3.1-3)$$

where σ_u and $\sigma_{0,2}$ = representative values for the blade material.

1.3.5.3.2 Blade edge thickness.

The blade edge thicknesses t_{edge} and t_{tip} thickness t_{tip} shall be greater than t_{edge} determined by formula

$$t_{edge} \geq x S S_{ice} \sqrt{3 p_{ice} / \sigma_{ref}} \quad (1.3.5.3.2)$$

where x = distance from the blade edge measured along the cylindrical sections from the edge and shall be 2,5 per cent of chord length, however not to be taken greater than 45 mm. In the tip area (above 0,975R) x shall be taken as 2,5 per cent of 0,975R section length and shall be measured perpendicularly to the edge, however not to be taken greater than 45 mm;

S = safety factor;

$S = 2,5$ for trailing edges;

$S = 3,5$ for leading edges;

$S = 5$ for tip;

S_{ice} = according to 1.3.4.2;

p_{ice} = ice pressure;

$p_{ice} = 16$ MPa for leading edge and tip thickness;

σ_{ref} = according to 1.3.5.3.1.

The requirement for edge thickness shall be applied for leading edge and in case of reversible rotation open propellers also for trailing edge. Tip thickness refers to the maximum measured thickness in the tip area above 0,975R. The edge thickness in the area between position of maximum tip thickness and edge thickness at 0,975R shall be interpolated between edge and tip thickness value and smoothly distributed.

1.3.5.3.3 to 1.3.5.4.2 Reserved.

1.3.5.5 Reserved.

1.3.5.6 Prime movers.

1.3.5.6.1 The main engine shall be capable of being started and running the propeller with the CP in full pitch.

1.3.5.6.2 Provisions shall be made for heating arrangements to ensure ready starting of the cold emergency power units at an ambient temperature applicable to the polar class of the ship.

1.3.5.6.3 Emergency power units shall be equipped with starting devices with a stored energy capability of at least three consecutive starts at the design temperature in 1.3.5.6.2 above. The source of stored energy shall be protected to preclude critical depletion by the automatic starting system, unless a second independent means of starting is provided. A second source of energy shall be provided for an additional three starts within 30 min, unless manual starting can be demonstrated to be effective.

1.3.6 Machinery fastening loading accelerations.

1.3.6.1 Essential equipment and main propulsion machinery supports shall be suitable for the accelerations as indicated in as follows. Accelerations shall be considered acting independently.

1.3.6.2 Longitudinal impact accelerations a_l .

Maximum longitudinal impact acceleration at any point along the hull girder, in m/s^2 , is determined by the formula

$$a_l = (F_{IB}/A) \{ [1,1 \tan(\gamma + \varphi)] + [7H/L] \} \quad (1.3.6.2)$$

where φ = maximum friction angle between steel and ice, normally taken as 10 deg.;

γ = bow stem angle at waterline, in deg.;

A = displacement;
 L = length between perpendiculars, in m;
 H = distance from the waterline to the point being considered, in m;
 F_{IB} = vertical impact force, defined in 1.2.13.2.1;
 F_i = total force normal to shell plating in the bow area due to oblique ice impact, defined in 1.2.3.2.1.

1.3.6.3 Vertical acceleration a_v .

Combined vertical impact acceleration at any point along the hull girder, in m/s^2 , is determined by the formula

$$a_v = 2,5(F_{IB}/A)F_x \quad (1.3.6.3)$$

where $F_x = 1,3$ at FP;
 $F_x = 0,2$ at midships;
 $F_x = 0,4$ at AP;
 $F_x = 1,3$ at AP for ships conducting ice breaking astern.

Intermediate values to be interpolated linearly.

1.3.6.4 Transverse impact acceleration a_t .

Combined transverse impact acceleration at any point along hull girder, in m/s^2 , is determined by the formula

$$a_t = 3F_t F_x / \Delta \quad (1.3.6.4)$$

where $F_x = 1,5$ at FP;
 $F_x = 0,25$ at midships;
 $F_x = 0,5$ at AP;
 $F_x = 1,5$ at AP for ships conducting ice breaking astern.

Intermediate values to be interpolated linearly.

1.3.7 Auxiliary systems.

1.3.7.1 Machinery shall be protected from the harmful effects of ingestion or accumulation of ice or snow. Where continuous operation is necessary, means shall be provided to purge the system of accumulated ice or snow.

1.3.7.2 Means shall be provided to prevent damage due to freezing, to tanks containing liquids.

1.3.7.3 Vent pipes, intake and discharge pipes and associated systems shall be designed to prevent blockage due to freezing or ice and snow accumulation.

1.3.8 Sea inlets and cooling water systems.

1.3.8.1 Cooling water systems for machinery that are essential for the propulsion and safety of the vessel, including sea chests inlets, shall be designed for the environmental conditions applicable to the ice class.

1.3.8.2 At least two sea chests shall be arranged as ice boxes for class **PC1** to **PC5** ships. The calculated volume for each of the ice boxes shall be at least 1 m^3 for every 750 kW of the total installed power. For **PC6** and

PC7 there shall be at least one icebox located preferably near centre line.

1.3.8.3 Ice boxes shall be designed for an effective separation of ice and venting of air.

1.3.8.4 Sea inlet valves shall be secured directly to the ice boxes. The valve shall be a full bore type.

1.3.8.5 Ice boxes and sea chests shall have vent pipes and shall have shut off valves connected direct to the shell.

1.3.8.6 Means shall be provided to prevent freezing of sea chests, ice boxes, ship side valves and fittings above the load waterline.

1.3.8.7 Efficient means shall be provided to re-circulate cooling seawater to the ice box. Total sectional area of the circulating pipes shall not be less than the area of the cooling water discharge pipe.

1.3.8.8 Detachable gratings or manholes shall be provided for ice boxes. Manholes shall be located above the deepest load line. Access shall be provided to the ice box from above.

1.3.8.9 Openings in ship sides for ice boxes shall be fitted with gratings, or holes or slots in shell plates. The net area through these openings shall be not less than 5 times the area of the inlet pipe. The diameter of holes and width of slot in shell plating shall be not less than 20 mm. Gratings of the ice boxes shall be provided with a means of clearing. Clearing pipes shall be provided with screw-down type non return valves.

1.3.9 Ballast tanks.

1.3.9.1 Efficient means shall be provided to prevent freezing in fore and after peak tanks and wing tanks located above the water line and where otherwise found necessary.

1.3.10 Ventilation system.

1.3.10.1 The air intakes for machinery and accommodation ventilation shall be located on both sides of the ship.

1.3.10.2 Accommodation and ventilation air intakes shall be provided with means of heating.

1.3.10.3 The temperature of inlet air provided to machinery from the air intakes shall be suitable for the safe operation of the machinery.

1.3.11 Reserved.

1.3.12 Alternative design.

1.3.12.1 As an alternative — a comprehensive design study may be submitted and may be requested to be validated by an agreed test programme.

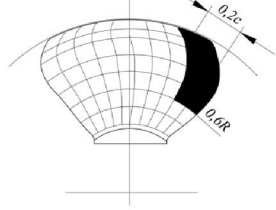
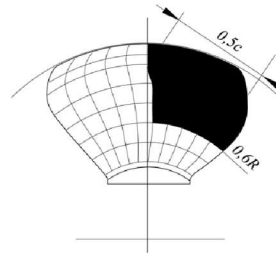
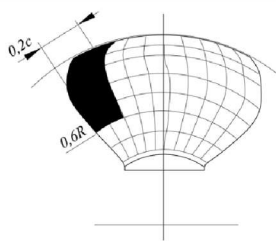
APPENDIX

Table 1

Load cases for open propeller

	Force	Loaded area	Right handed propeller blade seen from back
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 2	50 per cent of F_b	Uniform pressure applied on the back of the blade (suction side) on the propeller tip area outside of $0,9R$	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 4	50 per cent of F_f	Uniform pressure applied on propeller face (pressure side) on the propeller tip area outside of $0,9R$	
Load case 5	60 per cent of F_f or F_b which one is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

Table 2

Load cases for ducted propeller			
	Force	Loaded area	Right handed propeller blade seen from back
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,5$ times the chord length	
Load case 5	60 per cent of F_f or F_b which one is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

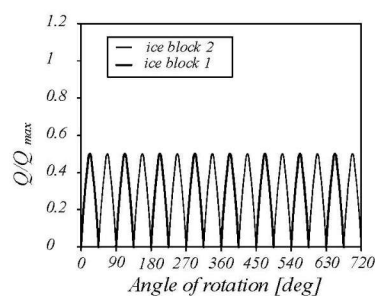
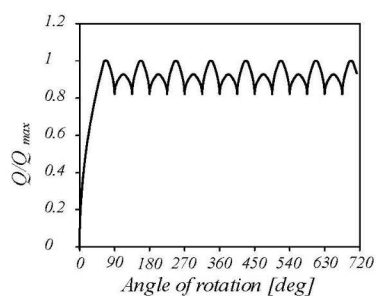
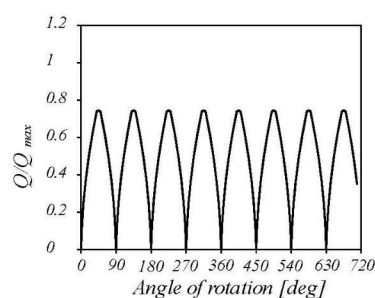
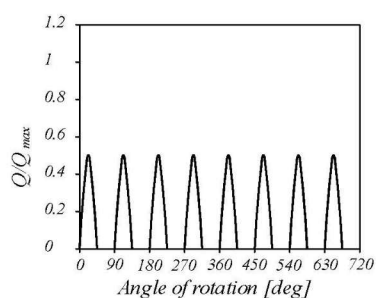


Fig. 1

The shape of the propeller ice torque excitation for 45, 90, 135 degrees single blade impact sequences and 45 degrees double blade impact sequence (two ice pieces) on a four bladed propeller

2 TECHNICAL REQUIREMENTS FOR ESCORT TUGS

2.1 GENERAL

2.1.1 Scope of application.

2.1.1.1 The technical requirements for escort tugs apply to tugs intended for escort service. These requirements are additional to the requirements of Parts I to XV of the Rules.

2.1.1.2 Tugs complying with the requirements of the present Section may be assigned the descriptive notation **Escort tug** added to the character of classification.

2.1.2 Definitions and explanations.

For the purpose of the present Section the following definitions and explanations have been adopted.

Manoeuvring time means a minimum manoeuvring time, in s, from maintained oblique position of the tug (from the centerline of the assisted ship) giving the maximum transverse steering force on one side of the assisted ship to mirror position on the other side.

Maximum steering pull of the tug means the maximum transverse steering force, in t, exerted by the tug on the stern of the assisted ship at the escort test speed of 8 and/or 10 knots.

Escort test speed means the speed, in knots, of the assisted ship during full scale trials.

Assisted ship means the ship being escorted by the escort tug.

Full scale trials mean sea trials of the escort tug to determine escort characteristics.

Escort service means steering, braking and otherwise controlling the assisted ship.

Escort characteristics:

maximum steering pull of the tug F_s , in t, at the escort test speed V , in knots, (refer to Fig. 2.1.2);

manoeuvring time t , in s.

Escort tug means a tug which in addition to towing and ship handling operations is intended for escort services.

2.1.3 Technical documentation.

2.1.3.1 Technical documentation to be submitted to the Register for approval shall include the following:

.1 towing arrangement plan required for escort service including towing line path and minimum breaking strength of towing line components and strength of appropriate structures;

.2 preliminary calculation of maximum steering pull of the tug at the escort test speed of 8 and/or 10 knots including propulsion components of the escort tug for balancing of oblique angular position of the tug;

.3 preliminary tug stability calculations for escorting service;

.4 plan of full scale trials.

2.2 TECHNICAL REQUIREMENTS

2.2.1 Arrangement and design.

2.2.1.1 A bulwark shall be fitted all around the exposed weather deck.

2.2.1.2 The towing winch intended for escort service shall be fitted with a load reducing system in order to prevent overload caused by dynamic oscillation in the towing line, and shall be capable of paying out the towing line if the pull exceeds 50 per cent of the breaking strength of the towing line.

2.2.1.3 The towing line components shall have a minimum breaking strength of at least 2,2 times the maximum towing pull as measured during the full scale trials (refer to 2.3).

2.2.1.4 In case of escort service of oil tankers and/or oil recovery vessels, supply vessels, ships intended for the carriage of explosives and inflammable cargoes, the requirements of 11.1.3, Part VIII "Systems and Piping" shall be complied with.

2.2.2 Stability.

2.2.2.1 In addition to the requirements for tugs set forth in 3.7, Part IV "Stability", stability of the escort tug shall comply with the criteria specified in 2.2.2.1.1 to 2.2.2.1.5.

2.2.2.1.1 The ratio between the righting and heeling areas between equilibrium and 20° angle of heel obtained

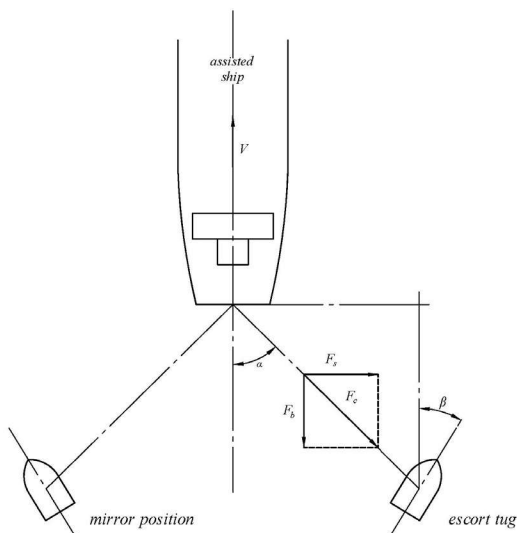


Fig. 2.1.2 Typical working mode of the escort tug
 F_s = steering pull; F_b = braking force; F_t = towing line tension;
 α = towing line angle; β = oblique angle;
 V = speed of the assisted ship

when the maximum steering pull F_s is applied from the tug (refer to Fig. 2.1.2) shall be not less than 1,25.

2.2.2.1.2 The ratio between the righting area and the heeling area due to the maximum steering pull between 0° heel and the angle of flooding or 40° angle of heel, whichever is less, shall be not less than 1,4.

2.2.2.1.3 The angle of heel of the escort tug under the effect of maximum working heeling moment, due to the towing line jerk under rolling shall not exceed the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

The following requirement shall be complied with (refer to Fig. 2.2.2.1.3):

$$K_3 = \sqrt{\frac{b+c}{a+c}} \geq 1,0 \quad (2.2.2.1.3-1)$$

where a = the area formed by the righting lever curve, the straight line corresponding to the lever $l+l_h$ and the angle of heel $\theta_1-\theta_{2r}$;
 b = the area formed from above by the righting lever curve, from below — by the straight line corresponding to the lever $l+l_h$ and from the right — by the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less;
 c = the area formed from the left by the righting lever curve, from above — by the straight line corresponding to the lever $l+l_h$, from the right — by the angle corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

When determining the angle of flooding θ_f the definition of the angle of flooding given in 1.2, Part IV "Stability" shall be considered.

The heeling lever l_h characterizing the effect of towing line jerk, in m, is determined by the formula

$$l_h = 0,2 \left(1 + 2 \frac{d}{B} \right) \frac{b^2}{(1+c^2)(1+c^2+b^2)} \frac{57,3}{(\theta_{2r} - \theta_1 + \theta_{\lim})} \quad (2.2.2.1.3-2)$$

where d, B = the draft and breadth of the tug respectively;
 c, b are calculated in accordance with 3.7.2.2, Part IV "Stability";
 $\theta_{\lim} = \theta_{\max}$ or θ_f , whichever is less.

2.2.2.1.4 The angle of dynamic heel of the tug which may occur during escort service in case of sudden failure of the main propulsion plant shall not exceed the angle

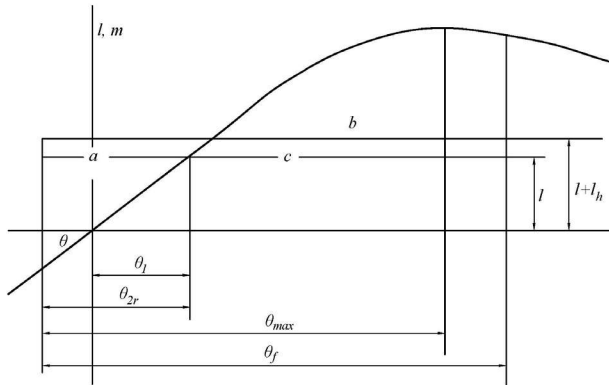


Fig. 2.2.2.1.3

corresponding to the maximum of the righting lever curve θ_{\max} or the angle of flooding θ_f , whichever is less.

2.2.2.1.5 At the design stage, the value of the maximum steering pull and the angle of heel under its effect may be determined based on the model tests results or by means of calculations. On completion of the ship's construction, the values of the maximum steering pull and the maximum possible angle of heel of the tug shall be ascertained based on the results of full scale trials or numerical simulation carried out in accordance with the procedure approved by the Register.

2.3 FULL SCALE TRIALS

2.3.1 Plan of full scale trials.

2.3.1.1 Prior to the full scale trials the plan of the trials, the approved Stability Booklet, as well as preliminary calculations of the ship's escort characteristics and the tug's stability during escort service shall be submitted to surveyor to the Register.

2.3.1.2 The plan of full scale trials shall stipulate determination of the tug's maximum transverse steering force at the speed of the assisted ship of 8 and/or 10 knots, the maximum angle of static heel at the specified modes, as well as the tug's manoeuvring time (refer to Fig. 2.1.2).

2.3.1.3 The plan shall include a list of measuring instruments, description of mandatory manoeuvres, a towing arrangement scheme for expected escort modes, design loads of strong points of the tug, as well as data of the safe working load of the strong points of the assisted ship.

2.3.2 Procedure of trials.

2.3.2.1 Full scale trials shall be carried out on:

.1 the first ship out of the series of ships, then every fifth ship of the series (i.e. sixth, eleventh, etc.) provided their propulsion plant is identical;

.2 every ship of non-series construction.

2.3.2.2 The trials shall be carried out in favourable weather (recommended limitation of wind force is 10 m/s, sea state 2), with the operating load of the tug equal to 50 — 10 per cent of provisions. Current velocity in the area of the trials (if any) shall be measured both upstream and down stream.

2.3.2.3 Displacement or powered of the assisted ship shall be sufficient to maintain the heading and speed with the help of the autopilot during the necessary tug manoeuvring.

2.3.2.4 The following data shall be recorded continuously in real time mode during trials for later analysis:

.1 position of the assisted ship in relation to the escort tug;

.2 towing line tension;

.3 escort test speed;

.4 angle of the tug heel during escort service;

.5 length and angle of the towing line from the centerline of the assisted ship;

.6 manoeuvring time from maintained oblique position of the tug on one side of the assisted ship to mirror position on the other side at the maximum tension value of towing line and the maximum towing line angle from the centerline of the assisted ship (but not more than 60°);

.7 angle of heel due to sudden loss of thrust.

2.4 REPORTING

2.4.1 Report in tabular form on the results of the tug's trials to determine the escort characteristics and including records of the parameters measured in real time mode shall be agreed with the surveyor to the Register attending the trials and be forwarded to the Register

Head Office for consideration. The Report shall contain calculation of the steering pull value taking into account the time of the tug's transfer to the mirror position. The Report shall be accompanied with the escort tug's stability calculation based on results of full scale trials.

2.4.2 Results of full scale trials are documented in the Act issued by surveyor to the Register.

2.4.3 Upon satisfactory results of full scale trials and consideration of stability calculation specified in 2.4.1, in the Classification Certificate issued for the tug the descriptive notation **Escort tug** is added to the character of classification, and in the column "Other characteristics" the following entry shall be made: "During escort service the maximum steering pull is equal to t, with the escort test speed 8 (or 10) knots and the minimum manoeuvring times". In case the measurements were taken at two values of escort test speed (8 and 10 knots), the data of both speeds shall be recorded.

3 REQUIREMENTS FOR THE EQUIPMENT OF SHIPS IN COMPLIANCE WITH THE DISTINGUISHING MARKS ECO AND ECO-S IN THE CLASS NOTATION

3.1 GENERAL

3.1.1 Scope of application.

The requirements for the equipment of ships in compliance with the distinguishing marks ECO and ECO-S in the class notation have been developed taking into account the following international instruments as amended:

- .1 Annexes I, II, IV, V, VI to MARPOL 73/78 and IMO resolutions specified in Table 3.2.2;
- .2 provisions of the International Convention on the Control of Harmful Anti-Fouling Systems on Ships, 2001;
- .3 Code on Intact Stability for All Types of Ships Covered by IMO Instruments (IMO resolution A.749(18));
- .4 provisions of IACS Unified Requirement L5 "Onboard computers for stability calculations" (Rev. 1, Feb. 2005);
- .5 IMO Guidelines on Ship Recycling, 2004 (IMO resolution A.962(23));
- .6 provisions of Directive 99/32/EU with amendments to Directive 2005/33/EU;
- .7 provisions of the 1987 Montreal Protocol on Substances that Deplete the Ozone Layer.

The requirements of the present Section are applied during survey of ships for assigning the distinguishing marks ECO and ECO-S in the class notation (refer to 3.2.1).

3.1.2 Terms. Definitions.

Noxious liquid substance (NLS) means any substance indicated in the Pollution Category column of Chapters 17 and 18 of the International Bulk Chemical Code (IBC Code).

Emission to air means any emission to air from ships subject to control by Annex VI to MARPOL 73/78.

Attained Energy Efficiency Design Index (Attained EEDI) means the EEDI value achieved by an individual ship in compliance with regulation 20 of chapter 4 in Annex VI to MARPOL 73/78.

Segregated ballast means the ballast water introduced into a tank which is completely separated from the cargo oil and fuel oil system and which is permanently allocated to the carriage of ballast or to the carriage of ballast or cargoes other than oil or noxious liquid substances.

Bilge water means water accumulated in the bilge of ship's machinery spaces which may be contaminated with oil.

Garbage means garbage generated during normal operation of the ship, sorted, stored and disposed of/incinerated in accordance with the provisions of Annex V to MARPOL 73/78.

NLS tanker means a ship constructed or adapted to carry a cargo of noxious liquid substances in bulk and includes an "oil tanker" as defined in Annex I to MARPOL 73/78 when certified to carry a cargo or part cargo of noxious liquid substances.

Oil residues mean oil residues generated during normal operation of the ship and include the following:

- used lubricating and hydraulic oils;
- fuel oil and lubricating oil leaked from the ship's machinery and systems;
- sludge from fuel oil and lubricating oil separators, from bilge separators.

Oil means petroleum in any form including crude oil, fuel oil, sludge, oil refuse and refined products (other than those petrochemicals which are subject to the provisions of Annex II to MARPOL 73/78) and, without limiting the generality of the foregoing, includes the substances listed in appendix I to Annex I to MARPOL 73/78.

New ship (for the purpose of application of the requirements for energy efficiency) means a ship:

- for which the building contract is placed on or after 1 January 2013; or
- in the absence of a building contract, the keel of which is laid or which is at a similar stage of construction on or after 1 July 2013; or
- the delivery of which is on or after 1 July 2015.

Passenger ship means a ship that carries more than 12 passengers.

Anti-fouling systems mean coatings, paints, surface treatment and devices that are used on a ship to control or prevent attachment of unwanted organisms.

Fire-fighting systems mean shipboard fixed fire-fighting systems containing fire-fighting substances with different ozone depleting potential (ODP) and global warming potential (GWP) values.

SO_x Emission Control Areas mean areas where emission of sulphur oxides is limited as defined in Annex VI to MARPOL 73/78 and Directive 99/32/EU, as amended.

Discharge to sea means any discharge from ships to sea of harmful substances or effluents containing such substances including any escape, disposal, spilling, leaking, pumping, emitting or emptying.

Bilge separator means any combination of a separator, filter or coalescer, and also a single unit designed to produce an effluent with oil content not exceeding 15 ppm or 5 ppm (whatever is applicable).

Bilge alarm means a device giving off a signal whenever the oil content in the effluent exceeds 15 ppm or 5 ppm (whatever is applicable).

Ballast water system means a system comprising tanks for ballast water with associated piping, pumps and ballast water treatment system, where provided.

Sewage system means a system comprising the following equipment:

- sewage holding tank with associated piping; or
- sewage treatment plant and sewage holding tank;
- discharge pipeline with pumps and standard discharge connectors.

Sewage means sewage generated during normal operation of the ship and includes drainage as defined in Annex IV to MARPOL 73/78.

Required Energy Efficiency Design Index (Required EEDI) means the maximum value of Attained EEDI that is allowed by regulation 21 of chapter 4 in Annex VI to MARPOL 73/78 for the specific ship type and size.

Chemical tanker means a ship constructed or adapted for the carriage in bulk of any liquid product listed in Chapter 17 of the IBC Code.

Sanitary and domestic waste waters mean drainage from wash basins, showers, laundries, wash tubes and scuppers, drainage from sinks and equipment of galleys and spaces annexed to galleys.

Refrigeration systems means shipboard systems (cargo refrigeration plants, air conditioning and refrigeration systems) containing refrigerants with different ozone depleting potential (ODP) and global warming potential (GWP) values.

3.2 CLASSIFICATION

3.2.1 Application.

The requirements of the present Section apply to the equipment and systems for prevention of pollution from emissions to air and discharges to sea and are aimed at prevention of environmental pollution in case of emergency.

Ships complying with the requirements of the present Section may be assigned the following distinguishing marks in the class notation:

ECO — the distinguishing mark in the class notation, which identifies compliance with the basic requirements for controlling and limiting operational emissions and discharges as well as requirements for prevention of oil and NLS spills during cargo operations and bunkering (the requirements are specified in 3.5);

ECO-S — the distinguishing mark in the class notation, which identifies compliance with more stringent requirements than those for assignment of the distinguishing mark **ECO** in the class notation (the requirements are specified in 3.6).

It is recommended to assign the above distinguishing marks in the class notation to the following ships:

ECO — to newbuildings and existing ships;

ECO-S — to newbuildings, existing passenger and coastal ships.

3.2.2 Requirements for ships with the distinguishing marks ECO and ECO-S in the class notation.

Table 3.2.2

Requirements	Distinguishing marks in the class notation	
	ECO	ECO-S
The following requirements shall be met on ships regarding prevention of air pollution:		
3.5.2.2 Prevention of pollution by emission from marine diesel engines	×	×
3.6.2.2 Prevention of pollution by emission from marine diesel engines	—	×
3.5.2.3 Prevention of pollution by emission from boilers and inert gas generators	×	×
3.6.2.3 Prevention of pollution by emission from boilers and inert gas generators	—	×
3.5.2.4 Prevention of pollution by refrigerant emission	×	×
3.6.2.4 Prevention of pollution by refrigerant emission	—	×
3.5.2.5 Prevention of pollution by fire extinguishing media emission	×	×
3.6.2.5 Prevention of pollution by fire extinguishing media emission	—	×
3.5.2.6 and 3.6.2.6 Prevention of pollution by volatile organic compounds emission	×	×
3.5.2.7 and 3.6.2.7 Prevention of pollution by emissions from shipboard incinerators.	×	×
3.5.2.8 Energy efficiency of ship	×	×
3.6.2.8 Energy efficiency of ship	×	×
The following requirements shall be met on ships regarding prevention of pollution of the marine environment:		
3.5.3.2 Discharge of cargo residues.	×	×
3.6.3.2 Discharge of cargo residues.	—	×
3.5.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.	×	×
3.6.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.	—	×
3.5.3.5 Prevention of pollution at oil contaminated water discharge	×	×
3.6.3.5 Prevention of pollution at oil contaminated water discharge	—	×
3.5.3.6 Prevention of pollution by garbage	×	×
3.6.3.6 Prevention of pollution by garbage	—	×
3.5.3.7 Prevention of pollution by sewage	×	×
3.6.3.7 Prevention of pollution by sewage	—	×
3.5.3.8 and 3.6.3.8 Control of harmful anti-fouling systems	×	×
3.5.3.9 and 3.6.3.9 Prevention of lubricating oil and hydraulic oil leakages into seawater	×	×
3.5.3.10 Prevention of pollution in case of the hull damage	×	×
3.6.3.10 Prevention of pollution in case of the hull damage	—	×
The following requirements shall be met on ships regarding prevention of pollution at ship recycling:		
3.5.4 and 3.6.5 Prevention of pollution at ship recycling	×	×

3.2.3 Any ship shall have AUT1 or AUT2 distinguishing automation mark of the machinery installation in the class notation.

3.3 APPLICATION OF INTERNATIONAL INSTRUMENTS' REQUIREMENTS

3.3.1 The requirements of the present Section are based on international instruments, the main of which are specified in 3.1. At the same time, some provisions of the requirements of the present Section are more stringent than the requirements of the relevant international instruments.

3.3.2 Required compliance of the ship's systems and equipment with international instruments.

Table 3.3.2

Ship's systems and equipment	International instrument
15 ppm bilge separators	IMO resolution MEPC.107(49)
15 ppm bilge alarms	IMO resolution MEPC.107(49)
Oil discharge monitoring and control systems	IMO resolution MEPC.108(49), as amended
Oil/water interface detectors	IMO resolution MEPC.5(XIII)
Shipboard incinerators	Regulation 16 of Annex VI to MARPOL 73/78, IMO resolution MEPC.76(40) or MEPC.244(66)
Sewage treatment plants	IMO resolution MEPC.159(55) or MEPC.227(64)
Cargo vapour collection systems of oil tankers	Regulation 15 of Annex VI to MARPOL 73/78, MSC/CIRC.585
Marine diesel engines	Regulation 13 of Annex VI to MARPOL 73/78, NO _x Technical Code
Exhaust gas cleaning systems to reduce the emission of sulphur oxides (SO _x)	Regulation 14 of Annex VI to MARPOL 73/78, IMO resolution MEPC.259(68).

3.3.3 International regulations and standards for use of fuel oil on ships, bunkering, sampling and testing of fuel oil.

Table 3.3.3

Required processes, specifications	International instrument
Sampling of fuel oil	IMO resolution MEPC.182(59), GOST 2517-85
Standard marine fuel oil	ISO 8217
Bunkering of ships	Regulation 18 of Annex VI to MARPOL 73/78
Fuel oil sulphur content test	ISO 8754

3.4 CERTIFICATES AND TECHNICAL DOCUMENTATION REQUIRED FOR ASSIGNING THE DISTINGUISHING MARKS ECO OR ECO-S IN THE CLASS NOTATION

3.4.1 Air Pollution Prevention Certificates:

.1 International Air Pollution Prevention Certificate (IAPP) with Supplement issued by any Administration or under the authorization thereof; or

International Air Pollution Prevention Certificate (form 2.4.6) with Supplement (form 2.4.23), issued in compliance with 1.11, Part III "Survey of Ships in Compliance with International Conventions, Codes, Resolutions and Rules for the Equipment of Sea-Going Ships" of the Guidelines on Technical Supervision of Ships in Service; or

Pollution From Ships Prevention Certificate (form 2.4.18rf).

.2 Engine International Air Pollution Prevention Certificate (EIAPP), issued by any Administration or under the authorization thereof; or

Engine International Air Pollution Prevention Certificate (form 2.4.40) with Supplement (form 2.4.41), issued in compliance with 1.11, Part III "Survey of Ships in Compliance with International Conventions, Codes, Resolutions and Rules for the Equipment of Sea-Going Ships" of the Guidelines on Technical Supervision of Ships in Service;

.3 SO_x Emission Compliance Certificate (SECC) issued by any Administration or under the authorization thereof; or

SO_x Emission Compliance Certificate (form 2.4.42), issued by the Register under the authorization of any Administration;

.4 International Energy Efficiency Certificate (IEEC) issued by any Administration or under the authorization thereof; or

International Energy Efficiency Certificate (form 2.4.3) with Supplement (form 2.4.3.1), issued in compliance with 1.11, Part III "Survey of Ships in Compliance with International Conventions, Codes, Resolutions and Rules for the Equipment of Sea-Going Ships" of the Guidelines on Technical Supervision for Ships in Service; or

Energy Efficiency Certificate (form 2.4.3rf) with Supplement (form 2.4.3.1rf).

3.4.2 Operating procedures and ship's technical documentation in respect of air pollution prevention:

.1 approved Technical File of the engine on the NO_x emission for each engine subject to survey in accordance with the NO_x Technical Code, including the engine fitted with NO_x-reducing device as an engine component;

.2 approved EGCS — SO_x Technical Manual (ETM) (where applicable);

.3 drawings of any exhaust gas cleaning system which shall be approved in compliance with the IMO Guidelines;

.4 approved Onboard Monitoring Manual (OMM) (where applicable);

.5 approved SO_x Emission Compliance Plan (SECP) (where applicable);

.6 Record Book of SO_x-Reducing Device Parameters;

.7 approved documentation on the ship's fuel oil system confirming possibility of ready change over to

low-sulphur content fuel oil when approaching SO_x emission control areas established under Annex VI to MARPOL 73/78 or Directive 99/32/EU accordingly (where applicable);

.8 procedure for preparing the ship's fuel oil system for operation in the SO_x emission control area (SECA) (where applicable);

.9 Fuel Oil Management Plan, Fuel Oil Record Book;

.10 incinerator systems diagram;

.11 refrigerating operations management procedure;

.12 refrigerating systems diagrams, list of refrigerants used;

.13 fire-fighting systems diagrams, list of fire extinguishing media used in these systems;

.14 Volatile Organic Compound (VOC) Management Plan;

.15 Energy Efficiency Design Index (EEDI) Technical File (where applicable);

.16 Ship Energy Efficiency Management Plan (SEEMP).

3.4.3 Marine Environment Pollution Prevention Certificates:

.1 International Oil Pollution Prevention Certificate (IOPP) issued by any Administration or under the authorization thereof; or

International Oil Pollution Prevention Certificate (form 2.4.5) with Supplement (forms 2.4.20 or 2.4.26) issued in compliance with 1.11, Part III "Survey of Ships in Compliance with International Conventions, Codes and Resolutions" of the Guidelines on Technical Supervision for Ships in Service; or

Pollution from Ships Prevention Certificate (form 2.4.18rf);

.2 International Sewage Pollution Prevention Certificate issued by any Administration or under the authorization thereof; or

International Sewage Pollution Prevention Certificate (form 2.4.9) issued in compliance with 1.11 Part III "Survey of Ships in Compliance with International Conventions, Codes, Resolutions and Rules for the Equipment of Sea-Going Ships" of the Guidelines on Technical Supervision for Ships in Service; or

Pollution from Ships Prevention Certificate (form 2.4.18rf);

.3 Certificate of Compliance of Equipment and Arrangements of the Ship with the Requirements of Annex V to MARPOL 73/78 (form 2.4.15) (where applicable); or

Pollution from Ships Prevention Certificate (form 2.4.18rf);

.4 International Anti-Fouling System Certificate issued by any Administration or under the authorization thereof; or

International Anti-Fouling System Certificate (forms 2.4.30 or 2.4.30ec) with the Records of Anti-

Fouling Systems (forms 2.4.31 or 2.4.3ec) respectively, issued by Register under the authorization of Administrations; or

Statement of Compliance of Anti-Fouling System (form 2.4.30.1) with the Record of Anti-Fouling System (form 2.4.31.1), where applicable; or

Declaration on Compliance of Anti-Fouling System with AFS-Convention, if applicable (refer to 3.5.3.8.3);

.5 International Ballast Water Management Certificate issued by any Administration or under the authorization thereof (with due regard to IMO circular BWM.2/Circ.40); or

International Ballast Water Management Certificate (form 2.5.4), issued in compliance with 1.11, Part III "Survey of Ships in Compliance with International Conventions, Codes, Resolutions and Rules for the Equipment of Sea-Going Ships" of the Guidelines on Technical Supervision for Ships in Service;

.6 Statement of compliance to IMO resolution on ship recycling "Green passport" (form 2.4.8) with Supplement (form 2.4.8.1).

3.4.4 Operating procedures and ship's technical documentation in respect of marine environment pollution prevention:

.1 ship's general arrangement plan and tanks plan;

.2 approved documentation confirming compliance of the oil tanker with the requirements for double hull construction in accordance with regulation 19 of Annex I to MARPOL 73/78;

.3 approved documentation confirming compliance of the ship with the requirements for protective location of fuel oil tanks as defined in regulation 12A of Annex I to MARPOL 73/78 (refer to 3.5.3.10.5 to 3.5.3.10.7 and 3.6.3.10.2);

.4 approved Shipboard Oil Pollution Emergency Plan or Shipboard Marine Pollution Emergency Plan (for Oil and Noxious Liquid Substances) considering regulation 37.4 of Annex I to MARPOL 73/78 in relation to fast access to computerized shore-based software for calculation of damage stability and residual structural strength, as well as Oil Record Book, Parts I and II (regulations 17 and 36 of Annex I to MARPOL 73/78);

.5 approved Shipboard Marine Pollution Emergency Plan for Noxious Liquid Substances (regulation 17 of Annex II to MARPOL 73/78), approved Procedures and Arrangement Manual (regulation 14 of Annex II to MARPOL 73/78) and Cargo Record Book (regulation 15 of Annex II to MARPOL 73/78);

.6 approved Transfer of Oil Cargo between Oil Tankers at Sea (STS Operations) Plan (for oil tankers, where available);

.7 approved Ballast Water Management Plan;

.8 approved Ship's Guidelines for Safe Water Ballast Exchange at Sea (where applicable);

.9 Ballast Water Record Book;

.10 approved ship's software for planning water ballast exchange at sea (where applicable in compliance with 3.5.3.4.2);

.11 Biofouling Management Plan and Biofouling Record Book in compliance with IMO resolution MEPC.207(62);

.12 approved ship's software for calculation of intact trim, stability and strength as well as damage trim and stability;

.13 Sewage Management Plan and Sewage Record Book;

.14 sewage system diagram and sanitary and domestic waste waters system diagram;

.15 Record Book of Detection and Elimination of Petroleum Products (Fuel oil, Hydraulic oil, etc) Operating Leakages to be avoid;

.16 diagrams of manifolds in cargo areas, as well as branch pipes and flanges for fuel oil and oil bunkering, oil residues and oily water discharge indicating the trays and appliances for prevention of spillage of Oil and Noxious Liquid Substances carried in bulk;

.17 diagrams and drawings of fuel oil system, bilge system, oil discharge, monitoring and control system for ballast and flushing water, ballast water system;

.18 Garbage Management Plans, placards and Garbage Record Book, diagrams and drawing of equipment for the prevention of pollution by garbage.

3.5 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ECO IN THE CLASS NOTATION

3.5.1 Introduction.

3.5.1.1 The provisions of the present Chapter cover the requirements on emissions to air from sources of power, oil tanker cargo systems and service systems onboard, as well as requirements for discharges to sea from sources of power, from ship's systems and equipment of machinery spaces and from cargo areas of oil tankers, chemical tankers and NLS tankers, from sewage systems, anti-fouling systems, as well as the requirements for the prevention of pollution by garbage.

3.5.1.2 The required documentation is specified in 3.4.

3.5.2 Prevention of air pollution.

3.5.2.1 General.

3.5.2.1.1 Fuel oil supplied to the ship shall not contain inorganic acids or chemical wastes that can endanger a ship, bring harm to the crew or that can add to air pollution.

3.5.2.1.2 Fuel oil shall be controlled in accordance with Fuel Oil Management Plan, Fuel Oil Record Book.

Quality of ordered fuel oil and quality of received fuel oil according to bunker delivery note shall be documented in Fuel Oil Record Book (refer to regulations 18.3 and 18.4 of Annex VI to MARPOL 73/78, as well as Directive 99/32/EU, as amended).

Fuel Oil Management Plan shall comprise adequate procedures for replacement of fuel oil in order to make sure that fuel oil burnt in the engine in the SO_x emission control area is of the required quality. Relevant ship's log shall contain evidence that the fuel oil of the required quality was used in relevant areas.

3.5.2.1.3 SECP shall be readily available in all ships using exhaust gas cleaning system to reduce SO_x emission to confirm compliance with the requirements of regulations 14.1 and 4.14 of Annex VI to MARPOL 73/78.

This Plan shall list all ship's plants for burning fuel oil, which comply with the operating requirements specified in the above regulations by adoption of the approved system specified above.

3.5.2.1.4 Bunker delivery note shall be accompanied by sample of supplied fuel oil properly sealed and signed by representatives of the bunkering company, ship master or ship officer responsible for bunkering operations. Bunker delivery note shall be kept onboard for three years. Fuel oil sample shall be stored under ship's officers control until the end of consumption but not less than 12 months from the date of supply.

This note shall confirm that a fuel oil is supplied in accordance with regulations 14 and 18 of Annex VI to MARPOL 73/78, i.e. sulphur content in the supplied fuel oil complies with the applicable requirements and there are no inorganic acids and chemical wastes in this fuel oil.

For the purpose of cross-reference the number of sample shall be stated in the note.

3.5.2.1.5 Sampling equipment and testing procedures shall comply with provisions of documents specified in 3.3.3.

In order to fulfill the requirements of IMO resolution MEPC.182(59) in respect of method and place of fuel oil sampling the ship shall be fitted with the sampling device of approved structure (irrespective whether the fuel oil supplier has a sampling device for installation on the inlet header of receiving ship or not).

3.5.2.2 Prevention of pollution by emission from marine diesel engines.

3.5.2.2.1 NO_x emission restrictions are applied to engines permanently fitted onboard of power output more than 130 kW, except engines that are part of any equipment used in emergency solely onboard the ships where they are installed and engines on lifeboats.

3.5.2.2.2 Level of emission from engines on all ships shall comply with Annex VI to MARPOL 73/78.

3.5.2.2.3 Appropriate certificates shall be issued to marine engines of power more than 130 kW (except emergency ones and those for lifeboats) and to exhaust gas cleaning systems to reduce SO_x emission (if applicable) in accordance with 3.4.1.

3.5.2.2.4 If the exhaust gas cleaning system is used to reduce NO_x emission, the engine and the above system for which it is installed are treated as a single whole. When

for NO_x reduction a selective catalytic reduction (SCR) system is used, the requirements of IMO resolution MEPC.198(62), as amended, shall be met.

3.5.2.2.5 Measurements of NO_x emission level from diesel engines with exhaust gas cleaning system to reduce NO_x emission or without it shall comply with methods specified in the NO_x Technical Code. Measurements and tests shall be performed and documented in accordance with the provisions of the Guidelines on Marine Diesel Engines Survey in Compliance with the Technical Code on Control of Emission of Nitrogen Oxides from Marine Diesel Engines.

3.5.2.2.6 When a ship operates outside the SO_x emission control areas the maximum sulphur content in fuel oil supplied to the ship shall be 3,0 %. When an exhaust gas cleaning system is used, the SO₂ (ppm)/CO₂ (% v/v) ratio shall not exceed 128,0.

3.5.2.2.7 During operation of ships in the territorial seas, coastal zones and EU ports the sulphur content in fuel oil shall not exceed values specified in EU Council Directive 1999/32/EU, as amended (articles 3 and 4).

3.5.2.2.8 During operation of passenger ships engaged on the regular voyages to/from the EU ports the sulphur content in fuel oil shall not exceed values specified in Directive 2005/33/EU (article 4a).

3.5.2.2.9 Transition from one type of fuel oil to another while coming in and out of the SO_x emission control areas specified in Annex VI to MARPOL 73/78, as well as while coming in and out of the EU territorial waters including mooring and anchoring in the EU ports shall be registered in the ship's log.

3.5.2.2.10 During survey of engines fitted with the exhaust gas cleaning systems to reduce SO_x emission, the compliance with SO_x emission norms specified in the Guidelines for On-Board Exhaust GAS-SO_x Cleaning System (IMO resolution MEPC.259(68)) shall be confirmed.

3.5.2.3 Prevention of pollution by refrigerant emission.

3.5.2.3.1 The requirements of the present Section for prevention of pollution by refrigerant emission are applied to cargo refrigerating plants, air conditioning plants and refrigerating systems of all ships.

The said requirements are not applied to autonomous home air-conditioners, refrigerators and freezers permanently sealed and having no connections for refrigerant charging onboard.

3.5.2.3.2 In accordance with provisions of the Montreal Protocol 1987 criteria for refrigerant emission are limited by requirements relative to qualities of used refrigerants in relation to their ozone depleting potential (ODP) and global warming potential (GWP).

3.5.2.3.3 It is not allowed to use ozone-depleting substances on ships.

The following substances may be used as refrigerants onboard:

natural refrigerants (such as, ammonia (NH₃) or carbonic acid (CO₂));

hydro fluorocarbon (HFC) with ODP = 0 and GWP < 3500.

3.5.2.3.4 The Refrigerant Management Procedure shall be implemented on board the ships to control presence of leaks which shall contain as a minimum the following issues:

operation of refrigerating plants to prevent/minimize possible leaks;

periodicity of inspections of refrigerating plants aimed at finding leaks and keeping records of their quantity;

performing corrective actions if leaks exceed norms, operating limitations to prevent such leaks.

Corrective actions shall be performed before the quantity of leaks reaches 10 per cent of the total quantity of refrigerant in each system.

3.5.2.3.5 In order to regenerate a refrigerant, compressors shall be able to discharge refrigerant from the system into the relevant receiver of the liquid refrigerant. Additionally, regenerating units shall be fitted to discharge refrigerant from the system into the existing refrigerant receivers or appropriate receivers.

3.5.2.3.6 When different types of refrigerants are used, measures shall be provided to prevent mixing of such substances.

3.5.2.3.7 In order to make sure there are no emissions to air or that they are reduced to minimum, refrigerants in the refrigerating systems shall be controlled by appropriate method to discover all types of leaks, including those that are usually not discovered by the automatic leak detection system.

One of the following methods or combination thereof may be used:

leak detection system appropriate for the used refrigerant with signaling if refrigerant is found outside refrigerating system;

measuring of refrigerant level in the refrigerating system with low level signaling;

registering refrigerant level in special journal at certain intervals (once in a week as a minimum) to find out minor leaks.

3.5.2.4 Prevention of pollution by fire extinguishing media emission.

3.5.2.4.1 Natural fire extinguishing media (such as argon, nitrogen, CO₂) used in fixed fire extinguishing systems are not considered as ozone depleting substances.

3.5.2.4.2 When other fire extinguishing media (for instance, hydrofluorocarbons (HFC) are used in fixed fire extinguishing systems, the media shall have the following properties: GWP < 4000, ODP = 0.

3.5.2.5 Prevention of pollution by volatile organic compounds emission.

3.5.2.5.1 In order to prevent emission of VOC from oil tankers carrying crude oil, petroleum products, as well as from chemical tankers carrying chemical cargoes with

flashpoint <60°C, standards for cargo vapour discharge systems shall be applied according to MSC/Circ.585.

3.5.2.5.2 Approved technical documentation for the cargo vapour discharge system including principal diagram of the pipeline for vapour collection on oil tanker with indication of location and purpose of all control and safety arrangements as well as cargo transfer instruction shall be available onboard. This instruction shall contain information on the maximum permissible speed of cargo transfer, maximum pressure drop in the ship vapour collection system at different speeds of loading, operation threshold of each high-speed or vacuum valve etc.

3.5.2.5.3 In Appendix to the International Air Pollution Prevention (IAPP) Certificate there shall be a note on the presence of cargo vapour collection system fitted and approved in accordance with MSC/Circ.585.

3.5.2.5.4 An approved VOC Management Plan shall be available on board the ship.

3.5.2.6 Prevention of pollution by emission from shipboard incinerators.

3.5.2.6.1 Shipboard incinerators shall be type-approved in accordance with IMO resolution MEPC.76(40) or MEPC.244(66), as applicable.

3.5.2.6.2 Approved diagrams of the incinerator systems, the copy of Incinerator Type Approval Certificate as well as incinerator operational manual shall be available on board the ship.

3.5.2.6.3 In the Certificates (Supplements) given in 3.4.1.1 and 3.4.3.3, Certificate shall contain notes on shipboard incinerator corresponding to IMO resolution MEPC.76(40) or MEPC.244(66), as applicable.

3.5.2.6.4 Operation of incinerators shall be in accordance with regulation 16 of Annex VI to MARPOL 73/78 and the approved Garbage Management Plan, and be recorded in the Garbage Record Book specified in regulations 10.2 и 10.3 of Annex V to MARPOL 73/78, respectively.

3.5.2.7 Energy efficiency.

3.5.2.7.1 New ship of 400 gross tonnage and above shall be constructed and operated in compliance with chapter 4 in Annex VI to MARPOL 73/78 (IMO resolution MEPC.203(62), as amended) in terms of energy efficiency depending on the ship type and propulsion plant.

3.5.2.7.2 Each (new and existing) ship of 400 gross tonnage and above, except platforms (including floating offshore oil-and-gas production units), mobile offshore drilling units irrespective of propulsion plants and any non-self-propelled ship, shall keep on board and implement Ship Energy Efficiency Management Plans (SEEMP).

3.5.3 Prevention of marine environment pollution.

3.5.3.1 General.

Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

3.5.3.2 Discharge of contaminated water and water polluted with noxious liquid substances from cargo areas of ships.

3.5.3.2.1 Discharge criteria apply to tankers carrying crude oil, petroleum products or noxious substances in bulk.

3.5.3.2.2 Discharge of contaminated ballast water or washing water from the area of cargo tanks of oil tankers shall be carried out by the system of automatic measuring, record and control of discharge of ballast and washing water. Discharge criteria shall be in compliance with Annex I to MARPOL 73/78.

3.5.3.2.3 Each tanker designed for the carriage of noxious substances in bulk shall be equipped with pumps and pipelines, providing stripping of each tank carrying cargoes with pollution categories X, Y and Z, in the way that the quantity of residues in the tank and associated piping does not exceed 75 l in accordance with Annex II to MARPOL 73/78. Discharge of contaminated water to sea shall be carried out by means specified in Annex II to MARPOL 73/78.

3.5.3.2.4 The above discharges and discharge to shore reception facilities shall be documented in the Oil Record Book, or Cargo Record Book, for oil tankers and chemical tankers, respectively.

3.5.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.

3.5.3.3.1 Oil tankers, chemical tankers and NLS tankers shall have fitted and implemented means and arrangements to reduce the possibility of oil or NLS spill on deck reaching the sea.

3.5.3.3.2 To keep cargo spills within the cargo area, provision shall be made for a permanent continuous coaming on the cargo deck extending from side to side and from a point 0,2L forward of amidships to the aft end of the cargo deck with the minimum heights given in Table 3.5.3.3.2:

Table 3.5.3.3.2

Minimum heights of continuous coaming		
Ships of 100000 t deadweight and over	0,2L forward of amidships	0,25 m
	Aft end of cargo deck	0,40 m
Ships of less than 100000 t deadweight	0,2L forward of amidships	0,10 m
	Aft end of cargo deck	0,25 m

3.5.3.3.3 To collect possible oil spills during cargo operations the main deck in the cargo area shall be fitted with a deck scupper system for collection of the spilled cargo with its accumulation in the holding tank or a slop tank. The deck scupper system may be arranged either with a manually operated valve or with automatic scuppers.

The drainage shall be used during cargo operations where cargo spills may occur, and shall not be used under normal conditions when at sea. When at sea, deck scupper system shall preclude free surface effect with negative impact on the ship's stability.

3.5.3.3.4 On oil tankers, chemical tankers and NLS tankers the points where cargo hoses are connected to

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cargo manifolds shall be fitted with spill trays with arrangement for spills collection to the holding or slop tank.

The trays shall have the following minimum dimensions:

tray length shall be so that the cargo manifold doesn't extend beyond forward and aft ends of the tray;

width — at least 1,8 m, at that the spill tray extends at least 1,2 m outboard of the end of the manifold flange;

minimum depth — 0,3 m.

3.5.3.3.5 Oil tankers, chemical tankers and NLS tankers shall be fitted with means to adequately support hoses in way of ship's side abreast of manifolds. The support shall preferably be arranged as a horizontal curved plate or pipe section.

3.5.3.3.6 Oil tankers, chemical tankers and NLS tankers shall be fitted with a closed sounding system with high and maximum level alarms in cargo tanks. Alternatively, a high level alarm may be accepted in combination with a closed sounding system, provided the alarm is independent from the sounding system.

3.5.3.3.7 Fuel oil, lubricating oil and other petroleum products bunker tanks on all ships shall be fitted with high level alarm to prevent overfilling.

3.5.3.3.8 Locations on the open deck in the area of fuel and lubricating oil pipes, standard connections for oil residues discharge (located outside the bunkering station areas), vent and overflow pipes, other areas where petroleum products and NLS spill may occur shall be fitted with spill trays or restricted by sufficient coamings to prevent their escape to sea.

Oil and fuel bunkering stations located in the provided spaces shall be fitted with deck scupper system for collection of spill with its accumulation in the relevant holding tank.

Installation of spill tray is allowed for several vent/overflow pipes with a volume of at least 160 l capacity.

The requirements specified in 3.5.3.3.8 may not be applied to vent/overflow pipes of small capacity independent tanks when their filling is provided on location area via portable pumps.

3.5.3.3.9 Any oil tanker involved in STS operations shall carry on board an approved plan how to conduct STS operations (STS Operations Plan) in compliance with IMO resolution MEPC.186(59).

3.5.3.4 Prevention of pollution at oil contaminated and bilge water discharge.

3.5.3.4.1 The requirements for filtering equipment and for discharge of oily bilge water in compliance with regulations 14 and 15 of Annex I to MARPOL shall apply to all ships as specified thereof.

3.5.3.4.2 In addition to the requirements of Annex I to MARPOL 73/78, each ship shall be fitted with the oil contaminated bilge water holding tank of sufficient capacity agreed with the Register for bilge water storage and disposal to reception facilities.

3.5.3.5 Prevention of pollution by garbage.

3.5.3.5.1 The requirements to garbage management and the availability of Garbage Management Plans and placards shall apply to all ships in compliance with Annex V to MARPOL 73/78 regardless the ship gross tonnage and permissible number of persons on board.

3.5.3.5.2 A ship shall be equipped with the marked containers with tight covers for garbage, collection and storage prior to its discharge to the sea in the allowed areas in accordance with the regulations 3 to 6 of Annex V to MARPOL 73/78 or prior to its incineration in the ship incinerators or discharge to shore reception facilities.

3.5.3.6 Prevention of pollution by sewage.

3.5.3.6.1 A ship shall be provided with a Certificate specified in 3.4.3.2.

3.5.3.6.2 All ships shall be fitted with a sewage holding tank and sewage treatment plant of sufficient capacity having a Certificate of Type Approval in compliance with IMO resolution MEPC.159(55) or MEPC.227(64), as applicable.

The above holding tank of sufficient capacity shall be fitted with the effective visual indication means of its capacity with visual and audible alarm activated at its filling by 80 per cent filling of the tank.

3.5.3.6.3 All ships equipped with a pipeline for discharge of untreated sewage shall be fitted with pipelines with a standard discharge connection in accordance with regulation 10 of Annex IV to MARPOL 73/78 for sewage discharge to reception facilities.

3.5.3.6.4 All ships equipped with a pipeline for discharge of untreated sewage shall be provided with calculations of the rate of discharge of untreated sewage approved by the Register upon authorization of the Administration. These calculations shall be drawn up according to Recommendation on Standards for the Rate of Discharge of Untreated Sewage from ships in compliance with IMO resolution MEPC.157(55).

3.5.3.6.5 All sewage discharges, whether to sea or to shore-based reception facilities shall be recorded in the appropriate record book with indication of date, location and quantity of sewage discharged. In cases where untreated sewage is discharged to sea, the record shall include information on the ship's speed which shall correspond to the approved rate of discharge and the distance to the nearest shore (more 12 nautical miles¹) at the moment of discharge.

3.5.3.7 Anti-fouling systems

3.5.3.7.1 Anti-fouling systems (coatings) containing organo-tin compounds (Tributyltin (TBT)) as the active ingredients are not permitted.

3.5.3.7.2 Ships of 400 gross tonnage and upwards shall carry one of Certificates, Statement or Declaration of Compliance of Anti-Fouling System with the International

¹Hereinafter a nautical mile is equal to 1852 m.

Convention on the Control of Harmful Anti-Fouling Systems of Ships, 2001 (AFS-Convention).

3.5.3.7.3 Ships having a length of 24 m (IC66) and more but of less than 400 gross tonnage shall carry declarations on compliance of their anti-fouling systems with AFS-Convention in accordance with form of Addenda 2 to Annex 4 to AFS Convention or with Annex III of EU Regulation 782/2003 (Regulation 5 of Annex 4 to AFS-Convention).

3.5.3.8 Prevention of lubricating oil and hydraulic oil leakages into seawater.

3.5.3.8.1 Requirements for prevention of leakages of lubricating oil and hydraulic oil into seawater shall be applied in the following cases:

if oil-lubricated stern tube bearings and sealing arrangements are provided;

if there is a possibility that lubricating oil will spill into the seawater from the lubricating oil system of the steering gear bearing;

if seawater cooled engines are provided;

if there is a probability that oil from the hydraulic system will spill into the seawater.

3.5.3.8.2 Occurrence of lubricating oil and hydraulic oil operating leakages into seawater shall be continuously monitored. If evidence of leakage is found, corrective actions shall be initiated and recorded in the ship's log. For this purpose all the insignificant oil leaks shall be monitored by the approved manual or automatic methods.

3.5.3.8.3 In case of oil-lubricated stern tube bearings and/or sealing arrangements, the above requirements shall be considered in addition to the requirements for oil level indicators and low level alarm of lubricating oil tanks as well as environmental safety of stern tube arrangements (refer to 5.6.4 and 5.7, Part VII "Machinery Installations").

3.5.3.9 Prevention of pollution in case of the hull damage.

3.5.3.9.1 The ship with the descriptive notations **Oil tanker** or **Oil/ore carrier** or **Chemical tanker** in the class notation shall be provided with double hull and

double bottom in the cargo area in accordance with regulation 19 of Annex I to MARPOL 73/78.

3.5.3.9.2 Requirements to the damage trim and stability characteristics specified in 3.3, Part V "Sub-division" shall be used during flooding of any compartment, if provisions of 3.4 of the above Part do not specify more rigid requirements.

3.5.3.9.3 Any ship shall be fitted with the onboard software to calculate intact trim, stability and strength and to calculate damaged ship trim and stability.

3.5.3.9.4 Oil tankers of 600 t deadweight and over, as well as other ships, with an aggregate fuel oil tanks capacity 600 m³ and over shall have prompt access to computerized, shore-based damage stability and residual structural strength calculation programs in accordance with regulation 37.4 of Annex I to MARPOL 73/78.

3.5.3.9.5 Ships having an aggregate fuel oil tanks capacity 600 m³ and over shall have double hull and double bottom to protect fuel oil tanks in accordance with regulation 12A of Annex I to MARPOL 73/78, irrespective of capacity of each fuel oil tank.

3.5.3.9.6 Location of suction wells in fuel oil tanks shall comply with the requirements of regulation 12A.10 of Annex I to MARPOL 73/78.

3.5.3.9.7 The valves for fuel oil pipelines located at a distance less than h from the ship's bottom shall be arranged at a distance of not less than $h/2$ from the ship's bottom (refer to Fig. 3.5.3.9.7).

3.5.3.10 Segregated ballast tanks.

3.5.3.10.1 Segregated ballast tanks shall be provided on ships with the descriptive notation **Oil tanker** or **Oil/ore carrier** or **Chemical tanker** in the class notation.

3.5.3.10.2 The capacity of the segregated ballast tanks shall be so determined that the ship may operate safely on ballast voyages without recourse to the use of cargo tanks for water ballast.

3.5.4 Prevention of pollution at ship recycling.

3.5.4.1 All ships shall have a Statement of Compliance to IMO resolution on Ship Recycling

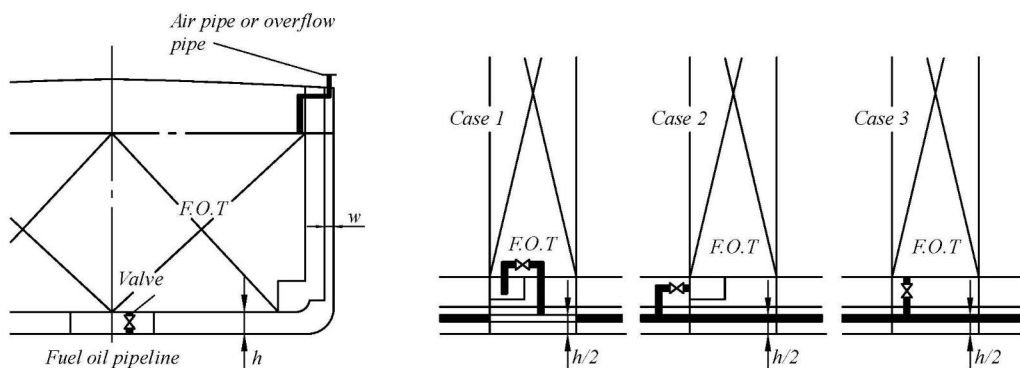


Fig. 3.5.3.9.7

Symbols:

h = the minimum distance of fuel oil tanks location from the moulded line of the bottom shell plating, in m;

w = the minimum distance of fuel oil tanks location from the moulded line of the side shell plating, in m;

F.O.T. = fuel oil tank.

"Green Passport" (form 2.4.8) with Supplement (form 2.4.8-1) according to the Guidelines on Ship Recycling (refer to IMO resolution A.962(23)), with additions or amendments thereto currently adopted.

3.5.4.2 The above Statement with Supplement shall be permanently available on board throughout the ship's operating life. The shipowner shall continuously update the Supplement and include thereto all major ship's structure and equipment changes to maintain the information of the Supplement (form 2.4.8-1) actual.

3.5.5 Environmental responsibilities.

All ships shall have a responsible environmental officer onboard.

This officer shall be responsible for the following:

- checking the compliance with the environment pollution prevention requirements;
- monitoring the implementation of the relevant procedures;
- maintaining the relevant ships' logs;
- education and training of personnel in the relevant environmental practices.

The responsible environmental officer may delegate authorities to other crew members remaining responsible for the organization of environment protection measures on board the ship.

3.6 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ECO-S IN THE CLASS NOTATION

3.6.1 Introduction.

3.6.1.1 The provisions of the present Chapter cover the requirements for emissions to air from sources of power, cargo systems of oil tankers and service systems on board the ship, as well as the requirements for discharges to sea from sources of power, shipboard systems and equipment of machinery spaces, from cargo areas of oil tankers, chemical tankers and NLS tankers, from sewage systems, anti-fouling systems of the ship, as well as the requirements for prevention of pollution by garbage.

3.6.1.2 Requirements for assigning the distinguishing mark ECO-S in the class notation are more stringent as regards prevention of air and marine environment pollution as compared to the requirements for assigning the distinguishing mark ECO in the class notation.

3.6.1.3 The required documentation is listed in 3.4.

3.6.2 Prevention of air pollution.

3.6.2.1 General.

3.6.2.1.1 Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

3.6.2.1.2 Fuel oil to be used onboard shall comply with the requirements 3.5.2.2.6 to 3.5.2.2.8.

3.6.2.2 Prevention of pollution by emission from marine diesel engines.

3.6.2.2.1 NO_x emission restrictions are applied to engines permanently fitted onboard of power output more than 130 kW, except engines that are part of any equipment used in emergency solely onboard the ships where they are installed and engines on lifeboats.

3.6.2.2.2 Level of emission from engines on all ships shall not exceed the following maximum values proceeding from nominal r.p.m. of engines:

13,4 g/Kw·h when $n < 130$ rpm;

$(44 n^{(-0,23)} - 1,0)$ g/Kw·h when $n \geq 130$ rpm but < 2000 rpm;

6,7 g/Kw·h when $n \geq 2000$ rpm.

3.6.2.2.3 The exhaust gas cleaning system to reduce NO_x emission (if fitted) shall comply with the requirements of 3.5.2.2.4.

3.6.2.2.4 Compliance with the requirements for SO_x emission restrictions shall be confirmed in accordance with 3.5.2.2.6 to 3.5.2.2.10.

3.6.2.3 Prevention of pollution by refrigerant emission.

3.6.2.3.1 The requirements of the present Section for prevention of pollution by refrigerant emission shall comply with the requirements of 3.5.2.4.

3.6.2.3.2 The following substances may be used as refrigerants onboard:

natural refrigerants (such as, ammonia (NH₃) or carbonic acid (CO₂));

hydrofluorocarbon (HFC) with ODP = 0 and GWP < 1890.

3.6.2.3.3 Structural and operational requirements shall comply with 3.5.2.4.4 to 3.5.2.4.8.

3.6.2.4 Prevention of pollution by fire extinguishing media emission.

3.6.2.4.1 Natural fire extinguishing media (such as argon, nitrogen, CO₂) used in fixed fire extinguishing systems are not considered as ozone depleting substances.

3.6.2.4.2 When other fire extinguishing media (for instance, hydrofluorocarbons (HFC) are used in fixed fire extinguishing systems, the media shall have the following properties: GWP < 1650, ODP = 0.

3.6.2.5 Prevention of pollution by volatile organic compounds emission.

In order to prevent emission of VOC from oil tankers carrying crude oil, petroleum products or chemical cargoes with flashpoint < 60 °C, the requirements of 3.5.2.5 shall be applied.

3.6.2.6 Prevention of pollution by emission from shipboard incinerators.

Shipboard incinerator shall comply with the requirements of 3.5.2.6.

3.6.2.7 Energy efficiency.

3.6.2.7.1 Energy efficiency shall be provided in compliance with the requirements in 3.5.2.8.

3.6.3 Prevention of marine environment pollution.

3.6.3.1 General.

Compliance with the requirements shall be confirmed in accordance with 3.2 to 3.4.

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3.6.3.2 Discharge of cargo residues.

3.6.3.2.1 Discharge criteria for cargo residues for tankers carrying crude oil, petroleum products or noxious substances in bulk are specified in 3.5.3.2.

3.6.3.2.2 Each tanker designed for the carriage of noxious substances in bulk shall be equipped with pumps and pipelines, providing stripping of each tank carrying cargoes with pollution categories X, Y and Z, in the way that the quantity of residues in the tank and associated piping does not exceed 50 l in accordance with Annex II to MARPOL 73/78. Discharge of contaminated water to sea shall be carried out by means specified in Annex II to MARPOL 73/78.

3.6.3.2.3 Cargo tanks shall have smooth inner surfaces and be equipped with cargo wells for efficient stripping. Horizontal framing shall be avoided as far as practicable. Corrugated bulkheads may be allowed with the maximum horizontal angle of corrugations of 65°.

3.6.3.2.4 A washing system with the cleaning machines so arranged that all the surfaces of each tank be washed is obligatory.

3.6.3.2.5 On chemical tankers type 3 as defined in 2.1.2 of the International Code for the Construction and Equipment of Ships Carrying Dangerous Chemicals in Bulk (IBC Code), cargo tanks shall be located at a distance of at least 0,76 from the shell plating.

3.6.3.3 Structural measures and equipment for prevention of oil spills during cargo operations and bunkering.

3.6.3.3.1 Oil tankers, chemical tankers and NLS tankers shall have fitted and implemented means and arrangements to reduce the possibility of oil or NLS spill on deck reaching the sea according to 3.5.3.3.2.

3.6.3.3.2 To collect possible oil spills during cargo operations the main deck in the cargo area shall be fitted with a deck scupper system for collection of the spilled cargo according to 3.5.3.3.3.

3.6.3.3.3 On oil tankers, chemical tankers and NLS tankers where cargo hoses are connected to cargo manifolds, the provision shall be made for spill trays with arrangements for spills collection to the tank according to 3.5.3.3.4.

3.6.3.3.4 In the drainage collecting system, shutoff valves shall be provided to stop the drainage into collecting tanks.

3.6.3.3.5 Oil tankers, chemical tankers and NLS tankers shall be fitted with means to support hoses according to 3.5.3.3.5.

3.6.3.3.6 Oil tankers, chemical tankers and NLS tankers shall be fitted with a closed sounding system with high and maximum level alarms.

3.6.3.3.7 Equipment of tanks for fuel oil, lubricating oil and other petroleum products bunkering in all ships, as well as equipment of bunkering stations, vent and overflow pipes and other areas where petroleum products spills may occur shall comply with the requirements of 3.5.3.3.7 and 3.5.3.3.8.

3.6.3.3.8 Oil and fuel bunkering stations located on the open deck outside the spaces shall be fitted with the closed system for collecting petroleum products to the holding tank or slop tank.

3.6.3.4 Prevention of pollution at oil contaminated water discharge.

3.6.3.4.1 Oil contaminated water discharge requirements apply to all ships according to regulations 15 and 34 of Annex I to MARPOL 73/78.

3.6.3.4.2 The maximum oil content at the outlet of bilge separators fitted onboard shall not exceed 5 ppm.

3.6.3.4.3 The above separators in all cases shall be fitted with 5 ppm bilge alarm and automatic shut-off valve.

3.6.3.4.4 Each ship shall be fitted with the bilge water holding tank of sufficient capacity agreed with the Register for bilge water disposal to reception facilities. Bilge water shall be collected to the above holding tank from all bilge wells of machinery spaces.

3.6.3.5 Prevention of pollution by garbage.

3.6.3.5.1 Prevention of pollution by garbage shall comply with the requirements of 3.5.3.6.

3.6.3.5.2 A ship having the descriptive notation *Passenger ship* in the class notation shall be fitted with the following equipment:

marked containers for garbage in accordance with the requirements 3.5.3.5;

food wastes comminutors shall provide for comminution to particles not exceeding 25 mm in size;

incinerators shall be type approved according to IMO resolution MEPC.76(40) or MEPC.244(66), as applicable, to provide full solid domestic waste incineration when allowed.

3.6.3.6 Prevention of pollution by sewage.

3.6.3.6.1 Prevention of pollution by sewage shall be in accordance with 3.5.3.6 (except for 3.5.3.6.2) and 3.6.3.6.2 to 3.6.3.6.4.

3.6.3.6.2 A ship shall be fitted with the sewage treatment plant being of a type approved in compliance with IMO resolution MEPC.159(55) or MEPC.227(64), as applicable, as well as sewage holding tank being equipped as specified in 3.5.3.6.2.

3.6.3.6.3 Ships having the descriptive notation *Passenger ship* in the class notation shall have a sewage holding tank of sufficient capacity to allow storage of both sewage ("black water") and sanitary and domestic waste waters ("grey water") while the ship is in the area where discharge is prohibited. The holding tank shall be fitted as specified in 3.5.3.6.2.

3.6.3.6.4 The sewage treatment plant of ships having the descriptive notation *Passenger ship* in the class notation shall be capable to treat both sewage ("black water") and sanitary and domestic waste waters ("grey water"). When the ship is operated in Special areas defined in compliance with the amendments to Annex IV to MARPOL 73/78 in IMO resolu-

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tion MEPC.200(62), the above plant shall have a Certificate of type approval for sewage treatment plants in compliance with IMO resolution MEPC.227(64).

3.6.3.7 Control of harmful anti-fouling systems.

The requirements of 3.5.3.7 are applicable.

3.6.3.8 Prevention of lubricating oil and hydraulic oil leakages into seawater.

The requirements of 3.5.3.8 are applicable.

3.6.3.9 Prevention of pollution in case of the hull damage.

3.6.3.9.1 For ships with aggregate capacity of fuel oil tanks 600 m³ and above, the requirements of 3.5.3.10 shall apply.

3.6.3.9.2 For ships with aggregate capacity of fuel oil tanks less than 600 m³, all fuel oil tanks shall be located at a distance of at least 0,76 m from the shell plating. This requirement shall not apply to small fuel oil tanks with the capacity not exceeding 30 m³.

3.6.3.9.3 All oil residue (sludge) tanks and oily bilge water holding tanks shall be located at a distance of at least 0,76 m from the shell plating. This requirement shall not apply to such small tanks with the capacity not exceeding 30 m³.

3.6.3.9.4 Cargo and slop tanks of oil tankers of less than 5000 t deadweight shall be protected throughout the length by ballast tanks or compartments not intended for carriage of pollutants located in compliance with the requirements of regulation 19.6.1 (from the ship's bottom shell plating) and regulation 19.6.2 for the distance w (from the ship's side shell plating) of Annex I to MARPOL 73/78.

On ships other than oil tankers, all cargo tanks designed and intended for carrying oil shall be located at a distance of at least 0,76 m from the shell plating.

3.6.3.10 Segregated ballast tanks.

Requirements of 3.5.3.11 are applicable.

3.6.4 Additional technical means.

3.6.4.1 In case of failure of essential machinery of the ship's propulsion plant responsible for maintaining the ship's manoeuvrability in case of emergency, alternative means shall be provided to keep the ship's manoeuvrability.

The following means may be used as alternative (as far as applicable):

two- and multi-shaft propulsion plants;

stem tube arrangements with the possibility of their repair without ship docking and using environmentally friendly media for lubrication and stem tube bearing cooling;

auxiliary retractable azimuth thrusters to keep the ship's speed and course in case of main propulsion plant damage;

four-blade propellers with detachable blades to ensure propulsion in case of damage to a blade where the opposite blade is removed;

"Power take-in" system to transmit the power from an auxiliary electric power plant to the propeller in case of main engine failure;

thrusters in case of main steering gear damage.

3.6.4.2 In addition to the navigational equipment and systems complying with the basic (main applicable) requirements of Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships, a ship shall be fitted with an automatic ground collision avoidance system, and the information on the ship's maneuvering characteristics shall be available on the navigation bridge.

3.6.5 Prevention of pollution at ship recycling.

The requirements of 3.5.4 are applicable.

3.6.6 Environmental responsibilities.

The requirements of 3.5.5 are applicable.

3.7 RECORDS

3.7.1 As a result of applying the requirements of the present Section, the following records will be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing marks ECO or ECO-S in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

4 REQUIREMENTS FOR THE EQUIPMENT OF SHIPS IN COMPLIANCE WITH THE DISTINGUISHING MARK ANTI-ICE IN THE CLASS NOTATION

4.1 GENERAL

4.1.1 Scope of application.

4.1.1.1 The requirements for the equipment of ships and FOP in compliance with the distinguishing mark **ANTI-ICE** in the class notation apply to ships and FOP (hereinafter for this Section referred to as "the ships") the design and equipment of which provide effective icing protection. These requirements are additional to the requirements of Part I "Classification", Part III "Equipment, Arrangements and Outfit", Part VIII "Systems and Piping" and Part XI "Electrical Equipment" of the Rules for the Classification and Construction of Sea-Going Ships, as well as Part II "Life-Saving Appliances", Part III "Signal Means", Part IV "Radio Equipment" and Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships.

4.1.1.2 Ships complying with the requirements of the present Section may be assigned with the distinguishing mark **ANTI-ICE** added to the character of classification.

4.1.1.3 The distinguishing mark **ANTI-ICE** in the class notation may be assigned to ships under construction and in service.

4.1.2 Definitions and explanations.

For the purpose of the present Section the following definitions and explanations have been adopted.

De-icing is removal of ice appearing on the ship's hull, structures and equipment.

Icing protection is a set of design and organizational measures aimed at reduction of the ship's icing and reduction of labour input into ice removal during operation of the ship.

Icing is a process of ice accretion on the ship's hull, structures and equipment due to sea water splashes or freezing of moisture condensing on the hull from the atmosphere.

Anti-icing is prevention of ice formation on the ship's structures and equipment by means of their heating or relevant covering.

Icing Protection Manual is a document describing actions of the ship's crew to provide icing protection. The scope of the Manual and contents of the information contained therein depend on the ship's type, purpose and area of navigation; they shall be chosen in the most efficient way and agreed with the Register.

4.1.3 Technical documentation.

4.1.3.1 The following technical documentation shall be submitted to the Register for approval to assign the distinguishing mark **ANTI-ICE** in the class notation:

.1 arrangement plan of anti-icing means with indication of their heating capacity;

.2 calculation of heating capacity of anti-icing systems equipment;

.3 electrical single-line diagram of anti-icing systems with heating cables (if any);

.4 circuit diagram of steam and/or thermal liquids anti-icing systems (if any);

.5 arrangement diagram of de-icing means.

4.1.3.2 The following documents approved by the Register shall be kept onboard:

.1 Icing Protection Manual;

.2 Stability Booklet including loading conditions considering icing.

4.2 TECHNICAL REQUIREMENTS FOR ASSIGNING THE DISTINGUISHING MARK ANTI-ICE IN THE CLASS NOTATION

4.2.1 General.

4.2.1.1 Ships with the distinguishing mark **ANTI-ICE** in the class notation shall, as a rule, be fitted with a tank of a shape providing effective water flow under all operating loading cases.

4.2.1.2 The following anti-icing means may be used:

.1 heating of structures and equipment by means of steam, thermal liquid or heating cables;

.2 use of permanent (awnings, casings) or removable (covers) protective covers;

.3 application of grid structures for platforms, stairs of outer ladders, gangways etc.

4.2.1.3 Besides heating of structures the following de-icing means may be used:

.1 washing and firing of ice by means of hot water or steam;

.2 anti-icing liquids;

.3 manual mechanical means including pneumatic instrument.

4.2.1.4 If steam systems are used for anti-icing the requirements of Section 18, Part VIII "Systems and Piping" shall be complied with.

4.2.1.5 If thermal liquid systems are used for anti-icing the requirements of Section 20, Part VIII "Systems and Piping" shall be complied with.

4.2.1.6 If systems with heating cables are used for anti-icing the requirements of 15.4, Part XI "Electrical Equipment" shall be complied with.

4.2.2 Stability and subdivision.

4.2.2.1 Ships with the distinguishing mark **ANTI-ICE** in the class notation shall comply with the requirements of Parts IV "Stability" and V "Subdivision".

4.2.3 Equipment, arrangements and outfit.

4.2.3.1 Platforms of outer ladders as well as platforms for servicing arrangements and equipment fitted on open decks shall have a grid structure or be equipped with heating elements.

4.2.3.2 Outer ladders located on the escape routes to life-saving appliances as well as muster stations to life-saving appliances (including guard rails) shall be equipped with anti-icing means.

4.2.3.3 Coamings of outer doors leading to the accommodation superstructure spaces shall be heated.

Decks in areas of exit from the said spaces shall be equipped with anti-icing means.

4.2.3.4 A passage from the accommodation superstructure spaces to the equipment fitted in the fore part of the ship shall be provided on tankers, including chemical tankers and gas carriers. This passage shall be provided with anti-icing means.

4.2.3.5 Side scuttles in the wheelhouse providing the arc of visibility required by 3.2, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships according to the ship's class shall be heated.

Windshield wipers on the said side scuttles (if any) shall be heated as well.

4.2.3.6 Shell doors, visor-type bow doors, cargo doors in the fore part of ro-ro ships shall be fitted with means for effective ice removal or other means to provide working capacity of the said appliances in case of icing (for example, with ice-breaking hydraulic cylinders).

4.2.3.7 Design of seals of cargo hatches, shell doors and other closing appliances providing the ship's operation in accordance with its main purpose shall preclude freezing of condensate inside seals.

4.2.3.8 Anti-icing shall be provided for the following arrangements and equipment:

.1 anchor and mooring equipment including (but not limited to) winches, capstans, windlasses, chain stoppers, drums, control panels;

.2 arrangements for emergency towing of tankers, including chemical tankers and gas carriers;

.3 hook releasing devices of lifeboats;

.4 launching appliances of survival craft (falls on drums, sheaves, winches of launching appliances, winch breaks and other elements engaged in launching);

.5 liferafts, including hydrostatic releasing devices.

The Register may require taking measures to prevent icing of additional equipment and arrangements in accordance with the ship's main purpose.

4.2.3.9 Lifeboats shall be of enclosed type and be equipped with the relevant heating elements to prevent icing and blocking of access hatches and/or doors.

4.2.3.10 Proper locations shall be provided on board for at-sea storage of removable covers used to prevent icing of equipment and fittings.

4.2.3.11 In addition to the emergency outfit specified in Section 9, Part III "Equipment, Arrangements and Outfit", ships with the distinguishing mark ANTI-ICE in the class notation shall have the necessary de-icing outfit (crowbars, ice-axes, axes, shovels, spades) kept in places of permanent storage and having the relevant marking.

4.2.4 Systems and piping.

4.2.4.1 Sufficient number of scuppers and freeing ports shall be provided for the effective water flow from open decks. Scuppers and freeing ports shall be located so as to preclude water stagnation on decks under all operating loading cases.

4.2.4.2 Air heads of ballast tanks and fresh water tanks shall be fitted with the relevant heating devices.

4.2.4.3 Design of air intakes of main, auxiliary and emergency power plants as well as of ventilation of spaces, which are of great importance for the ship's safety, shall preclude their icing that may cause air duct blockage.

4.2.4.4 Measures shall be taken to preclude freezing of liquid in the pipelines of fire extinguishing systems by means of their effective drying or heating.

Fire hydrants, monitors, fittings and other equipment of fire extinguishing systems fitted on open decks shall be protected from icing by means of heating or removable covers.

Cut-off valve of water and foam fire extinguishing systems shall be fitted in enclosed heated spaces or shall be heated.

4.2.4.5 Hot water or steam supply shall be provided for de-icing on open decks.

4.2.4.6 In addition to 4.2.4.1 to 4.2.4.5 the following items shall be heated on tankers, including chemical tankers and gas carriers:

.1 ventilation valves and pressure/vacuum valves (P/V valves) of cargo tanks and secondary barriers;

.2 level, pressure, temperature gauges and gas analysers in cargo tanks located on open decks, if necessary;

.3 inert gas system elements containing water and located on open decks;

.4 emergency shut-down system (ESD) on gas carriers.

4.2.4.7 Drives of remotely operated fittings of tankers, including chemical tankers and gas carriers, fitted on open decks shall be equipped with anti-icing means.

4.2.4.8 Pipelines equipped with electrical heating shall comply with the requirements of 5.8, Part VIII "Systems and Piping".

4.2.5 Electrical equipment, signal means, radio and navigational equipment.

4.2.5.1 The following electrical equipment, signal means, radio and navigational equipment located on open decks shall be designed so that to prevent icing or shall be heated:

.1 aerials of radio and navigational equipment (excluding rod aerials), aerial matching devices (if fitted on open decks);

.2 navigation lights;

.3 whistles;

.4 COSPAS-SARSAT satellite emergency position-indicating radio beacons;

.5 main and emergency lighting of open decks;

.6 TV cameras used during operation of the ship in accordance with its main purpose;

.7 aerials of telemetric and dynamic positioning systems;

.8 remote control stopping arrangements of pumps for oil contaminated water and sewage disposal to reception facilities.

4.2.5.2 If consumers, which according to 9.3.1, Part XI "Electrical Equipment" shall be fed from the emergency source of electrical power, are fitted with electrical heating, their heating elements shall be also fed from the emergency source of electrical power.

4.3 TESTS

4.3.1 Approved Icing Protection Manual shall be submitted to the Register prior to tests (only for ships without the distinguishing mark **WINTERIZATION** in the class notation.

4.3.2 Anti-icing means shall be tested including demonstration of their operation for the purpose specified and measurement of their heating capacity.

4.4 RECORDS

4.4.1 As a result of applying the Requirements for the Equipment of Ships in Compliance with the Distinguishing Mark **ANTI-ICE** in the Class Notation the following records shall be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark **ANTI-ICE** in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

5 REQUIREMENTS FOR THE EQUIPMENT OF OIL TANKERS FOR CARGO OPERATIONS WITH OFFSHORE TERMINALS

5.1 GENERAL

5.1.1 Scope of application.

5.1.1.1 The requirements for the equipment of oil tankers for cargo operations with offshore terminals are additional to those of Part I "Classification", Part III "Equipment, Arrangements, and Outfit", Part VI "Fire Protection", Part VIII "Systems and Piping", Part IX "Machinery", Part XI "Electrical Equipment" and Part XV "Automation".

5.1.1.2 A distinguishing mark BLS-SPM may be added to the character of classification of ships equipped with the bow loading system and complying with the requirements of the present Section in the full scope.

A distinguishing mark BLS may be added to the character of classification of ships equipped with the bow loading system and complying with the requirements of the present Section except for 5.6.2 to 5.6.9 and 5.6.12 to 5.6.14.

A distinguishing mark SPM may be added to the character of classification of ships which are not equipped with the bow loading system but complying with the requirements in 5.6.2 to 5.6.9 and 5.6.12 to 5.6.14. The mark SPM may be also added to the character of classification of ships carrying liquefied gas in bulk.

5.1.1.3 Distinguishing marks BLS-SPM, BLS and SPM may be assigned to ships under construction and in service.

5.1.2 Definitions.

Single point mooring (SPM) is a floating or stationary offshore structure intended for mooring the oil tankers or floating offshore oil-and-gas production units and for offloading at sea or at anchorage.

Offshore terminal is a ship or offshore structure which is used for mooring of the oil tanker for loading the cargo.

Bow loading coupler is a device of special design which is a part of the bow loading system and which is used to connect the cargo hose of the offshore terminal to the ship cargo system.

Bow loading system (BLS) is a set of ship equipment located in the fore end of a ship and intended for loading the cargo to the ship from offshore terminals.

5.1.3 Technical documentation.

5.1.3.1 The following technical documentation (where applicable) shall be submitted to the Register to assign distinguishing marks BLS-SPM, BLS or SPM in the class notation:

.1 BLS general arrangement plan with an indication of the cargo system and mooring equipment including:

bow loading coupler, guide roller, chain stopper, traction winch, hawse storage reel, BLS hull structures, control stations;

.2 description and drawings of the bow loading coupler;

.3 calculation and drawings of hull strengthenings for bow hawses and chain stoppers;

.4 fire protection diagram for BLS area;

.5 diagram and calculation of ventilation of BLS special spaces;

.6 drawings of BLS components and assembly units, which surfaces shall be protected by the materials precluding spark formation;

.7 drawings of electrical equipment layout and cable laying in BLS spaces;

.8 BLS circuit diagrams;

.9 BLS connection circuit diagrams;

.10 diagrams of BLS hydraulic system;

.11 BLS operating manual;

.12 BLS test program.

5.1.3.2 The Register may require additional documents to those listed in 5.1.3.1 proceeding from BLS design features.

5.2 SHIP STRUCTURE

5.2.1 Oil tankers equipped with BLS shall be fitted with CPP and thrusters or active means of ship's steering (AMSS) to enable sufficient maneuverability and ship stabilization during cargo operations.

5.2.2 Ships equipped with the dynamic positioning system shall be fitted with the devices for surveillance, verification, manual correction of the automated thrusters and automated propulsion system.

5.3 SHIP'S SPACES

5.3.1 Spaces where bow loading coupler and disconnecting couplings of the cargo pipeline are located, as well as the areas within the radius of 3 m from them are considered as hazardous zone 1 in accordance with 19.2.3, Part XI "Electrical Equipment".

5.3.2 Spaces adjacent to hazardous spaces and zones shall not open thereto and shall be equipped with the ventilation system providing at least 8 air changes per hour.

5.3.3 A space accommodating the bow loading coupler shall be provided with natural ventilation.

5.4 OPENINGS AND THEIR CLOSING APPLIANCES

5.4.1 Entrances, air inlets and other openings to machinery, service spaces and control stations shall not be faced to bow loading couplers and shall be located at a distance of at least 10 m from them.

5.4.2 Doors closing BLS shall comply with the requirements of 7.4, Part III "Equipment, Arrangements and Outfit".

5.4.3 Doors closing BLS, when in the open position, shall be protected from the contact with the metal parts of the equipment taken from the terminal by hardwood or equivalent electric insulating materials and by materials precluding spark formation.

5.4.4 When securing the BLS door there shall be no friction of spark-forming metals.

5.5 ANCHOR ARRANGEMENT

5.5.1 For the anchor arrangement of oil tankers fitted with BLS, design or procedural measures shall be taken to prevent its operation during loading the cargo through BLS.

5.6 MOORING ARRANGEMENT

5.6.1 Ships intended for operation with single point mooring (SPM) and having distinguishing marks BLS-SPM or SPM in the class notation shall be equipped with the mooring arrangement complying with the requirements of 5.6.2 to 5.6.9, 5.6.12 to 5.6.14.

5.6.2 The choice of the breaking strength of the mooring line shall be confirmed by the calculation.

Mooring lines shall comply with the requirements of 4.2, Part III "Equipment, Arrangements and Outfit".

Two mooring lines shall be used for mooring of ships of 150000 t deadweight and above. Each mooring line shall end with a chafing chain of 8 m in length and 76 mm in diameter.

The chain used for the chafing chain shall meet the requirements of 3.6, Part XIII "Materials" and shall be taken as follows:

Grade 3 for ships having a deadweight of up to 350000 t;

Grade R4 for ships of 350000 t deadweight and above.

5.6.3 The ship shall be equipped with one or two bow chain stoppers for the chain of 76 mm in diameter and one or two bow fairleads of at least 600 × 450 mm according to Table 5.6.3.

Table 5.6.3

Ship deadweight, in t	Number of bow chain stoppers	Number of bow fairleads	Safe working load (SWL), in kN
≤100000	1	1	2000
>100000 and <150000	1	1	2500
≥150000	2	2	3500

5.6.4 Bow chain stopper shall be capable of holding the chain of 76 mm in diameter in closed position and shall be designed so that in the open position the said segment of chain and its connection details would freely pass through. The upper yield stress of bow stopper material shall be determined based on the load of at least 2,0 SWL.

5.6.5 Bow chain stoppers shall be located between 2.7 and 3.7 m inboard from the bow fairleads, provided the bow fairlead, stopper and vertical roller (if any) or the winch drum or capstan drum shall be aligned.

5.6.6 In way of the chain stopper location the deck shall be sufficiently strengthened to withstand horizontal loads equal to 2,0 SWL.

5.6.7 The chain stopper shall remain in the closed position when the driving energy disappears. The chain stopper shall be manually driven to be opened.

5.6.8 A single bow fairlead shall be located at the ship centerline. Where two fairleads are fitted they shall be arranged symmetrically on each side of ship's centerline at a distance of 2 to 3 m between them.

The fairlead shall be oval or round in shape, the radius of fairlead rounding shall be at least 3,5 of the chain diameters.

The upper yield stress of fairlead material shall be determined based on the load of at least 2,0 SWL as specified in 5.6.3.

Hull strengthenings in way of the bow fairlead shall be calculated to take up the load equal to 2,0 SWL directed at an angle of $\pm 45^\circ$ in the horizontal plane and $\pm 15^\circ$ in the vertical plane from the fairlead axis.

5.6.9 The arrangement components which are in contact with the chafing chain shall be protected by materials precluding spark formation.

5.6.10 BLS mooring machinery shall comply with the requirements of 1.2, 6.1, 6.4, Part IX "Machinery".

5.6.11 BLS traction winch shall be fitted with a manual drive of drum for release of the hawser when the driving energy disappears.

5.6.12 Where a chain stopper is provided, the braking force of the automatic brake of BLS mooring machinery as required in 6.4.3.1, Part IX "Machinery" may be reduced to the value enabling paying out of the hawser with the constant tension equal to the rated pull of the drive.

5.6.13 The pull at a reel of the mooring winch or capstan used for BLS operation with SPM shall be at least 147 kN.

5.6.14 Where SPM pick-up rope is kept onboard, the winch storage drum used to stow the SPM pick-up rope shall be sufficient size to accommodate the rope of 150 m in length and of 80 mm in diameter.

5.7 SPECIAL ARRANGEMENT

5.7.1 Where a ship with BLS is provided with a special emergency towing arrangement it shall comply with the requirements of 5.6.9 in addition to those specified in 5.7, Part III "Equipment, Arrangements and Outfit".

5.8 SYSTEMS AND PIPING

5.8.1 Cargo system.

5.8.1.1 Cargo piping shall comply with the requirements of 9.2.3 to 9.2.7; 9.3.7, 9.5, Part VIII "Systems and Piping", considering the following:

.1 other facilities to ensure galvanic intrinsic safety may be used instead of those specified in 9.3.7, Part VIII "Systems and Piping" upon agreement with the Register;

.2 BLS piping shall be self-draining with a drainage to the cargo tank;

.3 provision shall be made for a tray of sufficient capacity with a drainage system for ships having in way of bow loading coupler a spraying system precluding cargo spills propagation.

5.8.1.2 Remote-controlled valves shall comply with the requirements of 4.1.1.2 to 4.1.1.5, Part VIII "Systems and Piping".

5.8.2 Hydraulic systems.

5.8.2.1 Hydraulic systems shall comply with the requirements of 7.3, Part IX "Machinery".

5.8.2.2 Hydraulic accumulators shall be located in the space not communicating with the hazardous spaces as specified in 5.3.1.

5.8.2.3 Hydraulic accumulators shall be provided with devices capable of being manually activated when driving energy disappears.

5.8.2.4 Design of the hydraulic drive of the bow loading coupler and chain stopper shall prevent its opening when driving energy disappears.

5.8.2.5 The possibility of manual disconnection of bow loading coupler from the terminal cargo hose in case of hydraulic system failure shall be provided from the local station.

5.9 SOUNDING ARRANGEMENTS AND AUTOMATION

5.9.1 Cargo control during BLS operation shall be realized from BLS control station that may be located

either in the wheelhouse or in a specially equipped room in the fore part of the ship.

The control station shall be equipped with all necessary monitoring and control instruments to carry out all operations for ship positioning and monitoring of the ship mooring and loading parameters.

Where the BLS control station is located in the fore part of the ship, the requirements of 5.10.2 and 5.12 shall be met.

5.9.2 To provide ship positioning the BLS control station shall be equipped with the following:

.1 control system for the controllable pitch propellers of the main propulsion plant (if any);

.2 thrusters control system;

.3 main engine(s) emergency shutdown arrangement;

.4 steering gear(s) control system;

.5 radar display;

.6 log display;

.7 device for monitoring of dynamic positioning system parameters (if any).

5.9.3 To provide monitoring of ship mooring parameters the BLS control station shall be equipped with the following:

.1 devices for indication and logging by recording device (if any) of hawser and cargo hose tension with actuation of alarm for maximum value;

.2 devices for indication and logging by recording device (if any) of chain tension in chain stopper.

5.9.4 To provide monitoring of ship loading parameters the BLS control station shall be equipped with the following:

.1 device for indication of bow loading coupler position;

.2 device for cargo system valves position indication;

.3 device for cargo tanks level indication and high level alarm;

.4 device for cargo pipe pressure indication at BLS inlet;

.5 device for signal transmission from ship to terminal for cargo pump stop and cargo valve closing on the terminal.

5.9.5 Bow loading coupler, chain stopper, cargo system valves shall be provided with position indicators (open-closed).

5.9.6 BLS control system shall provide blocking of the bow loading coupler inlet valve from being opened until receiving a confirmation that the following actions have been carried out:

.1 terminal cargo hose is properly connected to the bow loading coupler;

.2 sufficient number of ship cargo system valves and BLS cut-off valve are opened, oil tanker is ready for loading the cargo.

5.9.7 BLS control system shall provide blocking of the bow loading coupler inlet valve from being opened in case of BLS mooring arrangement blackout or failure.

5.9.8 Quick-acting emergency shutdown system (ESD) shall be provided for the bow loading coupler. ESD shall provide two operating modes:

.1 first emergency shutdown mode (ESD-1) which shall provide the following:

giving a signal for cargo pump stop on the terminal;

closing the bow loading coupler inlet valve and the terminal discharge valve upon receipt of a signal of emergency pressure drop at ship cargo system inlet;

.2 second emergency shutdown mode (ESD-2) which shall provide the following:

giving a signal for cargo pump stop on the terminal;

closing the terminal discharge valve, the bow loading coupler inlet valve and the BLS cut-off valve upon receipt of a signal of emergency pressure drop at ship cargo system inlet;

disconnection of bow loading coupler;

opening of chain stopper.

ESD-1 and ESD-2 commands shall be given from the BLS control station by means of appropriate controls (buttons, switches). After issuing the command the execution of all the above mentioned functions shall be performed sequentially in automatic mode.

Where ESD-1 mode is deactivated before the above mentioned sequence of operations has been carried out, the operations shall be completed automatically. In this case the bow loading coupler inlet valve and the BLS cut-off valve shall be fully closed.

Where ESD-2 mode is deactivated before the above mentioned sequence of operations has been carried out, the operations shall be immediately interrupted except for the bow loading coupler inlet valve and the BLS cut-off valve which shall be fully closed.

Controls for activation of ESD-1 and ESD-2 modes shall be protected from unauthorized use.

5.9.9 Additionally to automatic system specified in 5.9.7, provision shall be made for back-up manual system of emergency disconnection of bow loading coupler by means of which the independent operations for releasing the chain stopper and the locking arrangement of the bow loading coupler shall be provided.

5.9.10 The sequence and time of cargo operations in the emergency disconnection mode shall ensure minimum cargo leakage and preclude the hydraulic shock in the cargo pipeline.

The time of closing of the bow loading coupler inlet valve and the BLS cut-off valve shall be at least 25 s both in automatic and manual modes. The shorter time of closing shall be proved by the calculation confirming the absence of possibility of hydraulic shock in the cargo pipeline.

5.10 FIRE PROTECTION

5.10.1 Boundaries of spaces where BLS cargo system equipment is located shall comply with the requirements of 2.4, Part VI "Fire Protection".

5.10.2 BLS control station in the fore part of the ship shall comply with the following requirements:

.1 BLS control station shall be of "A-60" class boundaries;

.2 maintenance of surplus pressure shall be provided in the space;

.3 an emergency exit from the space shall be provided.

5.10.3 Fire-fighting equipment and systems shall comply with the requirements of Section 3, Part VI "Fire Protection".

5.10.4 The area where BLS cargo and mooring arrangements are located shall be protected by the foam fire extinguishing system independent from the main system.

5.11 ELECTRICAL EQUIPMENT

5.11.1 Electrical equipment shall comply with the requirements of Part XI "Electrical Equipment".

5.11.2 Electrical equipment fitted in the hazardous areas shall comply with the requirements 2.9, 2.10, 19.2.3 and 19.2.4, Part XI "Electrical Equipment".

5.11.3 Lighting of the loading area and the boundary along it shall provide efficient visual monitoring of the mooring arrangement, cargo hose connection, cargo hose and water surface around.

5.12 COMMUNICATIONS

5.12.1 Where the BLS control station is located in the fore part of the ship, provision shall be made for two-way internal communications between the wheelhouse and the cargo control room in accordance with 3.3.2, Part VII "Machinery Installations" and 7.2, Part XI "Electrical Equipment".

5.12.2 Two-way communications shall be provided between the BLS control station and the terminal.

5.12.3 Emergency communications shall be provided between the BLS control station and the terminal.

5.12.4 Provision shall be made for direct and indirect means enabling to check communications between the

BLS control station and the terminal in case of failures and faults during cargo operations.

Whether the surveyor to the Register shall attend the first cargo operations on board the other ships of the series shall be determined proceeding from the BLS tests on board the prototype ship.

5.13 TESTS

5.13.1 All BLS systems and components shall be tested after their installation onboard in accordance with the programs approved by the Register.

5.13.2 The first cargo operation on the prototype ship of the series using BLS shall be carried out in the presence of the surveyor to the Register. At that the BLS operation for the purpose specified shall be checked in accordance with the operating manual.

5.14 RECORDS

5.14.1 The following records are issued on the basis of application of the requirements of the present Section:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark BLS-SPM, BLS or SPM in the class notation;

.2 Report on Survey of the ship (form 6.3.10).

6 REQUIREMENTS FOR HELICOPTER FACILITIES

6.1 GENERAL

6.1.1 Application.

6.1.1.1 Requirements for helicopter facilities are additional to those of Part I "Classification", Part II "Hull", Part III "Equipment, Arrangements and Outfit", Part VI "Fire Protection", Part VIII "Systems and Piping", Part XI "Electrical Equipment" of the Rules for the Classification and Construction of Sea-Going Ships and Part IV "Radio Equipment" of the Rules for the Equipment of Sea-Going Ships.

6.1.1.2 Ships and fixed offshore platforms (herein-after referred to as "ships" for the present Section) complying with the requirements of the present Section may be assigned with the following distinguishing marks added to the character of classification:

.1 HELIDECK — for ships fitted with helidecks and complying with the requirements specified in 6.2, 6.3, 6.4.1, 6.6 and 6.7;

.2 HELIDECK-F — for ships fitted with the helicopter refuelling facilities and complying with the requirements specified in 6.4.2 (as applicable), 6.5.1 and 6.5.2 (as applicable) in addition to those of 6.1.1.2.1;

.3 HELIDECK-H — for ships fitted with a hangar and complying with the requirements of the present Section in a full scope.

6.1.1.3 Distinguishing marks **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** may be assigned to ships under construction and in service.

6.1.1.4 Ships shall also meet the requirements of International Civil Aviation Organization (ICAO) and the Flag State (if any) for ensuring safe operation of helicopters which shall be confirmed by the relevant statement or certificate issued by the appropriate Civil Aviation Authority.

6.1.2 Definitions.

Hangar is a purpose-built space for helicopter storage and/or maintenance and repair.

Helideck is a purpose-built helicopter take-off and landing area including all structures, fire-fighting appliances and other equipment necessary for the safe operation of helicopters.

Helicopter facility is a complex of technical means including a helideck, helicopter refuelling facilities and compressed gas or special liquid filling facilities (if any), as well as hangars and spaces where helicopter maintenance facilities are located (if any).

Final approach and take-off area (FATO) is a defined area over which the final phase of the approach manoeuvre to hover or landing of the helicopter is intended to be completed and from which the take-off manoeuvre is commenced.

Touchdown and lift-off area (TLOF) is a dynamic load-bearing area on which a helicopter may touchdown or lift off. For a helideck it is presumed that the FATO and the TLOF will be coincidental.

6.1.3 Technical documentation.

6.1.3.1 The following technical documentation shall be submitted to the Register for approval (as applicable) to assign distinguishing marks **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** in the class notation:

.1 helideck and hangar deck plans with indication of design loads;

.2 scantlings determination of helideck and hangar deck, as well as of deck- and bulkhead stiffeners in way of helicopter tie-down points;

.3 general arrangement plan of a helicopter facility elements with indication of escape routes, tie-down points, location of fire-fighting equipment and life-saving appliances, arrangement plan and specification of lighting and illumination means;

.4 drawing of helideck safety net;

.5 diagram of power driving gear for the helideck safety net hoisting and lowering, if any;

.6 diagram of helideck drainage system;

.7 diagram of fuel oil loading, transfer, storage and helicopter refuelling system;

.8 diagram of off-grade aviation fuel collection, storage and defueling system;

.9 diagram of nitrogen system for aviation fuel;

.10 electric diagram of main and emergency lighting in the spaces of helicopter facility arrangement;

.11 circuit diagram of helideck lighting and illumination means;

.12 drawings of electrical equipment layout and cable laying on the helideck, in hangar and in other spaces of helicopter facility arrangement;

.13 documentation on helideck and hangar deck covering;

.14 helicopter facility test program;

.15 diagram of obstacle restriction and removal approved by the Flag State Civil Aviation Authority (to be submitted for information);

.16 drawing of helideck and obstacle marking (colour, dimensions and configuration of marks shall be indicated), approved by the Flag State Civil Aviation Authority (to be submitted for information).

6.1.3.2 Helicopter facility operation manual containing equipment description, a checklist of inspections, guidance for the safe operation and equipment maintenance procedures shall be provided on board. This operation manual shall also contain the procedures and precautions to be followed during helicopter refuelling

operations developed in accordance with the recognized safe practices.

For mobile offshore drilling units (MODU) and fixed offshore platforms (FOP) this operation manual can be included in the operating manual to be developed in compliance with the requirements of Chapter 14 of the Code for the Construction and Equipment of Mobile Offshore Drilling Units, 2009.

6.1.3.3 The Register may require additional documents to those listed in 6.1.3.1 proceeding from the ship design features.

6.2 HELIDECK DESIGN

6.2.1 Helideck arrangement with regard to provision of horizontal and vertical sectors for helicopter approach, landing and take-off shall comply with the requirements of ICAO and the Flag State (if any).

6.2.2 Helideck arrangement shall provide:

- .1 free helicopter approach to helideck;
- .2 safety of helicopter take-off and landing operations and maintenance personnel;
- .3 helideck location at a maximum possible distance from the ship's hazardous spaces and areas.

6.2.3 Helideck may have any configuration in plan view, generally, circle or regular polygon. In any case FATO shall be of sufficient size to contain an area within which can be drawn a circle of diameter not less than D of the largest helicopter the helideck is intended to serve, where D is the largest dimension of the helicopter when the main and tail rotors are turning.

6.2.4 If the helideck forms the ceiling of a deckhouse or superstructure it shall be of "A-60" class.

6.2.5 Helideck shall be made of steel. Aluminum alloys may be used provided the following:

- .1 a helideck, irrespective of its type and location, shall be subject to a survey in case of fire on the helideck or in close proximity;
- .2 if a helideck is located above the deckhouse or similar structure, the following conditions shall be additionally satisfied:

.2.1 the deckhouse top and bulkheads below the helideck shall have no openings;

.2.2 windows below the helideck shall be provided with steel covers.

.3 surfaces of the steel and aluminium alloy structures contacting at the point of connection and exposed to sea water shall be separated by gaskets made of non-absorbent electrically insulating material. Bolts, nuts and washers connecting the steel and aluminium structures shall be made of stainless steel. Bolts shall be installed in the bushes made of non-absorbent electrically

insulating material which structure shall exclude the contact of aluminium alloy and steel. The aluminium alloy structure insulated from the steel structure shall be grounded to the ship's hull;

.4 bimetal materials shall be approved by the Register, and certificates shall be issued for them by the Register.

6.2.6 Helideck on FOP shall be sloping or prominent for drainage to avoid accumulation of rain water and fuel spills on FATO surface. Inclination of these sloping or prominent surfaces shall be about 1:100. Sagging of helideck surface induced by helicopter at rest shall not lead to accumulation of fuel spills on FATO surface.

6.2.7 Helidecks and helicopter refuelling areas shall be clearly marked and provided with coamings and/or gutters to prevent fuel oil leakage from spreading.

6.2.8 Design of the helideck being the upper deck or superstructure or deckhouse shall comply with the following requirements:

.1 deck longitudinals shall be installed parallel to the helicopter axis at the take-off and landing;

.2 thickness of deck plating, section modulus and web cross-sectional area of longitudinals and beams shall be determined according to 3.2.4.1 – 3.2.4.3, Part II "Hull" at Q determined as per Formula (3.2.3.4) of Part II "Hull" and l_a and l_b equal to 0,3 m. In Formula (3.2.3.4) Q_0 shall be taken equal to the maximum take-off weight of the helicopter, $k_d = 3$, $n_0 = 2$, $n = 1$;

.3 scantlings of deep members and pillars as well as thickness of deck plating for the helicopter having skid instead of wheels shall be determined by direct calculation.

6.2.9 Helideck not being a part of the upper deck or superstructure or deckhouse shall comply with the following requirements:

.1 the plating thickness, section modulus and web cross-sectional area of longitudinals and beams shall be determined according to 6.2.8 of this Part and 2.12 of Part II "Hull" both for the short superstructure deck or deckhouse of the relevant tier;

.2 dimensions of stanchions and struts shall be determined according to 2.9 of Part II "Hull" as for the pillars;

.3 dimensions of beams, stanchions and struts shall be determined with due regard to inertia force from the deck structure weight. Accelerations for determination of inertia forces shall be determined as per 1.3.3.1 and 1.3.4.4 of Part II "Hull";

.4 aluminium alloys may be used. Strength and stability of helidecks from aluminium alloys may be determined by the model tests to be conducted in the presence of the Register representative according to the approved program.

6.3 EQUIPMENT OF HELIDECKS

6.3.1 The helideck surface shall be smooth, no steps or recesses in FATO are generally allowed. As an exception, the steps on the FATO perimeter line (outside the helideck white perimeter line) shall not exceed 250 mm in height, and within the FATO (within the helideck white perimeter line) shall not exceed 25 mm in height. Objects the function of which requires that they be located on the helideck within the FATO shall only be present provided they do not cause a hazard to helicopter operations.

As an exception, for ships which keels are laid before 1 January 2012, the steps within the FATO of height not exceeding 60 mm with the edge slop 1/3 are allowed.

6.3.2 The helideck, including its marking, and hangar deck shall have a skid-resistant surface.

6.3.3 For helicopter operation in winter period easily detachable rope net, rather of natural fiber (sisal), diameter of 20 mm and maximum mesh dimensions 200 × 200 mm, shall be provided along the perimeter of the FATO.

Recommended dimensions of the net, depending on the overall helicopter length, are determined by sufficiency to cover the landing area:

- 6 × 6 m at helicopter length less than 15 m;
- 12 × 12 m at helicopter length from 15 to 20 m;
- 15 × 15 m at helicopter length more than 20 m.

The net shall be reliably secured to the deck along the FATO perimeter and fixed to it in any 1,5 m and shall be tightened with a load not less than 2225 N.

The dismantled net shall be kept onboard.

6.3.4 Outboard edges of the helideck shall be provided with fixed or hinged safety net of at least 1,5 m in width, made of fire-resistant flexible material.

For MODU and FOP, as well as for sea-going ships, which keels are laid before 1 January 2012, outboard edge of the fixed safety net shall not rise above the plane of FATO more than 0,25 m, and the net shall be inclined upwards at an angle of at least 10°.

For MODU and FOP, as well as for sea-going ships, which keels are laid on and after 1 January 2012, outboard edge of the fixed safety net shall not rise above the plane of FATO, and the net shall be inclined upwards at an angle of at least 10°.

Hinged safety net in tumble position shall comply with the same requirements.

The safety net shall be strong enough to withstand, without damage, a 75 kg mass being dropped, and the net shall provide hammock effect for person falling into it rather than the trampoline effect produced by some rigid materials.

6.3.5 In addition to the requirements of **6.3.4** the hinged safety net shall comply with the following requirements:

.1 safety net shall be reliably secured in a hoist position;
.2 safety net shall be reliably fixed in a hinged position so as to prevent its hoist due to the effect of airflow from the helicopter rotor;

.3 safety net hoisting and lowering shall be performed so as to minimize the risk of personnel falling overboard during the operations;

.4 any failure of power driving gear for safety net hoisting shall not prevent from its lowering by hand.

6.3.6 To minimize the risk of personnel or equipment sliding from the helideck, the outboard edges of the helideck shall have coamings of recommended height of 50 mm. The coamings shall also meet the requirements of **6.2.7**.

6.3.7 The helideck in way of helicopter parking place and maintenance areas, as well as the hangar (if any) shall be equipped with the tie-down points and means for fastening of helicopter maintenance facilities (if any), flush type is preferable. Connection dimensions, arrangement plan and design forces of tie-down points shall be selected for fastening of one or several types of helicopter taking into account the requirements of **6.3.1**.

6.3.8 Where handrails associated with access/escape points exceed the elevation of the FATO by more than 0,25 m, they shall be made collapsible and removable. They shall be collapsed or removed whilst helicopter manoeuvres are in progress.

6.4 FIRE PROTECTION

6.4.1 Fire protection of helidecks.

6.4.1.1 The helideck shall be provided with both main and emergency means of escape and access for fire-fighting and rescue personnel. These shall be located as far apart from each other as practicable, and preferably on the opposite sides of the helideck.

If more than 50 per cent of the helideck area is projected from the main ship structure, it is recommended to arrange two entrances to helideck within the range of such overhanging parts that is providing at least one exit from helideck to windward side in case of fire.

6.4.1.2 Helideck shall be protected by a fixed foam fire extinguishing system according to item 20 of Table 3.1.2.1 of Part VI "Fire Protection".

The minimum capacity of the foam production system depends upon the size of the area to be protected and the foam consumption rate, the minimum foam application rate shall be not less than 6 l/min/m² within a circle having a diameter equal to at least the *D*-value.

Amount of foam concentrate shall provide a minimum of 5 min discharge capability of a circle having a diameter equal to the *D*-value.

Foam delivery at the minimum application rate shall start within 30 s of system activation.

The foam concentrate shall be suitable for use with seawater and meet the requirements not inferior to those, which are adopted by ICAO.

The location and characteristics of the equipment of the foam fire extinguishing system shall provide extinguishing of fire on helicopter high-level units.

It is recommended to provide additionally 100 % reserve of foam concentrate for supply of its calculated value in case of helicopter landing after partial use of foam concentrate in testing, drills or fire extinction.

6.4.1.3 The number and position of fire hydrants shall be such that at least two jets of water may reach any part of the helideck.

6.4.1.4 In close proximity to the helideck the following fire-fighting outfit shall be provided and stored near the means of access to that helideck:

.1 at least two dry powder fire extinguishers having a total capacity not less than 45 kg;

.2 carbon dioxide fire extinguishers having a total capacity not less than 18 kg or equivalent; fire extinguishers shall be equipped with flexible nozzles for extinguishing a fire in the upper part of a helicopter;

.3 at least two nozzles of an approved dual-purpose type with hoses sufficient to reach any part of the helideck;

.4 at least two sets of fireman's outfits in addition to those required by item 10 of Table 5.1.2, Part VI "Fire Protection";

.5 at least the following equipment stored to provide its immediate use and protection from weather exposure:

- adjustable wrench;
- blanket (fire-resistant);
- cutter for bolts with at least 60 cm handle;
- hook, grab or salving;
- hacksaw, heavy duty, complete with 6 spare blades;
- ladder;
- lifeline of 5 mm in diameter and 15 m in length;
- pliers, side-cutting;
- set of assorted screwdrivers;
- harness knife complete with sheath;
- crowbar;
- 3 pairs of fireproof gloves (recommended);
- rescue axe of non-blocking type (recommended);
- universal shears or equivalent cutting tool (recommended).

6.4.1.5 Drainage facilities in way of helidecks shall be constructed of steel or other arrangements providing equivalent fire safety; lead directly overboard independent of any other system; and designed so that drainage does not fall onto any part of the unit.

6.4.2 Fire protection of hangars and spaces where helicopter refuelling and maintenance facilities are located.

6.4.2.1 Structural fire protection, fixed fire extinguishing systems and fire detection and alarm systems and fire-fighting outfit for hangars and spaces where helicopter

refuelling and maintenance facilities are located shall be similar to those of category A machinery spaces.

6.4.2.2 The boundary structures of hangars and spaces where helicopter refuelling and maintenance facilities are located shall be made of steel.

6.4.2.3 Refuelling station for helicopters shall meet the following requirements:

.1 the boundaries and means of closing openings at the station shall secure gas tightness thereof. Doors leading to the station shall be of steel;

.2 deck covering shall preclude spark formation. Arrangements and machinery shall be so arranged and located as to exclude the possibility of spark formation;

.3 pipelines and cables passing through the boundaries of the station shall not cause loss of its gas tightness;

.4 storage tank fuel pumps shall be provided with means which permit remote shutdown from a safe location in the event of a fire. Where a gravity-fuelling system is installed, equivalent closing arrangements shall be provided to isolate the fuel source;

.5 where several fuel tanks are fitted, the fuel system design shall provide for fuel supply to the helicopter being refuelled only from one tank at a time;

.6 provision shall be made for the arrangement whereby a fuel spillage may be collected and drained into an off-grade fuel tank;

.7 fuel oil piping shall be of steel or equivalent material, as short as possible, and protected against damage;

.8 the refuelling facility shall incorporate a metering device to record the quantity of supplied fuel, a flexible hose with a nozzle fitted with a self-closing valve and a device to prevent over-pressurization of the fuel system.

6.4.2.4 The number and position of the hydrants shall be such that at least three jets of water may reach any part of the hangar.

6.4.2.5 "NO SMOKING" signs shall be displayed at appropriate locations in hangars and spaces where helicopter refuelling and maintenance facilities are located.

6.4.2.6 Storage of flammable liquids and materials, paint materials, lubricating oils, hydraulic liquids and any types of fuel in hangar is not allowed.

6.5 SYSTEMS AND PIPING

6.5.1 Helicopter refuelling systems.

6.5.1.1 Shipboard helicopter refuelling system shall comply with the requirements actual in the Civil Aviation of Flag State in part of bunkering, storage, cleaning, quality control and fuel filling. Refuelling facilities shall be certified (approved) for compliance with the requirements of the Flag State aviation regulations.

6.5.1.2 All the equipment used in refuelling operations shall be effectively earthed. All the equipment, arrangements, machinery and deck coverings shall be manufactured and installed so as to prevent spark formation.

6.5.1.3 As a rule, tanks used for storage of helicopter fuel shall be located on the open deck in specially designed area, which shall be:

.1 as remote as practicable from accommodation and machinery spaces, escape routes and embarkation stations, as well as from locations containing sources of ignition;

.2 isolated from areas containing sources of vapour ignition;

.3 the fuel storage area shall be provided with arrangements whereby fuel spillage may be collected and drained to off-grade fuel tank;

.4 where tanks for storage of helicopter fuel and off-grade fuel tanks are located in enclosed spaces, such tanks shall be surrounded by cofferdams filled with inert gas;

.5 in cofferdams referred to in 6.5.1.3.5 the length of oil fuel line and the number of its detachable joints shall be kept to a minimum, and its valves shall be located in easily accessible places, generally, on the open deck;

.6 cofferdams referred to in 6.5.1.3.4 shall not be connected to any piping system serving other spaces.

6.5.1.4 Provision shall be made for fuel jettisoning from tanks of the helicopter located on the helideck or in hangar to the off-grade fuel tank. Provision shall be made for off-grade fuel delivery to the shore or ship's tanks.

6.5.1.5 Tanks used for storage of helicopter fuel and associated equipment shall be protected against physical damage and from a fire in an adjacent space or area. Tanks shall be protected against direct sunrays.

6.5.1.6 When equipping tanks for the storage of helicopter fuel with facilities for their emergency jettisoning precautions shall be taken to prevent the tank jettisoned from impact against ship's structures. The tanks shall be as remote as practicable from survival craft muster and embarkation stations and survival craft launching stations.

6.5.1.7 The fuel tanks shall be made of materials which resist attacks by corrosion and helicopter fuel.

Fuel may be stored both in transported and fixed tanks.

Tanks shall be efficiently secured, closed and bonded. The tanks shall be readily accessible for inspection.

Tanks and piping for anti-crystallization fluids shall be made of stainless steels.

6.5.1.8 Each fuel oil tank shall be fitted with filling, outlet, sounding and air pipes. The end of a filling pipe shall not be more than 300 mm above a tank bottom. It is recommended to use closed-type flow-meters. The

sounding pipe shall end 30 to 50 mm above a tank bottom and shall be laid to the open deck.

6.5.1.9 Air pipes of fuel oil tanks shall be laid to a height of at least 2,4 m above the open deck. Open ends of air pipes shall be spaced at a distance of at least 10 m from air in-takes and openings of enclosed spaces with ignition sources, and from a deck machinery and equipment, which may present an ignition hazard, and shall be fitted with flame-arresting meshes or other fittings approved by the Register.

6.5.1.10 A fuel oil pump shall take in fuel oil simultaneously from one tank only. Pipelines shall be made of steel or equivalent material, shall be short (where possible) and shall be protected against damages.

6.5.1.11 Fuel oil pumps shall be provided with shutdown means positioned in a remote safe place. Service tanks shall be provided with quick-closing valves driven from outside the tank area.

6.5.1.12 All pipelines and equipment of the system for bunkering, storage and fuelling shall be electrically continuous and shall be earthed to the ship hull.

6.5.1.13 Fuel pipelines shall have no stagnant sections. Where it is structurally impossible to avoid stagnant sections, provision shall be made for pipe drainage by means of nitrogen purging or another way of pipeline emptying. The lower parts of piping system shall be provided with drain cocks to remove sediment to off-grade fuel tank.

6.5.1.14 Helicopter refuelling system shall be so designed as to provide free access for its maintenance, fuel sampling and repair.

6.5.2 Ventilation system of hangars and spaces where helicopter refuelling and maintenance facilities are located.

6.5.2.1 Hangars and spaces where helicopter refuelling and maintenance facilities are located shall be provided with mechanical exhaust ventilation sufficient to give at least 10 air changes per hour. Fans shall be of flameproof design and shall meet the requirements of 5.3.3, Part IX "Machinery" and 19.3.4, Part XI "Electrical Equipment".

6.6 ELECTRICAL EQUIPMENT

6.6.1 Electrical equipment and electric wiring of hangars and spaces where helicopter refuelling and maintenance facilities are located shall comply with the requirements of 2.9, Part XI "Electrical Equipment".

6.6.2 Lighting and illumination means for helidecks shall comply with the requirements of 6.9, Part XI "Electrical Equipment" of the Rules for the Classification and Construction of Sea-Going Ships and the Flag State Civil Aviation requirements.

6.7 COMMUNICATIONS

6.7.1 To ensure helicopter operation the ship shall be equipped with necessary radio and meteorological equipment in compliance with the Flag State Civil Aviation requirements.

6.8 TESTS

6.8.1 All systems and components of the helicopter facility when installed onboard shall be tested according to the programs approved by the Register.

6.8.2 Upon request of the Flag State Civil Aviation flight trials and/or test flights may be performed on ships in compliance with the Flag State regulatory documents.

6.9 RECORDS

6.9.1 As a result of applying the requirements of the present Section the following records will be issued:

.1 Classification Certificate (form 3.1.2) with the distinguishing mark **HELIDECK**, **HELIDECK-F** or **HELIDECK-H** in the class notation;

.2 Report on Survey of the Ship (forms 3.1.2 and 3.1.2P).

7 REQUIREMENTS FOR SHIP EQUIPMENT TO ENSURE LONG-TERM OPERATION AT LOW TEMPERATURE

7.1 GENERAL

7.1.1 Application.

7.1.1.1 The requirements for ship equipment and FOP (hereinafter for this Section referred to as "the ships") to ensure long-term operation at low temperature apply to ships intended for operation in cold climatic conditions, including the Gulf of Saint Lawrence, northern part of the Baltic Sea, the Arctic Ocean and Antarctic Seas, and are additional to the requirements of Part I "Classification", Part II "Hull", Part III "Equipment, Arrangements and Outfit", Part VII "Machinery Installations", Part VIII "Systems and Piping", Part IX "Machinery", Part XI "Electrical Equipment" and Part XIII "Materials" of the Rules for the Classification and Construction of Sea-Going Ships, Part II "Life-Saving Appliances", Part III "Signal Means", Part IV "Radio Equipment" and Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships, as well as the Rules for the Cargo Handling Gear of Sea-Going Ships.

7.1.1.2 For ships complying with the requirements of the present Section a distinguishing mark **WINTERIZATION(DAT)** may be added to the character of classification at the shipowner's request. Design ambient temperature shall be indicated in brackets, for example: **WINTERIZATION(−40)**.

7.1.1.3 The necessary conditions for assigning the distinguishing mark **WINTERIZATION(DAT)** are as follows:

.1 availability of ice class not less than **Arc4** in compliance with 2.2.3, Part I "Classification". At shipowner's request the distinguishing mark **WINTERIZATION(DAT)** may be assigned to ships of ice class **Ice3** and below, in this case the extent of compliance with the requirements of this Section shall be determined by the Register upon agreement with the shipowner considering the intended operational conditions and structural particulars of the ship;

.2 availability of the distinguishing mark **ANTI-ICE** for ships fitted with equipment for icing protection in compliance with Section 4.

7.1.1.4 The distinguishing mark **WINTERIZATION(DAT)** may be assigned to ships under construction and in service.

7.1.2 Definitions, explanations and abbreviations.

For the purpose of the present Section the following definitions, explanations and abbreviations have been adopted.

A c c o m m o d a t i o n s p a c e s are spaces complying with the requirements of 1.5.2, Part VI "Fire Protection".

P o l l u t a n t means any substance, which falls within the limits for marine disposal in compliance with MARPOL 73/78.

E n c l o s e d s p a c e is a space with a direct access to the open deck which is fitted with an appropriate closure.

IBC Code — International Code for the Construction and Equipment of Ships Carrying Dangerous Chemicals in Bulk;

LSA Code — International Life-Saving Appliances Code;

MARPOL 73/78 — International Convention for the Prevention of Pollution from Ships, 1973 and Protocol, 1978 thereto.

O p e n s p a c e is a space with a direct access to the open deck which is not fitted with closure or shall be kept open for long periods as regards operational conditions of equipment installed in this space.

D e s i g n a m b i e n t t e m p e r a t u r e (D A T) is the outside air temperature, in °C, used as the criterion for selection and testing of materials and equipment subject to low temperatures.

D e s i g n t e m p e r a t u r e o f t h e s t r u c t u r e is the temperature, in °C, assumed for choosing of construction material. When the Rules or this Section contain no additional provisions, the design ambient temperature is assumed as a design temperature of the structure.

W o r k i n g l i q u i d s mean fuel and lubricating materials, and hydraulic oils, except for marine fuel, necessary for normal operation of a ship and its equipment.

7.1.3 Technical documentation.

7.1.3.1 The following technical documentation shall be submitted to the Register for approval to assign the distinguishing mark **WINTERIZATION(DAT)** in the class notation:

.1 Manual on operation of ship at low temperature (**Winterization Manual**);

.2 one line diagrams of electric heating systems (electric heating appliances, systems utilizing heating cables);

.3 certificates for machinery, equipment, arrangements, outfit, foam concentrate specified in the present Section, confirming suitability of their use at design ambient temperature;

.4 test programs for the equipment intended for prolonged exposure to low service temperatures, specified in the present Section.

7.1.3.2 The following documents approved by the Register shall be available on board the ship:

.1 Manual on operation of ship at low temperature (**Winterization Manual**);

.2 Stability Booklet including loading cases considering icing;

.3 Damage Stability Booklet;

.4 Ice Ship Safety Certificate.

7.1.3.3 Technical documentation on products to be submitted for approval in addition to the Rules requirements is specified in the relevant Chapters of the present Section.

7.2 DESIGN TEMPERATURES

7.2.1 Design ambient temperature value is established by the shipowner according to the ship purpose and service conditions.

7.2.2 The following standard values of design ambient temperature are stipulated by the present Section: $-30\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION**(-30)); $-40\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION**(-40)); $-50\text{ }^{\circ}\text{C}$ (the distinguishing mark **WINTERIZATION**(-50)).

7.2.3 Design ambient temperature shall not be assumed above the temperature specified in 1.2.3.3 of Part II "Hull" for the appropriate ice class.

7.2.4 Design temperature of hull structures shall be assumed according to 1.2.3.4 of Part II "Hull". In this case, design ambient temperature shall be assumed as the value of T_A .

7.2.5 For equipment and machinery installed on the open decks, as well as in the open spaces, the design ambient temperature shall be assumed as design temperature of structures. For equipment and machinery installed in unheated enclosed spaces exposed to the environment and adjoining unheated adjacent enclosed spaces the design ambient temperature shall be assumed as the design temperature. For equipment and machinery installed in unheated enclosed spaces exposed to the environment and adjoining heated adjacent enclosed spaces the temperature of $20\text{ }^{\circ}\text{C}$ above the design ambient temperature shall be assumed as the design temperature of structure.

7.3 GENERAL REQUIREMENTS

7.3.1 Cargo and slop tanks of oil tankers of less than 5000 t deadweight shall be protected throughout the length by ballast tanks or compartments not intended for carriage of pollutants located in compliance with the requirements of regulation 19.6.1 (from the ship's bottom shell plating) and regulation 19.6.2 for the distance w (from the ship's side shell plating) of Annex I to MARPOL 73/78.

On ships other than oil tankers, all cargo tanks designed and intended for carrying oil shall be located at a distance of at least 0,76 m from the shell plating.

On chemical tankers type 3 as defined in 2.1.2 of the International Code for the Construction and Equipment

of Ships Carrying Dangerous Chemicals in Bulk (IBC Code), or NLS tankers, cargo tanks shall be located at a distance of at least 0,76 from the shell plating.

Location of cargo and slop tanks (if any) of chemical tankers relative to shell plating shall comply with the requirements of regulation 2.6 of the IBC Code depending on the ship's type. Therewith, for carriage of selected vegetable oils onboard the type 3 chemical tankers the requirements of regulation 4.1.3 of Annex II to MARPOL 73/78 shall be met. Other type 3 chemical tankers, as well as tankers intended for carriage of hazardous substances in bulk shall be fitted with cargo and slop tanks located at least at 760 mm distance from the shell plating.

7.3.2 For ships with aggregate capacity of fuel oil tanks less than 600 m^3 , all fuel oil tanks shall be located at a distance of at least 0,76 m from the shell plating. This requirement shall not apply to small fuel oil tanks with the capacity not exceeding 30 m^3 .

7.3.3 All oil residue (sludge) tanks, tanks intended for storage of working liquids and oily bilge water holding tanks shall be located at a distance of at least 0,76 m from the shell plating. This requirement shall not apply to such small tanks with the capacity not exceeding 30 m^3 .

7.3.4 In addition to the requirements of Annex I to MARPOL 73/78, each ship shall be fitted with oil residue holding tank(s) as well as oily bilge water holding tank(s) of sufficient capacity agreed with the Register, for the total retention on board of accumulated oil residues (sludge) and oily bilge water during voyages in polar waters and disposal to reception facilities.

7.3.5 Navigation bridge wings shall be closed.

Angles of view shall meet the requirements of 3.2, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships. Bridge front, rear and side windows (including wings) shall be inclined from the vertical plane top out, at an angle of not less 10° and not more than 25° .

7.3.6 Exit from corridors of accommodations to the open deck shall be arranged through the heated companions.

7.3.7 A heated deckhouse shall be provided as a shelter for crew while performing the following functions: observation of the environment during the ship's movement or using guards whilst in a port.

7.4 EQUIPMENT, ARRANGEMENTS AND OUTFIT

7.4.1 Anchor arrangement.

7.4.1.1 Materials for manufacture of anchor shall meet the requirements of Section 8, Part XIII "Materials".

7.4.1.2 Materials for manufacture of anchor chain shall meet the requirements of 7.12.7.

7.4.1.3 Materials of castings for manufacture of anchor hawse pipe shall meet the requirements of 7.12.4.

The Register certificates issued for anchor hawse pipes to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.1.4 Anchor stoppers shall meet the requirements of 3.6.1, Part III "Equipment, Arrangements and Outfit".

The Register certificates issued for anchor stoppers to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.2 Mooring appliances.

7.4.2.1 Materials of castings for manufacture of mooring bollards, fairleaders and other mooring appliances shall meet the requirements of 7.12.4.

The Register certificates issued for mooring appliances to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.2.2 Chain stoppers for single-point mooring to offshore terminals shall meet the requirements of 7.4.1.4.

7.4.3 Towing arrangement.

7.4.3.1 Materials of castings for manufacture of bitts, towing bollards, fairleaders, chocks, roller and other towing arrangement shall meet the requirements of 7.12.4.

The Register certificates issued for mooring appliances to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.3.2 Chains of emergency towing arrangement shall meet the requirements of 7.12.7.

7.4.4 Side scuttles.

7.4.4.1 Side scuttles of wheelhouse and cargo control room shall be provided with heating in compliance with 4.2.3.6 of the present Part.

7.4.4.2 Onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** the side scuttles with double glass shall be installed in accommodation spaces.

7.4.4.3 When the cargo deck is viewed through the side scuttles of master's cabin, at least one of these side scuttles shall be provided with heating.

7.4.4.4 External access or other equivalent means for cleaning of side scuttles of navigation bridge and cargo control room shall be provided.

7.4.5 Hatchways, shell doors, cargo doors.

7.4.5.1 Materials for manufacture of cargo hatch covers and hatchways of cargo tanks, shell doors, cargo doors, including seals shall meet the requirements of 7.12.1 to 7.12.6.

7.4.5.2 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.4.5.3 The Register certificates issued for cargo hatch covers and cargo tanks, shell doors, cargo doors to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.4.6 Signal means.

7.4.6.1 Manually operated flashing red light visible from astern to indicate when the ship is stopped shall be provided onboard. The flashing light shall have a range of visibility of at least 2 nautical miles. Construction and characteristics of the light shall meet the applicable requirements of 3.1.6 and 3.2.1, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships. Arc of visibility in horizontal and vertical plane shall be the same as for stern lights in compliance with 3.1.2, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships.

7.4.6.2 The light specified in 7.4.6.1 shall be effective at design ambient temperature or at the temperature stated in 3.1.3.3, Part III "Signal Means" of the Rules for the Equipment of Sea-Going Ships (whichever is lower).

7.5 STABILITY AND SUBDIVISION

7.5.1 The requirements of Parts IV "Stability" and V "Subdivision" shall be met.

7.5.2 The ship shall be provided with a reliable draught measurement system whereby the forward and aft draughts can be easily determined.

7.6 MACHINERY INSTALLATIONS

7.6.1 Propulsion plants of ice class ships with distinguishing marks **WINTERIZATION(–30)**, **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall be capable of maintaining rated power and required rated torque at propeller shafts in a range of rotation speed corresponding to the appropriate operating conditions and modes in accordance with the assigned ice class.

7.6.2 Means shall be provided to ensure that machinery may be brought into operation from the dead

ship condition without external aid, as well as storage and supply of fuel to the emergency diesel-generator with pour point temperature being 5 °C lower than design ambient temperature indicated in brackets of the distinguishing mark **WINTERIZATION(DAT)**. As an alternative, self-contained portable arrangements may be provided on board to ensure that machinery may be brought into operation from the dead ship condition.

7.6.3 Based on their design, the machinery, shafting, boilers and other pressure vessels, as well as pipelines of systems and fittings, shall remain operative during the ship stay at design ambient temperature.

7.6.4 Onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** air supply to main engines shall not lead to overcooling of machinery space. Technical means shall be provided to exclude increase of mechanical load on cylinders and pistons and bearings of main engines due to the harmful effect of reduced temperatures of scavenging air.

7.6.5 When environmentally hazardous refrigerants are used, the stern-tube seals shall be so designed as to prevent leakage out of the seal housing when operated within the specified modes. Permissible leakage of non-toxic and biologically neutral refrigerants are not considered as pollution from ships.

7.6.6 Technical means shall be provided for complete shaft line turning during the ship stay in close floating ice.

7.6.7 In general, at least two auxiliary boilers shall be provided onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)**.

7.6.8 In general, steel four-bladed propellers with detachable blades shall be used.

7.6.9 Ships shall be provided with technical means for replacing defective blades afloat.

7.7 SYSTEMS AND PIPING

7.7.1 Fittings, formed components, expansion joints.

7.7.1.1 Materials for manufacture of fittings, expansion joints and formed components of pipelines to be installed on the open decks, as well as in the open unheated spaces shall meet the requirements of 7.12.1 to 7.12.6.

For products and seals manufactured of rubber as well as materials of organic origin in fittings, cold endurance type tests may be replaced by checking the operability of assembled fittings in low temperatures. For this purpose, a sample of each standard sized valve shall be conditioned within 6 h at a temperature of 10 °C lower than design ambient temperature indicated in brackets of the distinguishing mark **WINTERIZATION(DAT)**. Immediately after removal from the refrigerating chamber, 10 cycles of closing and opening of the fittings shall

be made, after which hydraulic tests are carried out with working pressure at normal temperature.

7.7.1.2 The Register certificate issued for fittings, expansion joints and formed components of pipelines to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** and installed on the open decks, as well as in the open unheated spaces shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.7.1.3 Side fittings installed above the load water-line shall meet the requirements of 4.3.1.2 of "Systems and Piping".

7.7.2 Ballast and sewage systems.

7.7.2.1 Ballast system shall meet the requirements of 8.3.2, Part VIII "Systems and Piping".

7.7.2.2 Discharge pipeline of ballast system shall be provided with heating.

7.7.2.3 Where submerged electrically-driven ballast pumps are used, their serviceability at design ambient temperature shall be ensured and documented; and the relevant information shall be introduced into the certificates issued by the Register.

7.7.2.4 Hydraulic liquids used as working media for ballast pumps driving and remotely controlled fittings shall be suitable for use at design ambient temperature.

7.7.2.5 Sewage holding tanks and pipelines leading thereto shall be located in heated spaces or provided with heating.

7.7.3 Fire-fighting systems and outfit.

7.7.3.1 All fire pumps, including emergency fire pump, shall be located in compartments maintained above freezing. Where fixed water-based firefighting systems are located in a space separate from the main fire pumps and use their own independent sea suction, this sea suction shall be also capable of being cleared of ice accumulation.

7.7.3.2 Design of water fire main system and foam fire extinguishing system shall meet the requirements of 3.2 and 3.7, Part VI "Fire Protection" considering the requirements of 4.2.4.4.

7.7.3.3 A foam concentrate for foam fire extinguishing system shall be approved by the Register and be stored in the space with positive temperature.

7.7.3.4 Air-foam nozzles intended for installation onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall work properly at required design ambient temperature and shall have the relevant Register approval.

7.7.3.5 Fire hoses shall meet the requirements of 5.1.4, Part VI "Fire Protection" They shall be approved by the Register and be suitable for operation at design ambient temperature.

Fire hoses need not be connected to the fire main at all times, and may be stored in protected locations near the hydrants.

7.7.3.6 The fire extinguishers shall be located in positions protected from freezing temperatures, as far as practical. Locations subject to freezing shall be provided with fire extinguishers capable of operation under the polar service temperature according to 5.1.9.15.7, Part VI "Fire Protection".

7.7.3.7 The firefighter's outfits shall be stored in warm locations on the ship. The radio communication equipment shall be operable at the polar service temperature.

7.7.4 Systems of tankers and combination carriers.

7.7.4.1 Cargo system.

7.7.4.1.1 Where submerged electrically-driven ballast pumps are used, their serviceability at design ambient temperature shall be ensured and documented and the relevant information shall be introduced into the certificates issued by the Register.

7.7.4.1.2 Hydraulic liquids used as working media for ballast pumps driving and remotely controlled fittings shall be suitable for use at design ambient temperature.

7.7.4.1.3 The Register certificates issued for cargo hoses of oil and chemical tankers shall contain an indication whether it is allowed to use them at design ambient temperature.

7.7.4.2 Bow loading system.

7.7.4.2.1 Materials of components of the bow loading system shall meet the requirements of 7.12.1 to 7.12.6.

7.7.4.2.2 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.7.4.2.3 The Register certificates issued for bow loading system to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.7.4.3 Inert gas system.

7.7.4.3.1 Sea water supply pipeline for deck water seal, a gas scrubber and other equipment of inert gas system shall be fitted with heating.

7.7.5 Ventilation system.

7.7.5.1 In addition to the requirements of Section 12, Part VIII "Systems and Piping" the ventilation system shall meet the requirements of 4.2.4.3.

7.8 DECK MACHINERY

7.8.1 Materials used for manufacture of deck machinery components shall comply with the requirements of 7.12.1 to 7.12.6.

7.8.2 The Register certificates issued for deck machinery intended for installation onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication

whether it is allowed to use it at appropriate design ambient temperature.

7.8.3 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.9 LIFE-SAVING APPLIANCES

7.9.1 General requirements for life-saving appliances.

7.9.1.1 Life-saving appliances shall comply with the requirements of Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships; at that, they shall be in the operating condition when stored at design ambient temperature.

7.9.1.2 The Register certificates issued for life-saving appliances intended for ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.9.1.3 Life-saving appliances intended for ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall be marked **W(–40)** and **W(–50)** accordingly.

7.9.1.4 Sufficient emergency rations for the maximum expected time of rescue shall be provided onboard.

7.9.2 Lifeboats.

7.9.2.1 Lifeboats shall be of an enclosed type and shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 a lifeboat shall provide accommodation for a specified number of persons in warm clothes with personal survival kits stipulated by 7.9.6.2;

.2 a lifeboat keel shall be provided with additional strip of steel or other equivalent material to protect the keel from contact with ice; adequate protection is allowed;

.3 a lifeboat engine shall be equipped with a means for its cold start at design ambient temperature within 2 min from the start; a starter shall be driven from two independent sources of power;

.4 cooling system of a lifeboat engine shall ensure its operation at design ambient temperature;

.5 a lifeboat propeller shall be properly protected from damage by ice;

.6 lifeboat engine fuel oil and oils used shall provide engine safe operation at design ambient temperature;

.7 a lifeboat cockpit shall be electrically heated;

.8 lifeboat scuttles which provide the required visibility from a control station shall be heated;

.9 prior to launching, a lifeboat shall be fitted with a two-way VHF radiotelephone apparatus in compliance with the requirements of 12.2 or 12.3, Part IV "Radio

Equipment" of the Rules for the Equipment of Sea-Going Ships; apparatus shall be operable at appropriate design ambient temperature;

.10 drinking water shall be stored in containers that allow for expansion due to freezing;

.11 a lifeboat shall be additionally supplied with a food ration in the quantity equal to 30 per cent of the ration required by the LSA Code to account for high rates of energy expenditure under cold conditions;

.12 a lifeboat on-load release mechanism shall be provided with heating or other measures ensuring safe actuation of a release mechanism at design ambient temperature shall be taken;

.13 a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of 4.2.3.12 shall be available in the vicinity of a lifeboat as additional means;

.14 immersion suits shall be of the insulated type.

7.9.3 Rescue boats.

7.9.3.1 Rescue boats shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 only rigid rescue boats shall be used;

.2 safe starting of the engine at design ambient temperature shall be provided;

.3 rescue boat engine fuel oil and oils used shall provide engine safe operation at design ambient temperature;

.4 prior to launching, a rescue boat shall be fitted with a two-way VHF radiotelephone apparatus in compliance with the requirements of 12.2 or 12.3, Part IV "Radio Equipment" of the Rules for the Equipment of Sea-Going Ships; apparatus shall be operable at appropriate design ambient temperature.

7.9.4 Liferafts.

7.9.4.1 Liferafts shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 inflation of a liferaft shall be completed within 3 min at design ambient temperature;

.2 containers of inflatable liferafts and hydrostatic release units shall be provided with heating or other measures to ensure ease launching, inflation and release of liferafts at design ambient temperature shall be taken;

.3 a manual inflation pump that is proven to be effective at design ambient temperature shall be stored in a heated space in the vicinity of the inflatable liferaft;

.4 liferafts shall be additionally supplied with a food ration in the quantity equal to 30 per cent of the ration required by the LSA Code to account for high rates of energy expenditure under cold conditions;

.5 a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of 4.2.3.12 shall be available in the vicinity of the liferafts as a secondary means.

7.9.5 Launching appliances of lifeboats, rescue boats and liferafts.

7.9.5.1 Launching appliances of lifeboats, rescue boats and liferafts shall comply with the following additional requirements with regard to Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships:

.1 materials used for their manufacture shall comply with the requirements of 7.12.1 to 7.12.6;

.2 hydraulic liquids and lubricating oils used in launching and embarkation appliances shall be suitable for use at design ambient temperature;

.3 electric motors and winches of launching appliances, automatic release hook shall be provided with heating or removable covers; if heating is not provided, a suitable icing removal mallet or another tool for ice accretion removal complying with the requirements of 4.2.3.12 shall be available in the vicinity of the launching appliance as a secondary means;

.4 electric motors, hydraulic drives, winches, brakes and other components of the launching appliance shall be effective at design ambient temperature, their operability shall be confirmed by appropriate testing;

.5 drums with falls, sheaves, winches, winch brakes and other components of the equipment engaged in launching shall be provided with heating or other measures ensuring safe launching of survival craft and rescue boats at design ambient temperature shall be taken.

7.9.6 Group and personal survival kits.

7.9.6.1 In addition to the equipment listed in Section 6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships, group and personal survival kits shall be provided.

Personal survival kits (PSK) complying with the requirements of 7.9.6.2 shall be carried onboard the ship with a distinguishing mark **WINTERIZATION(DAT)** in the class notation whenever a voyage is expected to encounter mean daily temperatures below 0 °C.

Group survival kits (GSK) complying with the requirements of 7.9.6.4 shall be carried onboard the ship with a distinguishing mark **WINTERIZATION(DAT)** in the class notation whenever a voyage is expected to encounter ice conditions which may prevent the launching and operation of survival craft.

Sufficient number of group and personal survival kits (as applicable) shall be carried to cover at least 110 per cent of the rated complement of the ship.

7.9.6.2 A personal survival kit shall be stored so that it may be easily retrieved in an emergency situation (in cabins or in dedicated lockers near muster and embarkation stations).

A personal survival kit shall consist of the following items:

.1 clothing;

head protection — 1 (vacuum packed);

neck and face protection — 1 (vacuum packed);
 hand protection — mitts — 1 pair (vacuum packed);
 hand protection — gloves — 1 pair (vacuum packed), if they are not permanently attached to thermal protective aid;

foot protection — socks — 1 pair (vacuum packed);

foot protection — boots — 1 pair;

personal thermal protective aid complying with the requirements of 6.6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships — 1;

approved immersion suit — 1 (not required, if an immersion suit is provided for every person onboard in compliance with 4.2.3.2 of Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships);

thermal underwear — 1 set (vacuum packed);

.2 miscellaneous:

handwarmers for 240 h;

sunglasses — 1;

survival candle — 1;

matches — 2 boxes;

whistle — 1;

drinking mug — 1;

pen knife — 1;

handbook (Arctic Survival) — 1;

carrying bag — 1.

Personal survival kits shall not be opened and used for training purposes and the following notice written in English or the language understood by the crew shall be displayed wherever they are stored:

"CREW MEMBERS AND PASSENGERS ARE REMINDED THAT THEIR PERSONAL SURVIVAL KIT IS FOR EMERGENCY SURVIVAL USE ONLY. NEVER REMOVE ITEMS OR SURVIVAL CLOTHING OR TOOLS FROM THE PERSONAL SURVIVAL KIT CARRYING BAG — YOUR LIFE MAY DEPEND ON IT".

7.9.6.3 In addition to the equipment listed in 7.9.6.2, it is recommended to include the following items in a personal survival kit:

impact-heated thermosoles for boots — 1 pair;

thermotowels for local body warming — 1 pack;

disposable diapers — 1 pack.

7.9.6.4 Group survival kit shall be stored in containers so that they may be easily retrieved in emergency; in general, containers shall be located adjacent to survival craft and be stowed on cradles; containers shall be floatable and be designed so that they may be easily moved over the ice.

A group survival kit shall consist of the following items:

.1 group equipment:

tents — 1 per 6 persons;

air mattresses — 1 per 2 persons;

sleeping bags — 1 per 2 persons (vacuum packed);

stove — 1 per tent;

stove fuel — 0,5 l per person;

fuel paste — 2 tubes per stove;

matches — 2 boxes per tent;

pan (with sealing lid) — 1 per tent;

fortified health drink — 5 packets per person;

flashlight — 1 per tent;

candles and holders — 5 per tent;

snow shovel — 1 per tent;

snow saw — 1 per tent;

snow knife — 1 per tent;

tarpaulin — 1 per tent;

foot protection — boots — 1 pair per person;

GSK container — 1;

.2 spare personal equipment (1 set per GSK container):

head protection — 1 (vacuum packed);

neck and face protection — 1 (vacuum packed);

hand protection — mitts — 1 pair (vacuum packed);

hand protection — gloves — 1 pair (vacuum packed);

foot protection — socks — 1 pair (vacuum packed);

foot protection — boots — 1 pair;

personal thermal aid complying with the requirements of 6.6, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships — 1;

thermal underwear — 1 set (vacuum packed);

handwarmers for 240 h — 1 set;

sunglasses — 1;

whistle — 1;

drinking mug — 1.

7.9.6.5 It is recommended to provide air mattresses included in a group survival kit with a self-inflation system.

7.9.6.6 Where a shot gun or hunting rifle is provided to protect survivors from wildlife, it shall be stored in a secure location readily available in an emergency.

7.10 CARGO GEAR

7.10.1 Cargo handling gear.

7.10.1.1 Materials for manufacture of cargo handling gear elements shall meet the requirements of 3.1 of the Rules for the Cargo Handling Gear of Sea-Going Ships and the requirements of 7.12.1 to 7.12.6.

Design ambient temperature is assumed as design temperature of the structure.

7.10.1.2 When cargo-handling gear is equipped with operator's cabin it shall be provided with heating and fitted with window wiper.

Control panels of the cranes not fitted with cabins, as well as derricks, shall have heating or relevant shelter.

7.10.1.3 Necessary means for cold start of machinery of cargo handling gear at design ambient temperature shall be provided.

7.10.1.4 For hydraulic and electro-hydraulic cargo handling gear, heating of hydraulic liquid shall be provided.

7.10.1.5 Hydraulic liquids and lubricating oils shall be suitable for use at design ambient temperature.

7.10.1.6 The Register certificates issued for cargo handling gear to be installed onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.10.2 Devices for cargo securing on open decks.

7.10.2.1 Materials of devices for securing cargo on open decks, including guides for fastening of deck containers shall meet the requirements of 7.12.1 to 7.12.4.

7.10.2.2 The Register certificates issued for devices for securing cargo on open decks intended for installation onboard the ships with distinguishing marks **WINTERIZATION(–40)** and **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use them at appropriate design ambient temperature.

7.11 ELECTRICAL, RADIO AND NAVIGATIONAL EQUIPMENT

7.11.1 Installation of cables.

7.11.1.1 Cables to be installed on the open decks and in the open unheated spaces shall be tested at following temperatures:

1 for ships with distinguishing marks **WINTERIZATION(–30)** at temperature of $-40\text{ }^{\circ}\text{C}$ and **WINTERIZATION(–40)** at temperature of $-50\text{ }^{\circ}\text{C}$;

2 for ships with distinguishing marks **WINTERIZATION(–50)** at the temperature of $-60\text{ }^{\circ}\text{C}$;

3 when design ambient temperature is below $-50\text{ }^{\circ}\text{C}$ the testing temperature shall be $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature.

7.11.1.2 Cable intended for installation on open decks shall have indications in the Register Certificate/Type Approval Certificate whether it is allowed to use it at appropriate temperatures.

7.11.1.3 Materials for manufacture of cable fastening parts (hangers, cable boxes, pipes) and cable sealing shall meet the requirements of 7.12.1 to 7.12.4.

7.11.1.4 Means shall be provided to protect cable installed on open decks from mechanical damage at manual ice removal.

7.11.2 Equipment.

7.11.2.1 All electric motors, switchboards and control panels provided on the open decks and in the open unheated spaces shall be equipped with the means of anticondensation heating.

7.11.2.2 All electrical equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 10.5.4.2, Part IV "Technical Supervision During Manufacture of Products" of the Rules for Technical Super-

vision During Construction of Ships and Manufacture of Materials and Products for Ships at the temperature in the chamber being $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-40\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for electrical equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.3 All radio equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 4.2, Appendix 1 to Section 15, Part IV "Technical Supervision during Manufacture of Products" of the Rules for Technical Supervision during Construction of Ships and Manufacture of Materials and Products for Ships at the working temperature in the chamber being $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-40\text{ }^{\circ}\text{C}$ (whichever is lower) and at the limiting temperature in the chamber being $20\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-60\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for radio equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.4 All navigational equipment intended for installation on the open decks and in the open unheated spaces shall be tested for cold endurance according to 4.2, Appendix 1 to Section 16, Part IV "Technical Supervision during Manufacture of Products" of the Rules for Technical Supervision during Construction of Ships and Manufacture of Materials and Products for Ships at the working temperature in the chamber being $10\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-40\text{ }^{\circ}\text{C}$ (whichever is lower) and at the limiting temperature in the chamber being $20\text{ }^{\circ}\text{C}$ lower than the design ambient temperature or at the temperature of $-60\text{ }^{\circ}\text{C}$ (whichever is lower).

The Register certificates issued for navigational equipment to be installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(–50)** shall contain an indication whether it is allowed to use it at appropriate design ambient temperature.

7.11.2.5 The list of navigational equipment onboard the ships with a distinguishing mark **WINTERIZATION(DAT)** in the class notation shall meet the requirements of 2.2.3, Part V "Navigational Equipment" of the Rules for the Equipment of Sea-Going Ships in respect of additional requirements for the icebreakers, ships of ice classes **Arc4** to **Arc9**, as well as ships of all polar classes.

7.11.3 Lighting and signal means.

7.11.3.1 Ships shall be equipped with at least two suitable searchlights which shall be controllable from conning positions.

7.11.3.2 Searchlights specified in 7.11.3.1 shall be installed to provide, as far as is practicable, all-round illumination suitable for mooring, astern manoeuvres and emergency towing.

7.11.3.3 Searchlights specified in 7.11.3.1 shall be designed so as to prevent icing or shall be provided with heating.

7.11.4 Electrical heating appliances.

7.11.4.1 Electrical heating fed from emergency sources of electrical power shall be provided for the following ship spaces:

- .1 wheelhouse;
- .2 radioroom (if any);
- .3 main machinery control room;
- .4 cargo control room;
- .5 fire extinguishing station;
- .6 one of public spaces (for instance, messroom);
- .7 hospital;
- .8 engineering workshop.

7.11.4.2 Heating appliances capacity fitted in the above spaces shall provide positive temperature in these spaces at design ambient temperature.

7.11.4.3 Emergency sources of electrical power shall ensure supply of the above heating appliances during the time period stated in 9.3.1, Part XI "Electrical Equipment".

7.11.4.4 Battery compartments shall be heated in compliance with the requirements of 13.3, Part XI "Electrical Equipment". Heating appliances, where fitted, shall be fed from emergency source of electrical power. Thus, it is allowed to perform heating, when power is supplied only from the emergency source of electrical power, by any means in compliance with the international and national standards for explosive atmosphere.

7.12 MATERIALS

7.12.1 Materials used for hull structures and ship machinery items subject to the technical supervision of the Register in accordance with the relevant Parts of the Rules shall comply with the requirements of Part XIII "Materials" and with the Register approved standards and/or with the Register agreed specifications.

7.12.2 Steel plates and sections for hull structural members, ship equipment and machinery intended for prolonged exposure to low service temperatures shall be selected to accordance with 1.2.3, Part II "Hull" with due regard to the adopted value of design ambient temperature. Proceeding from the selected strength level and service conditions, the requirements for steel are

specified in 3.2, 3.5, 3.13, 3.14 and 3.17 of Part XIII "Materials".

In particular cases, at the request of the Register, steel for essential hull structures may be used upon receipt of data on crack resistance of the steel. The information received shall be assessed with regard to the requirements of Part XII "Materials" of the Rules for the Classification, Construction and Equipment of Mobile Offshore Drilling Units and Fixed Offshore Platforms.

7.12.2.1 Steel for machinery and equipment foundations installed on the open decks, in open and enclosed unheated spaces shall comply with the requirements of 1.2.3.1, Part II "Hull" (structural members of category I).

The design temperature of structure shall be assumed according to 7.2.6.

7.12.3 Welded and seamless steel pipes for systems on the open decks and in the open unheated spaces shall comply with the requirements of 3.4 and 3.16, Part XIII "Materials", with the Register approved standards and/or Register agreed specifications.

The material for pipes shall be selected proceeding from the purpose of the systems, with regard to their operating temperature and the requirements of 3.5, Part XIII "Materials" of the Rules, as well as the requirements of Table 2-4, Part IX "Materials and Welding" of the Rules for the Classification and Construction of Gas Carriers for the minimum design temperature of -55°C .

7.12.4 The material of steel forgings and castings for the components of ship equipment, machinery and fittings installed on the open decks and in the open unheated spaces of ships shall comply with the requirements of 3.7 or 3.8, Part XIII "Materials" accordingly, or with the Register approved standards and/or Register agreed specifications.

The material for pipes shall be selected proceeding from the purpose of the forgings and castings, and with regard to their operating temperature and the requirements of 3.5, Part XIII "Materials".

7.12.5 Grey iron and ductile cast iron of ferritic structure is not permitted for the manufacture of components of ship equipment, machinery and fittings installed on the open decks and in the open unheated spaces of ships with a distinguishing mark **WINTERIZATION(DAT)** in the class notation.

7.12.6 Plastics, gasket and seal materials, as well as materials of organic origin used for ship equipment, machinery and fittings and for systems installed on open the decks and in the open unheated spaces of ships shall comply with the applicable requirements of Section 6, Part XIII "Materials", with the Register approved standards and/or with the Register agreed specifications. In addition, a documentary confirmation of the above materials reliability at design temperature or test reports issued by the laboratories recognized by the Register,

another classification society (ACS) or authorized state authorities shall be submitted.

7.12.6.1 The underwater hull and sides of at least 1,0 m above the upper boundary of the ice strake shall have an ice resistant coating (unless clad steel is used for ice strake plating where the appropriate electrochemical protection is provided). The coating supply documentation shall be agreed between the shipowner, the shipyard and the coating manufacturer and shall be submitted to the Register for consideration.

7.12.6.2 The paint coatings of hull structures, machinery and equipment intended for prolonged exposure to low service temperature shall provide required resistance at the design temperature of the structure. The coating supply documentation shall be agreed between the shipowner, the shipyard and the coating manufacturer and shall be submitted to the Register for consideration.

7.12.7 The use of anchor and mooring chain cables of category 1 is not permitted.

The material for anchor and mooring chain cables shall comply with the requirements of 3.6 and Section 7 of Part XIII "Materials", as well as with the Register approved standards and/or with the Register agreed specifications. The maximum impact test temperature is equal to $-20\text{ }^{\circ}\text{C}$.

The results of steel test at operating temperature shall be submitted to the Register.

7.13 TESTS

7.13.1 Tests for cold endurance of materials and products prototypes specified in this Section are generally carried out by manufacturer (enterprise) or laboratories recognized by classification societies or authorized state authorities in accordance with the Rules for Technical Supervision during Construction of Ships and Manufacture of Materials and Products for Ships. Test results may apply to serial products provided the applied materials are identical. In particular cases, e.g. where a product cannot be tested due to its weight and size characteristics, such tests may be replaced by verification of materials and components conformity to the design temperatures. The possibility of such replacement shall be agreed with the Register at the stage of technical documentation and test program review.

7.14 RECORDS

7.14.1 As a result of applying the requirements of the present Section the following records will be issued:

.1 Classification Certificate (forms 3.1.2 and 3.1.2P) with the distinguishing mark **WINTERIZATION(DAT)** in the class notation;

.2 Report on Survey of the Ship (form 6.3.10).

8 REQUIREMENTS FOR PROPULSION PLANT REDUNDANCY

8.1 SCOPE OF APPLICATION AND MARKS IN THE CLASS NOTATION

8.1.1 Compliance with the requirements of this Section is mandatory for the ships, which are assigned according to the requirements of 2.2.27, Part I "Classification" one of the following distinguishing marks added to the class notation:

.1 RP-1 – when the propulsion plant provides for the redundancy of its components, except the main engine, reduction gear, shafting and propeller; at that a single failure in any component of systems and equipment serving the said components shall not lead to the loss of propulsion, power and ship's steering;

.2 RP-1A – when the propulsion plant provides for the redundancy of its components, except the main engine, reduction gear, shafting and propeller; at that a single failure in any component of the propulsion plant, its auxiliary machinery and systems shall not lead to the loss of propulsion and ship's steering;

.3 RP-1AS – when the propulsion plant provides for the redundancy of its components, as required for **RP-1A**, and at that the main engines or the engines of the alternative propulsion plant are located in independent machinery spaces in such a way that the loss of one compartment due to fire or flooding shall not lead to the loss of propulsion, power and ship's steering;

.4 RP-2 – when the propulsion plant provides for the redundancy of its components and consists of several propulsion plants; at that a single failure in any component of the propulsion plant and steering gear shall not lead to the loss of propulsion, power and ship's steering;

.5 RP-2S – when the propulsion plant provides for the redundancy of its components, as required for **RP-2** and is located in two independent machinery spaces in such a way that the loss of one compartment due to fire or flooding shall not lead to the loss of propulsion, power and ship's steering.

8.1.2 Distinguishing marks **RP-1**, **RP-1A**, **RP-1AS**, **RP-2** or **RP-2S** may be assigned to the ships under construction and in service.

8.2 DEFINITIONS AND EXPLANATIONS

8.2.1 The alternative propulsion plant means the totality of machinery, systems and arrangements producing thrust for the ship's motion in emergency conditions in case of a failure of the main propulsion plant. A standby emergency engine, electric motor or shaft

generator applied as a propulsion motors, may be used as the alternative propulsion plant. Total capacity of the alternative propulsion plant shall be at least one eighth of the total capacity of the main propulsion plant.

Auxiliary machinery and systems of the propulsion plant mean all the support systems (fuel system, lubricating oil system, cooling system, compressed air system, hydraulic system, etc.) required for normal operation of the propulsion machinery and propeller.

Main propulsion plant means the totality of machinery, systems and arrangements producing thrust for the ship's motion and comprising propulsion machinery of approximately equal capacity, auxiliary machinery and supporting systems, propellers, as well as all necessary monitoring, control and alarm systems. When the main propulsion plant consists of several engines, each of propulsion engines is considered the main one. When each propulsion plant in two-shaft or more propulsion plant is fully independent, every plant is considered as the main propulsion plant.

Propulsion device/propeller means the machinery (propeller, azimuth thruster, water jet propellers, etc.) converting mechanical energy of the propulsion machinery into thrust for the ship's motion.

Single failure in the propulsion plant means a failure either in an active component (main engine, generator, their local control system, remotely controlled valve, etc.) or in a passive component (pipeline, power cable, manually controlled valve, etc.) not leading to failures of other components.

Power of the propulsion plant means the total power of the propulsion machinery installed onboard the ship. Unless otherwise stated, the capacity of the propulsion plant shall not include the capacity produced by the propulsion machinery but used under normal operating conditions for other purpose than the ship's propulsion (e.g., power of the shaft generator).

Propulsion machinery means the machinery (diesel, turbine, electric motor, etc.) producing mechanical energy for the propeller drive.

Redundancy of the propulsion plant means single or repeated duplication of its components when the propulsion plant is arranged in such a way that a single failure of one of its active or passive components does not lead to the loss of propulsion and ship's steering under the external conditions specified in the Rules.

Marine power plant means the totality of machinery, systems and arrangements that provides the ship with all types of energy and may consists of the following components: main propulsion plant, alternative propulsion plant, electrical power plant, auxiliary machinery.

8.3 TECHNICAL DOCUMENTATION

8.3.1 To assign the distinguishing marks **RP-1**, **RP-1A**, **RP-1AS**, **RP-2** or **RP-2S** added to the class notation of the ship, the following documentation shall be submitted to the Register for approval (where applicable):

.1 calculation results demonstrating that a single failure does not lead to the loss of propulsion and ship's steering according to **8.5.3** (for ships with the distinguishing marks **RP-1A**, **RP-1AS**, **RP-2** or **RP-2S**). As an alternative, the results of the model or full-scale tests may be submitted;

.2 qualitative failure analysis for propulsion and steering (in compliance with Section 12, Part VII "Machinery Installations") or Failure Mode and Effect Analysis (FMEA) of the propulsion plant components based on the failure tree or the equivalent risk analysis agreed with the Register;

.3 torsional vibration calculations in compliance with **3.2.8.5.11**, Part I "Classification"; at that the possibility of long-term operation of the alternative propulsion plant shall be considered separately;

.4 programmes of mooring and sea trials.

8.4 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK RP-1 IN THE CLASS NOTATION

8.4.1 All the components comprising the following auxiliary machinery and systems of the main propulsion plant shall be subject to redundancy:

.1 fuel oil system, including settling tanks, except the fuel oil filling, transfer and separation system;

.2 lubricating oil system of the propulsion machinery, reduction gear, shafting bearings, stern tube bearings, etc., except the oil filling, transfer and separation system;

.3 hydraulic systems providing operation of the propulsion unit couplings, controllable pitch propellers, reverse deflectors of water jet propellers, etc.;

.4 sea water and fresh water cooling systems serving the main propulsion plant;

.5 fuel heating systems in storage tanks serving the main propulsion plant;

.6 starting systems (air, electrical, hydraulic) serving the propulsion plant;

.7 electrical power sources;

.8 ventilation plants, where necessary, for example supplying air for cooling of primary movers;

.9 monitoring, alarm and control systems.

8.4.2 A single failure in the auxiliary pumps and components of the systems indicated in **8.4.1**, including damage of fixed piping, shall not lead to the loss of propulsion and ship's steering. To meet this requirement, the necessary by-pass piping and redundancy of equipment (pumps, heaters, etc.) shall be provided in the systems. In

case of a single failure, reduction of the main engine output may be allowed but not exceeding 50 per cent.

8.4.3 Provision shall be made for disconnection of the sections of systems and piping where a failure occurred from the properly functioning sections.

8.4.4 The ship shall be provided with the main and auxiliary steering gears in compliance with **2.9** of Part III "Equipment, Arrangement and Outfit". Control of the main and auxiliary steering gears shall be independent and provided both on the navigation bridge and in the steering gear compartment.

8.5 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK RP-1A IN THE CLASS NOTATION

8.5.1 In addition to the requirements of **8.4**, the ships with distinguishing mark **RP-1A** in the class notation shall meet the requirements of **8.5**.

8.5.2 The main propulsion plant shall consist of two or more propulsion machinery, at that one reduction gear, one propulsion electric motor, one shaftline and one propeller are allowed. One of the propulsion machinery may be the alternative propulsion plant. Therewith, for independent systems serving the redundant machinery, there is no need to comply with the requirements of **8.4.2** regarding the redundancy of each component of the system.

8.5.3 In case of a single failure in the main propulsion plant, the existing propulsion machinery or the alternative propulsion plant shall provide the following under any conditions of ship's loading:

.1 ship's motion at a speed of 6 knots or 50 per cent of the specified speed of ship according to **1.1.3**, Part II "Hull", whichever is less, at a sea state 5 as per Beaufort scale;

.2 ship's steering sufficient for obtaining the safe position as regard to stability and maintenance of this position at a sea state 8 as per Beaufort scale;

.3 compliance with the requirements of **8.5.3.1** and **8.5.3.2** for at least 72 h; for ships the maximum duration of which voyage is less than 72 h, the above time may be restricted by the maximum duration of the voyage.

8.5.4 The alternative propulsion plant shall be put into operation not later than in 5 min after a failure in the main propulsion plant.

8.5.5 A single failure leading to the loss of one or more generators may be accepted, provided the Failure Mode and Effect Analysis (FMEA) demonstrates that after a failure sufficient power is produced to provide the ship's propulsion and steering in compliance with the requirements of **8.5.3** without the standby generator putting into operation.

After a failure the electrical power shall be sufficient to start the heaviest consumer without the electrical load imbalance.

At that the standby electrical pumps may not be considered for the electrical load balance while operating the alternative propulsion plant.

8.5.6 The main switchboard shall consist of two sections. In case of a failure in one section, the remaining one shall be capable to supply power to the following consumers:

- .1 drives of the alternative propulsion plant and steering gears, including the hinged equipment;
- .2 equipment for transmitting propulsive thrust;
- .3 propulsion electrical motor, where available;
- .4 propeller;
- .5 auxiliary machinery and propulsion plant systems;
- .6 monitoring, alarm and control systems.

8.5.7 Monitoring, alarm and control systems of the alternative propulsion plant shall be independent of the systems of the main propulsion plant.

8.6 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK RP-1AS IN THE CLASS NOTATION

8.6.1 In addition to the requirements of 8.5, the ships with distinguishing mark **RP-1AS** in the class notation shall meet the requirements of 8.6.

8.6.2 The main propulsion plant shall be fitted with at least two main engines located, at least, in two independent engine rooms according to 8.6.3 and 8.6.4. Non-redundant components of the main propulsion plant (reduction gear, propeller, shaftline, propulsion electric motor) common for several main engines shall be located in an independent space separated from the engine rooms with the main engines by a watertight bulkhead of "A-0" class fire integrity according to 2.7.1.2, Part II "Hull".

8.6.3 The bulkhead separating the engine rooms indicated in 8.6.2 shall be watertight bulkhead of "A-60" class fire integrity according to 2.7.1.2, Part II "Hull".

When the engine rooms are separated by cofferdams, tanks or other compartments, the bulkheads shall be at least of "A-0" class fire integrity but not lower than required for the adjacent spaces and compartments in Section 2, Part VI "Fire Protection".

8.6.4 When the closures are provided in the bulkheads indicated in 8.6.2 and 8.6.3, they shall meet the requirements of 7.12, Part III "Equipment, Arrangements and Outfit". These closures may not be considered as the emergency exits of the engine rooms.

8.7 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK RP-2 IN THE CLASS NOTATION

8.7.1 In addition to the requirements of 8.4 and applicable requirements of 8.5, the ship shall meet the requirements of 8.7.

8.7.2 The ship shall be fitted with at least two independent main propulsion plants.

In case of a single failure in one propulsion plant, at least 50 per cent of the ship propulsion power shall remain available and provide propulsion and ship's steering under any loading conditions.

8.7.3 In case of a single failure in one propulsion plant, the following requirements shall be met:

.1 a failure shall not affect the remaining propulsion plant, if it was operative at the moment of a failure (in particular, the drive power and speed shall not be significantly modified);

.2 the remaining propulsion plant, if not operative at the moment of a failure, shall be kept in hot standby in order to be ready for operation within 45 s after a failure;

.3 safety measures shall be provided for the failed propulsion plant, in particular, interlocking of shafting.

8.7.4 The ship shall be fitted with at least two independent steering gears according to 2.9, Part III "Equipment, Arrangements and Outfit". At that at a single failure of one steering gear, the remaining gear shall remain operative, as well as in case of a failure in the synchronizing system.

The ship's steering shall be provided under the conditions indicated in 8.5.3 even in case when one of the rudders is blocked at the maximum hard-over angle, at that the possibility shall be provided of the rudder shifting to the position parallel to the ship centreline and fixing the rudder in this position.

8.7.5 When only the azimuth thrusters are provided as propellers and devices for the ship control, at least two independently operated propulsion plants shall be provided.

The ship's steering shall be provided under conditions indicated in 8.5.3 even in case when one of the azimuth thrusters is blocked or disconnected, at that the possibility shall be provided of the thruster shifting to the position parallel to the ship centreline and fixing the thruster in this position.

8.8 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK RP-2S IN THE CLASS NOTATION

8.8.1 In addition to the requirements of 8.4, applicable requirements of 8.5 and the requirements of 8.7, the ship shall meet the requirements of 8.8.

8.8.2 The ship shall be fitted with at least two independent propulsion plants (including reduction gear, propeller and shafting) according to 8.7.2 and 8.7.3 and located, as a minimum, in two independent engine rooms.

8.8.3 The longitudinal bulkhead separating the engine rooms indicated in 8.8.2 shall be watertight bulkhead of "A-60" class fire integrity according to 2.7.1.2, Part II "Hull".

When the machinery rooms are separated by the cofferdams, tanks or other compartments, the bulkheads shall be at least of "A-0" class fire integrity but not lower than required for the adjacent spaces and compartments in Section 2, Part VI "Fire Protection".

8.8.4 When closures are provided in the longitudinal bulkhead indicated in **8.8.2**, they shall meet the requirements of 7.12, Part III "Equipment, Arrangements and Outfit".

These closures may not be considered as the emergency exits of the machinery rooms.

8.8.5 The ship shall be fitted with at least two independent steering gears in compliance with **8.7.4** located, as a minimum, in two independent steering gear compartments.

8.8.6 The longitudinal bulkhead separating the steering gear compartments shall be watertight bulkhead of at least "A-0" class fire integrity according to 2.7.1.2, Part II "Hull".

8.8.7 The main sources of electrical power shall be located in separate compartments according to **8.8.3** and **8.8.4** that in case of fire or flooding in one compartment, power supply to the consumers indicated in **8.5.6** shall be provided.

8.8.8 The main switchboard shall be divided in two sections according to **8.5.6**.

Each section shall be located in a separate compartment. The bulkhead separating the main switchboard compartments shall comply with the requirements of **8.8.3** and **8.8.4**.

8.8.9 Automation, monitoring and control systems of the propulsion plants and steering gears shall be located in such a way that the loss of one engine rooms due to fire or flooding may lead to the loss of one propulsion plant or one steering gear only.

Control stations shall be arranged in such a way that in case of fire or flooding in one machinery space or one steering gear compartment the control functions shall be provided.

9 REQUIREMENTS FOR SHIPS EQUIPPED FOR USING GASES OR LOW-FLASHPOINT FUELS

9.1 GENERAL

9.1.1 Application.

The requirements of this Section apply to ships using gases or other low-flashpoint fuels. In addition to these requirements, the ship shall comply with requirements of the International Code of Safety for Ships Using Gases or Other Low-Flashpoint Fuels (IGF Code).

If the ship is a LNG gas carrier and uses cargo as fuel, it shall comply with requirements of the International Code for the Construction and Equipment of Ships Carrying Liquefied Gases in Bulk (IGC Code) and the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk.

If a gas carrier use as fuels gas other than liquefied natural gas (LNG) or other low-flashpoint fuels as fuel, the present requirements and the requirements of the IGF Code shall be complied with in addition to the IGC Code requirements.

In addition to sea-going ships, the requirements of this Section apply to other offshore installations subject to the RS technical supervision, oil-and-gas production units and other offshore installations. The relevant national requirements applicable to these installations shall be taken into account additionally to the present requirements.

9.1.2 Class notation.

Ships fitted for the use of gas fuel in compliance with this Section are assigned a distinguishing mark **GFS** (Gas Fuelled Ship) added to the character of classification.

9.1.3 Terms and definitions.

In addition to the below mentioned, the definitions specified in 1.2, Part I "Classification" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk are applicable to the requirements of this Section.

Non-hazardous atmosphere means air environment where gas concentration is lower than the level corresponding to activating an alarm on high gas concentration in the air.

Bunkering means transfer of liquid or gaseous fuel from land based or floating facilities to ships' fixed tanks or connection of transported tanks to the fuel supply system.

Dual fuel engine means a heat engine so designed that both gas and fuel oil may be used as fuel, simultaneously or separately.

Gas means a fluid having a vapour pressure exceeding 0,28 MPa absolute at a temperature of 37,8°C.

Gas-safe machinery space means closed gas-safe space with gas fuel consumers, explosion safety

of which is ensured by installation of gas-containing equipment in gastight enclosures (piping, ducting, partitions) for gas fuel bleed-off, and the inner space of partitions and ducting shall be considered gas-dangerous.

Gas-safe space means a space other than a gas-dangerous space.

Gas area means an area where gas-containing systems and equipment are located, including the weather deck spaces above them.

Gas fuel means any hydrocarbon fuel having at the temperature of 37,8 °C the absolute pressure of saturated vapours according to Reid equal to 0,28 MPa and above.

Gas-dangerous machinery space means enclosed gas-dangerous space with gas fuel consumers, explosion safety of which in case of gas fuel leakage is ensured by emergency shutdown (ESD) of all machinery and equipment which may be an ignition source.

Gas-dangerous space means a space in the gas area which is not equipped with approved device to ensure that its atmosphere is at all times maintained in a gas-safe condition. It is subdivided into explosion hazardous zones 0, 1, 2 the boundaries of which are specified in 9.9.2.

Gas-containing systems mean systems intended for storage, feed, supply and discharge of gas to ship consumers.

Master gas fuel valve means an automatic valve installed at gas supply pipeline to each engine located outside machinery space where the equipment for gas fuel combustion is used.

Fuel oil means liquid hydrocarbon petroleum-derived fuel which complies with the requirements specified in 1.1.2, Part VII "Machinery Installations".

Enclosed space means any space inside of which, in the absence of mechanical ventilation, natural ventilation is restricted in such a way that any explosive atmosphere is not subject to natural dispersion.

Open space means a space open from one or several sides in all parts of which effective natural ventilation is arranged via permanently open openings in the side partitions and in the above located deck.

Semi-enclosed space means a space restricted by decks and bulkheads where natural ventilation is available but its efficiency sufficiently differs from normal at the weather deck.

Gas fuel storage room means a room where gas fuel storage tanks are located.

Fuel preparation room means any space containing pumps, compressors or vaporizers for fuel preparation purposes.

Gas consumer means any ship equipment using gas as a fuel.

Gas engine means an engine capable of operating only on gas, and not able to switch over to operation on any other type of fuel.

Multi-fuel engine means an engine capable of using two or more different fuels that are separate from each other.

Fuel storage tank means a tank designed as an initial gas fuel tank for storage on board the ship in liquid or compressed gaseous form.

CNG tank means compressed gas fuel storage tank.

LNG tank means liquefied gas fuel storage tank.

A, B and C type tanks mean independent fuel storage tanks complying with the requirements for A, B and C type independent tanks of gas carriers specified in the International Code for the Construction and Equipment of Ships Carrying Liquefied Gases in Bulk.

Fuel containment system means the arrangement for the storage of fuel including tank connection spaces. The fuel containment system includes a primary and, where fitted, a secondary barriers, associated insulation and any intervening spaces, and adjacent structures, if necessary for the support of these elements. If the secondary barrier is part of the hull structure, it may be a boundary of the fuel storage hold space. The spaces around the fuel tank are defined as follows:

.1 fuel storage hold space means a space enclosed by the ship's structures in which a fuel containment system is situated. If tank connection spaces are located in the fuel storage hold space, it will also be a tank connection space;

.2 interbarrier space means the space between a primary and a secondary barrier, whether or not completely or partially occupied by insulation or other material; and

.3 fuel storage tank connection space means a space surrounding all fuel storage tank connections and tank valves that are required for such tanks in enclosed spaces.

Filling limit (FL) means the maximum liquid volume in a fuel tank relative to the total tank volume when the liquid fuel has reached the reference temperature.

Reference temperature means the temperature corresponding to the vapour pressure of the fuel in a fuel tank at the set pressure of the pressure relief valves (PRVs).

Vapour pressure means the equilibrium pressure of the saturated vapour above the liquid, in MPa, absolute at a specified temperature.

Secondary barrier means the liquid-resisting outer element of a fuel containment system designed to afford temporary containment of any envisaged leakage of liquid fuel through the primary barrier and to prevent the lowering of the temperature of the ship's structure to an unsafe level.

Source of release means a point or location from which a gas, vapour, mist or liquid may be released into the atmosphere so that an explosive atmosphere could be formed.

IGF Code means the International Code of Safety for Ships Using Gases or Other Low-Flashpoint Fuels.

9.1.4 Technical documentation.

In addition to the technical documentation specified in Section 3, Part I "Classification", the following technical data and ship documents confirming fulfillment of the Rules shall be submitted to the Register:

.1 drawings of fuel tanks arrangement with their distances from side plating and the bottom specified;

.2 drawings of supports and other structures to ensure fastening and limiting shifting of fuel tanks;

.3 calculations of heat emission from the flame which may occur during the fire affecting gas fuel tanks and other equipment and spaces related to gas fuel;

.4 drawings and diagrams of systems and piping for gas fuel specifying such assemblies as compensators, flange joints, stop and control valves and fittings, drawings of quick-closing arrangements of the gas fuel system, diagrams of gas fuel preparation, heating and pressure control, calculations of stresses in piping containing gas fuel at a temperature below -110°C ;

.5 drawings of safety and vacuum safety valves of fuel storage tanks;

.6 drawings and descriptions of all systems and arrangements for the measurement of fuel amount and characteristics, and for gas detection;

.7 diagrams of gas fuel pressure and temperature control and regulating systems;

.8 drawings and calculations of bilge and ballast systems in gas-hazardous spaces;

.9 diagrams and calculations of gas-dangerous spaces ventilation;

.10 diagrams and calculations of gas-freeing system;

.11 circuit diagrams of electric drives and control systems for fuel preparation plants, ventilation of hazardous spaces and airlocks;

.12 circuit diagrams of electric measurement and alarm systems for equipment related to the use of gas fuel;

.13 general arrangement drawings of electrical equipment related to the use of gas fuel;

.14 drawings of cable laying in hazardous spaces and areas;

.15 drawings of earthing for electrical equipment, cables, piping located in gas-dangerous spaces;

.16 technical background of electrical equipment fitness;

.17 ship general arrangement drawings specifying the layout of the following:

gas fuel storage tanks and any openings in them;

spaces for fuel storage and preparation and any openings to them;

doors, hatches and any other openings into hazardous spaces and areas;

venting pipes and air inlet and outlet locations of a ventilation system of hazardous spaces and areas;

doors, scuttles, companions, ventilation duct outlets locations and other openings in spaces adjacent to hazardous area;

.18 data on the properties of gas fuel intended for the use on board the ship;

.19 analysis of risks related to the use and storage of gas fuel and possible consequences of its leakages according to IACS Recommendations No. 146¹.

The analysis shall consider the risks of damage of hull structural members and failure of any equipment after accident related to the use of gas fuel. The results of risk analysis shall be taken into account in the operating manual.

.20 regarding the LNG tanks, the technical documentation shall be submitted in the extent required for approval of a cargo tank for carrying LNG on board the gas carrier in compliance with the requirements of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk and the International Code for the Construction and Equipment of Ships Carrying Compressed Natural Gas.

Regarding the CNG tanks, the technical documentation shall be submitted in the extent required for approval of a cargo tank for carrying CNG on board the gas carrier in compliance with the Rules for the Classification and Construction of CNG Gas Carriers.

When the standard cylinders are used, the calculation of permissible pressure shall be submitted.

9.2 GENERAL REQUIREMENTS FOR SHIP STRUCTURE

9.2.1 All dimensions of hull structure elements, except those specially mentioned in this Chapter, shall be determined in accordance with the requirements of the Rules for the Classification and Construction of Sea-going Ships depending on purpose and structural type of the ship.

9.2.2 Onboard location of fuel storage tanks.

9.2.2.1 Fuel storage tanks both in liquefied (LNG) and compressed (CNG) condition may be located directly on the open deck of the ship or in special enclosed spaces in the ship's hull. In the enclosed spaces, liquefied gas fuel shall be stored at the pressure not exceeding 1 MPa.

Where a fuel storage tank is located on the weather deck or in a special enclosure designed as a semi-enclosed space, provision shall be made for sufficient natural ventilation to prevent accumulation of escaped gas.

Membranes ensuring a seal between a deck and fuel storage tank shall be provided where the fuel storage tank gets through the upper weather deck. Therewith, the

space located below the membranes may be considered as an enclosed gas-dangerous space, and the space above the membranes may be considered as an open space.

Gas fuel storage tanks shall not be installed under the survival craft except for the liferafts in compliance with 4.1.1.4, Part II "Live-saving Appliances" of the Rules for the Equipment of Sea-Going Ships.

9.2.2.2 Fuel storage tanks shall be protected against mechanical damage.

When fuel is carried in a fuel containment system requiring a complete or partial secondary barrier:

.1 fuel storage hold spaces shall be segregated from the sea by a double bottom/inner bottom; and

.2 ship shall have longitudinal bulkheads forming side tanks.

9.2.2.3 The fuel storage tanks shall be protected from external damage caused by collision or grounding in the following way:

.1 fuel tanks shall be located at a minimum distance of $B/5$ or 11,5 m, whichever is less, measured inboard from the ship side at right angles to the centreline at the level of the summer load line draught.

where B = the greatest moulded breadth of the ship at the summer load line draught) (refer to SOLAS regulation II-1/2.8).

As an alternative, the calculation method specified in 5.3.4 of the IGF Code may be used to determine the acceptable location of fuel tanks;

.2 boundaries of each fuel tank shall be taken as the extreme outer longitudinal, transverse and vertical limits of the tank structure including its valves;

.3 for independent tanks the protective distance shall be measured to the tank shell (the primary barrier of the tank containment system). For membrane tanks, such distance shall be measured to the bulkheads surrounding the tank insulation;

.4 in no case shall the boundary of the fuel tank be located closer to the shell plating or aft terminal of the ship than as follows:

.1 for passenger ships: $B/10$ but in no case less than 0,8 m. However, this distance shall not be greater than $B/15$ or 2 m, whichever is less, where the shell plating is located inboard for $B/5$ or 11,5 m, whichever is less, as specified in 9.2.3.1;

.2 for cargo ships:

for $V_c \leq 1000 \text{ m}^3$ — 0,8 m;

for $1000 \text{ m}^3 < V_c < 5000 \text{ m}^3$ — $0,75 + V_c \times 0,2/4000$ m;

for $5000 \text{ m}^3 \leq V_c < 30000 \text{ m}^3$ — $0,8 + V_c/25000$ m;

and

for $V_c \geq 30000 \text{ m}^3$ — 2 m

where V_c corresponds to 100 % of the gross design volume of the individual fuel storage tank at 20 °C, including domes and appendages;

¹Refer to Supplement to rules and guidelines of Russian Maritime Register of Shipping "IACS Procedural Requirements, Unified Interpretations and Recommendations" (published in electronic format as a separate edition).

.5 the lowermost boundary of the fuel storage tank shall be located above the minimum distance of $B/15$ or 2,0 m, whichever is less, measured from the moulded line of the bottom shell plating at the centreline;

.6 for multi-hull ships, the value B may be specially considered;

.7 fuel storage tanks shall be located abaft a transverse plane at $0,08L$ measured from the forward perpendicular in accordance with SOLAS regulation II-1/8.1 for passenger ships, and abaft the collision bulkhead for cargo ships

where L = length as defined in the International Convention on Load Lines (refer to SOLAS regulation II-1/2.5).

9.2.3 Drip trays.

9.2.3.1 Drip trays for spilled liquefied gas shall be fitted where liquefied gas leakage may occur which can cause damage to the ship structure or where limitation of the area, which is effected from a spill, is necessary.

9.2.3.2 Drip trays shall be made of suitable material.

9.2.3.3 The drip tray shall be thermally insulated from the ship's structure so that the surrounding hull or deck structures are not exposed to unacceptable cooling, in case of leakage of liquid fuel.

9.2.3.4 Each drip tray shall be fitted with a drain valve to enable rain water to be discharged overboard.

9.2.3.5 Each drip tray shall have sufficient capacity to ensure that the maximum amount of spill according to the risk assessment can be handled.

9.2.4 Machinery spaces.

9.2.4.1 In order to minimize the probability of gas explosion in a machinery space containing gas-fuelled machinery one of the following two alternatives of machinery space arrangement may be applied:

.1 gas-safe machinery spaces: arrangements in machinery spaces are such that the spaces are considered gas safe under all conditions, normal as well as unplanned conditions, i.e. inherently gas safe.

In a gas-safe machinery space a single failure cannot lead to release of fuel gas into the machinery space;

.2 ESD protected machinery spaces: arrangements in machinery spaces are such that the spaces are considered non-hazardous under normal conditions, but under certain abnormal conditions may have the potential to become hazardous. In the event of abnormal conditions involving gas hazards, emergency shutdown (ESD) of non-safe equipment (ignition sources) and machinery shall be automatically executed while equipment or machinery in use or active during these conditions shall be of a certified safe type and have relevant certificates.

In an ESD protected machinery space, a single failure resulting in gas release into the space is allowable provided that the gas is removed by venting.

Failures leading to dangerous gas concentrations, e.g. gas pipe or gasket ruptures are covered by explosion pressure relief devices and ESD arrangements.

9.2.4.2 Requirements for gas-safe machinery spaces.

.1 single failure within the fuel system shall not lead to gas release into the machinery space;

.2 all gas piping within machinery space boundaries shall be enclosed in a gas tight enclosure.

9.2.4.3 Requirements for ESD protected machinery spaces.

.1 ESD protection shall be limited to machinery spaces that are intended for periodically unmanned operation.

.2 measures shall be applied to protect against explosion and damage of areas outside the machinery space and ensure redundancy of power supply. At least the following measures and arrangements shall be provided:

- gas detector;
- shut-off valve;
- redundancy;
- efficient ventilation.

9.2.4.4 Gas supply piping without a gastight external enclosure within machinery spaces may be accepted under the following conditions:

.1 engines for generating propulsion power and electric power shall be located in two or more machinery spaces not having any common boundaries unless it can be documented that a single failure will not affect both spaces;

.2 gas machinery space shall contain only a minimum of such necessary equipment, components and systems as are required to ensure that the gas machinery maintains its function;

.3 fixed gas detection system arranged to automatically shutdown the gas supply, and disconnect all electrical equipment or installations not of a certified safe type, shall be fitted.

9.2.4.5 Distribution of engines between the different machinery spaces shall be such that shutdown of fuel supply to any one machinery space does not lead to an unacceptable loss of power.

9.2.4.6 ESD protected machinery spaces separated by a single adjacent bulkhead shall have sufficient strength to withstand the effects of local gas explosion in either space, without affecting the integrity of the adjacent space and equipment within that space.

9.2.4.7 ESD protected machinery spaces shall have a geometrical shape that will minimize the accumulation of gases or formation of gas pockets.

9.2.4.8 The ventilation system of ESD protected machinery spaces shall be arranged in accordance with 9.7.

9.2.4.9 Requirements for location and protection of fuel piping:

.1 fuel piping shall not be located less than 800 mm from the ship's side;

.2 fuel piping shall not pass directly through accommodation spaces, service spaces, electrical equipment rooms or control stations;

.3 fuel piping passing through ro-ro cargo spaces, special category spaces and on weather decks shall be protected against mechanical damage.

.4 gas fuel piping in ESD protected machinery spaces shall be located, as far as practicable, from the electrical installations and tanks containing flammable liquids.

9.2.4.10 Gas fuel piping in ESD protected machinery spaces shall be protected against mechanical damage.

9.2.4.11 Requirements for fuel preparation room design.

Fuel preparation rooms shall be located on the open deck or within an open space unless those rooms are arranged and fitted in accordance with the requirements for tank connection spaces.

9.2.5 Requirements for bilge systems.

9.2.5.1 Bilge systems installed in areas where gas or other low-flashpoint fuels may be present shall be segregated from the bilge system of spaces where fuel cannot be present.

9.2.5.2 Where fuel is carried in a fuel containment system requiring a secondary barrier, suitable drainage arrangements for dealing with any leakage into the hold or insulation spaces through the adjacent ship structure shall be provided. The bilge system shall not lead to pumps in safe spaces. Means of detecting such leakages shall be provided.

9.2.5.3 The hold or interbarrier spaces of type A independent tanks for liquid gas shall be provided with a bilge system suitable for handling liquid fuel in the event of fuel tank leakage or rupture.

9.2.6 Requirements for arrangement of entrances and other openings in enclosed spaces.

9.2.6.1 Direct access shall not be permitted from a gas-safe area to a gas-dangerous area. Where such openings are necessary for operational reasons, an airlock, which complies with **9.2.7**, shall be provided.

9.2.6.2 If a fuel preparation room is approved to be located below deck, the room shall, as far as practicable, have an independent access directly from the open deck. Where a separate access from deck is not practicable, an airlock, which complies with the requirements of **9.2.7**, shall be provided.

9.2.6.3 Unless access to the tank connection space is independent and directly from the open deck, it shall be arranged as a bolted hatch. The space containing the bolted hatch is a hazardous space.

9.2.6.4 If access to an ESD protected machinery space is from another enclosed space of the ship, the entrances shall be arranged with an airlock, which complies with the requirements of **9.2.7**.

9.2.6.5 For inerted spaces, access arrangements shall be such that unintended entry by personnel shall be prevented. If access to such spaces is not from the open deck, sealing arrangements shall prevent leakages of inert gas to adjacent spaces.

9.2.7 Requirements for airlocks.

9.2.7.1 An airlock is a space enclosed by gastight bulkheads with two substantially gastight doors spaced at least 1,5 m and not more than 2,5 m apart. Unless subject to the requirements of the International Convention on Load Lines, the door coaming shall not be less than 300 mm in height. The doors shall be self-closing without any holding back arrangements.

9.2.7.2 Airlocks shall be mechanically ventilated at overpressure relative to the adjacent hazardous area or space.

9.2.7.3 The airlock shall be designed in a way that no gas can be released to safe spaces in case of the most critical event in the gas-dangerous space separated by the airlock. The events shall be evaluated in the risk analysis according to **9.1.4.19**.

9.2.7.4 Airlocks shall have a simple geometrical form. They shall provide free and easy passage, and shall have a deck area not less than 1,5 m². Airlocks shall not be used for other purposes, e.g. as store rooms.

9.2.7.5 An audible and visual alarm system to give a warning on both sides of the airlock shall be provided to indicate if more than one door is moved from the closed position.

9.2.7.6 For gas-safe spaces with access from hazardous spaces below deck where the access is protected by an airlock, upon loss of underpressure in the hazardous space access to the space is to be restricted until the ventilation is reinstated. Audible and visual alarms shall be given at a manned location to indicate both loss of pressure and opening of the airlock doors when pressure is lost.

9.2.7.7 Essential equipment required for safety shall not be de-energized and shall be of a certified safe type. This may include lighting, fire detection, public address and general alarms systems.

9.3 DESIGN OF GAS FUEL TANKS

9.3.1 General requirements for gas fuel storage.

9.3.1.1 Natural gas in a liquid state may be stored with a maximum allowable relief valve setting (MARVS) of up to 1,0 MPa.

9.3.1.2 The maximum allowable working pressure (MAWP) of the gas fuel tank shall not exceed 90 % of the maximum allowable relief valve setting (MARVS).

9.3.1.3 A fuel containment system located below deck shall be gastight towards adjacent spaces.

9.3.1.4 All tank connections, fittings, flanges and tank valves shall be enclosed in gastight tank connection spaces, unless the tank connections are on the open deck. The space shall be able to contain leakage from the tank without overpressure in case of leakage from the tank connections.

9.3.1.5 Pipe connections to the fuel storage tank shall be mounted above the highest liquid level in the tanks, except for fuel storage tanks of type C. Connections below the highest liquid level may, however, also be accepted for other tank types after special consideration.

9.3.1.6 Each gas fuel storage tank (LNG or CNG) shall be equipped with a remote operated isolation shutoff valve located at any piping connected to the tank or directly on the tank. A branch pipe between the tank and the isolation valve which release LNG in case of pipe failure shall have equivalent safety to the type C tank, with permissible stress not exceeding the least of values $R_m/2.5$ or $R_e/1.2$, where R_e is a minimum yield stress at room temperature, and R_m is a minimum tensile strength at room temperature.

9.3.1.7 The material of the structures of the tank connection space shall have a design temperature corresponding to the lowest temperature that can be subject to in a probable maximum leakage scenario. The tank connection space shall be designed to withstand the maximum pressure build up during such a leakage. Alternatively, pressure relief venting to a safe location (mast) may be provided.

9.3.1.8 The probable maximum leakage into the tank connection space shall be determined based on design calculations using the operating parameters of detection and shutdown systems.

9.3.1.9 If connected below the liquid level of the tank, piping shall be protected by a secondary barrier up to the first valve.

9.3.1.10 If LNG tanks are located on the open deck, steel structures shall be protected against potential leakages from tank connections and other sources of leakage by use of drip trays. The material shall have a design temperature corresponding to the temperature of fuel carried at atmospheric pressure. The normal operation pressure of tanks shall be taken into consideration for protecting the steel structures of the ship.

9.3.1.11 Means shall be provided to safely empty liquefied gas storage tanks.

9.3.1.12 It shall be possible to empty, purge and vent fuel storage tanks with fuel piping systems. Instructions for carrying out these procedures shall be available on board. Inerting shall be performed with inert gas prior to venting with dry air to avoid an explosion hazardous atmosphere in tanks and fuel pipelines. Requirements to the inerting system are specified in 9.9.

9.3.1.13 For single fuel (gas only) main engines at least two gas fuel storage tanks of approximately equal capacity shall be provided and they shall be located in separate spaces.

9.3.1.14 All fuel storage tanks shall be provided with a pressure relief system appropriate to the design of the fuel containment system and the fuel being carried. Fuel storage hold spaces, interbarrier spaces, tank connection spaces and tank cofferdams, which may be subject to pressures beyond their design capabilities, shall also be

provided with a suitable pressure relief system. Pressure relief system shall be independent of the pressure control systems specified in 9.4.

9.3.2 Liquefied gas storage tanks (LNG tanks).

9.3.2.1 LNG tanks shall be designed in compliance with the requirements of Section 6.4 of IGF Code.

9.3.2.2 All LNG tanks shall be fitted with safety valves in compliance with the requirements of Section 6.7 of IGF Code.

9.3.2.3 The outlets of vent pipes from the pressure relief valves shall be located at least $B/3$ or 6 m, whichever is greater, above the weather deck and 6 m above the working area and forward and aft gangways. Gas outlet piping system shall be designed so that the outgoing gas shall be directed upwards and the possibility of water and snow ingress into the system shall be kept to minimum.

9.3.2.4 All gas outlets shall be located at a distance of at least 10 m from:

the nearest air inlet or openings in the accommodation and service spaces and control stations or from other gas-safe spaces;

outlets in the machinery space.

9.3.2.5 LNG tanks shall be provided with the pressure control system specified in 9.4.

9.3.3 Compressed gas storage tanks (CNG tanks).

9.3.3.1 CNG tanks shall be designed in compliance with the requirements of Part X "Boilers, Heat Exchangers and Pressure Vessels" or other applicable standards for design of gas storage pressure vessels agreed upon with the Administration. Standard cylinders, for which it is necessary to make calculation of permitted pressure, and specially designed pressure vessels may be used as CNG tanks.

9.3.3.2 Each compressed gas storage tank shall be equipped with safety valves with cracking pressure less than design pressure of the tank. Safety valves of CNG tanks located in the hull or on the open deck shall be connected with gas outlet pipes. The outlets of vent pipes from the pressure relief valves shall comply with requirements specified in 9.3.2.3 and 9.3.2.4.

9.3.3.3 Adequate means shall be provided to depressurize the tank in case of fire, which can affect the tank.

9.3.3.4 Storage of CNG in enclosed spaces is generally not acceptable, but may be permitted provided the following is fulfilled in addition to 9.3.1.4 and 9.3.1.6:

1 adequate means are provided to depressurize and inert the tank in case of fire which can affect the tank;

2 all surfaces within such enclosed spaces containing the CNG storage are provided with suitable thermal protection against any high-pressure gas leakages and resulting condensation unless the bulkheads are designed for the lowest temperature that can arise from gas expansion leakage; and

3 a fixed fire-extinguishing system is installed in the enclosed spaces containing the CNG storage. In addition,

special arrangements for extinguishing of jet-fires shall be provided.

9.3.3.5 CNG tanks shall be secured on the hull in a manner which will prevent their movement under static or dynamic loads. Tanks with supports shall be designed for a static angle of heel of 30°. The supports and fittings shall be designed with due regard to loads determined in accordance with 6.4.9.4 of IGF Code.

9.3.4 Regulations for portable liquefied gas fuel tanks.

9.3.4.1 The design of the tank shall comply with the requirements of IGF Code for type C independent tanks. The tank support (container frame or truck chassis) shall be designed for the intended purpose.

9.3.4.2 Portable fuel tanks shall be located in dedicated areas fitted with:

- .1 mechanical protection of the tanks depending on location and damage hazard during cargo operations;
- .2 if located on open deck: spill protection and water spray and cooling systems; and
- .3 if located in an enclosed space: the space shall be considered as a tank connection space.

9.3.4.3 Portable fuel tanks shall be secured to the deck when connected to the ship systems. The arrangement for supporting and fixing the tanks shall be designed for the maximum expected static and dynamic inclinations, as well as the maximum expected values of acceleration, taking into account the ship characteristics and the position of the tanks.

9.3.4.4 Consideration shall be given to the strength and the effect of the portable fuel tanks on the ship's stability.

9.3.4.5 Connections to the ship's fuel piping systems shall be made by means of approved flexible hoses or other suitable means designed to provide sufficient flexibility.

9.3.4.6 Arrangements shall be provided to limit the quantity of fuel spilled in case of inadvertent disconnection or rupture of the non-permanent connections.

9.3.4.7 The pressure relief system of portable tanks shall be connected to a fixed venting system.

9.3.4.8 Control and monitoring systems for portable fuel tanks shall be integrated in the ship's control and monitoring system. A safety system for portable fuel tanks shall be integrated in the ship's safety system (e.g. shutdown systems for tank valves, gas detection systems).

9.3.4.9 Safe access to tank connections for the purpose of inspection and maintenance shall be ensured.

temperature, liquefied gas fuel tanks' pressure and temperature shall be maintained at all times within their design range by one of the following methods:

- .1 reliquefaction of vapours;
- .2 thermal oxidation of vapours;
- .3 pressure accumulation;
- .4 liquefied gas fuel cooling.

The method chosen shall ensure maintaining tank pressure below the set pressure of the tank pressure relief valves for a period of 15 days assuming the full tank at normal service pressure and the ship in non-working condition, i.e. only power for domestic load is generated.

9.4.2 The overall capacity of the system shall be such that it can control the pressure within the design conditions without venting to atmosphere. The system shall be sized in a sufficient way also in case of no or low consumption. Venting of fuel vapour for controlling the tank pressure is not acceptable except in emergencies.

9.4.3 For worldwide service, the upper ambient design temperature shall be 32 °C for sea water and 45 °C for air. For service in particularly hot or cold zones, these design temperatures shall be increased or decreased as agreed upon with the Register.

9.4.4 The reliquefaction system shall be designed and calculated in one of the following ways:

- .1 a direct system where evaporated fuel is compressed, condensed and returned to the fuel tanks;
- .2 an indirect system where fuel or evaporated fuel is cooled or condensed by refrigerant without being compressed;

.3 a combined system where evaporated fuel is compressed and condensed in a fuel/refrigerant heat exchanger and returned to the fuel tanks; or

.4 if the reliquefaction system produces a waste stream containing methane during pressure control operations within the design conditions, these waste gases shall, as far as reasonably practicable, be disposed of without venting to atmosphere.

9.4.5 Thermal oxidation can be done by either consumption of the vapours according to the regulations for consumers specified in 9.4 or in a dedicated gas combustion unit (GCU). It shall be demonstrated that the capacity of the oxidation system is sufficient to consume the required quantity of vapours. In this regard, periods of slow steaming and no consumption from propulsion plant or other consumers of the ship shall be considered.

9.4.6 Refrigerants or auxiliary agents used for cooling of fuel shall be compatible with the fuel they may come in contact with (not causing any hazardous reaction or excessively corrosive products). In addition, when several refrigerants or agents are used, these shall be compatible with each other.

9.4.7 The redundancy of the system and its supporting auxiliary services shall be such that in case of a single failure (of mechanical non-static component or a component of the control system) the fuel tank

9.4 STORED FUEL PRESSURE AND TEMPERATURE CONTROL SYSTEM

9.4.1 With the exception of liquefied gas fuel tanks designed to withstand the full gauge vapour pressure of the fuel under conditions of the upper ambient design

pressure and temperature can be maintained by another system or service.

9.4.8 Heat exchangers that are necessary for maintaining the pressure and temperature of the fuel tanks within their design ranges shall have redundancy unless they have a capacity in excess of 25 % of the largest required capacity for pressure control and they can be repaired on board without external sources.

9.5 FUEL SYSTEM

9.5.1 General requirements for fuel pipelines.

9.5.1.1 Fuel pipes and all the other piping needed for a safe and reliable operation and maintenance shall be colour marked in accordance with EN ISO 14726:2008 or equivalent.

9.5.1.2 Where tanks or piping are separated from the ship's structure by thermal isolation, provision shall be made for electrically bonding to the ship's structure both the piping and the tanks. All gasketed pipe joints and hose connections shall be electrically bonded.

9.5.1.3 All pipelines or components which may be isolated in a liquid full condition shall be provided with relief valves.

9.5.1.4 Pipelines which may contain low temperature fuel shall be thermally insulated to an extent which will minimize condensation of moisture.

9.5.1.5 Wall thickness of pipes under internal pressure shall be at least equal to that determined by Formula (2.3.1), Part VII "Systems and Piping" of the Rules for the Classification and Construction of Sea-Going Ships with regard to additional requirements specified in 2.2.1 to 2.2.4, Part VI "Systems and Piping" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk.

9.5.1.6 During manufacture of fuel system pipelines and selection of connections, requirements specified in 2.3 to 2.5, Part VI "Systems and Piping" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk shall be complied with.

9.5.2 Bunkering stations.

9.5.2.1 The bunkering station shall be located on open deck so that sufficient natural ventilation is provided. Closed or semi-enclosed bunkering stations shall be subject to special consideration within the risk assessment in accordance with IACS Recommendation No. 146.

The bunkering station shall not be installed near the survival craft except for the liferafts required in compliance with 4.1.1.4, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships.

9.5.2.2 Connections and piping shall be so positioned and arranged that any damage to the fuel piping does not cause damage to the ship's fuel containment system resulting in an uncontrolled gas discharge.

9.5.2.3 Arrangements shall be made for safe management of any spilled fuel.

9.5.2.4 Suitable means shall be provided to relieve the pressure and remove liquid contents from pump suctions and bunker lines. Liquid shall be discharged to the LNG tanks or other suitable location.

9.5.2.5 The surrounding hull or deck structures shall not be exposed to unacceptable cooling in case of leakage of fuel.

9.5.2.6 For CNG bunkering stations, low temperature steel shielding shall be fitted to protect against low temperatures if the escape of cold jets impinging on surrounding hull structure is possible.

9.5.2.7 The bunkering manifold shall be designed to withstand the external loads during bunkering. The connections at the bunkering station shall be of dry-disconnect type equipped with additional safety dry break-away coupling/self-sealing quick release. The couplings shall be of a standard type.

9.5.2.8 An arrangement for purging fuel bunkering lines with inert gas shall be provided.

9.5.2.9 The bunkering system shall be so arranged that no gas is discharged to the atmosphere during filling of storage tanks.

9.5.2.10 A manually operated stop valve and a remote operated shutdown valve in series, or a combined manually operated and remote valve shall be fitted in every bunkering line close to the connecting point. It shall be possible to operate the remote valve in the control location for bunkering operations and/or from another safe location.

9.5.2.11 Means shall be provided for draining any fuel from the bunkering pipes upon completion of operation.

9.5.2.12 Bunkering lines shall be arranged for inerting and gas freeing. When not engaged in bunkering, the bunkering pipes shall be free of gas, unless the consequences of not gas freeing is evaluated and approved.

9.5.2.13 In case bunkering lines are arranged with a cross-over it shall be ensured by suitable isolation arrangements that no fuel is transferred inadvertently to the ship side not in use for bunkering.

9.5.2.14 A ship-shore link (SSL) or an equivalent means for automatic and manual ESD communication to the bunkering source shall be fitted.

9.5.2.15 The actuation time (from the trigger of the alarm to full closure) of the remote operated valve required by 9.6.2.10 shall be adjusted and be not greater than:

$$3600U/BR \text{ s}$$

where U = ullage volume at operating signal level, in m^3 ;
 BR = maximum bunkering rate agreed between ship and shore facility, in m^3/h ; or
 5 s , whichever is the least.

The actuation time may be increased if the calculation demonstrates that it is required due to hydraulic impact hazard.

9.5.3 Requirements for redundancy of fuel supply systems.

9.5.3.1 For single fuel installations the fuel supply system shall be arranged with full redundancy and segregation all the way from the fuel tanks to the consumers so that a leakage in one system does not lead to an unacceptable loss of power.

9.5.3.2 For single fuel installations, the fuel storage shall be divided between two or more tanks. The tanks shall be located in separate compartments.

9.5.3.3 For type C tank only, one tank may be accepted if two completely separate tank connection spaces are provided for the one tank.

9.5.4 Safety of gas supply systems.

9.5.4.1 Fuel storage tank inlets and outlets shall be provided with valves located as close to the tank as possible. Valves required to be operated during normal operation and bunkering which are not readily accessible shall be remotely operated. Tank valves whether accessible or not shall be automatically operated when the safety system required in Table 9.10.4.4 is activated for automatic closure of the tank valve.

9.5.4.2 The main gas supply line to each gas consumer or set of consumers shall be equipped with a manually operated stop valve and an automatically operated master gas fuel valve coupled in series or a combined manually and automatically operated valve. The valves shall be situated in the part of the piping that is outside the machinery space containing gas consumers, and placed as near as possible to the installation for gas treatment, if fitted. The master gas fuel valve shall automatically cut off the gas supply to the machinery space with gas consuming engines when activated by the safety system required in Table 9.10.4.4.

9.5.4.3 The automatic master gas fuel valve shall be operable from safe locations on escape routes inside a machinery space containing a gas consumer, the engine control room, if applicable; outside the machinery space, and from the navigation bridge.

9.5.4.4 Each gas consumer shall be provided with a double block and bleed valves arrangement. These valves shall be arranged as specified in 9.5.4.4.1 and 9.5.4.4.2 so that when the safety system required in Table 9.10.4.4 is activated this will cause the shut-off valves that are in series to close automatically and the bleed valve to open automatically and:

.1 two shut-off valves shall be in series in the gas fuel pipe to the gas consuming equipment. The bleed valve shall be in a pipe that vents to a safe location in the open air from that portion of the gas fuel piping that is between the two valves in series; or

.2 the functions of one of the shut-off valves in series and the bleed valve can be incorporated into one valve body, so arranged that the flow to the gas utilization unit will be blocked and the ventilation opened.

9.5.4.5 The two valves shall be of the fail-to-close type, while the bleed valve shall be fail-to-open.

9.5.4.6 The double block and bleed valves shall also be used for normal stop of the engine.

9.5.4.7 In cases where the master gas fuel valve is automatically shutdown, the complete gas supply branch downstream of the double block and bleed valve shall be automatically ventilated assuming possible reverse flow from the engine to the pipe.

9.5.4.8 There shall be one manually operated shutdown valve in the gas supply line to each engine upstream of the double block and bleed valves to assure safe isolation during maintenance of engines.

9.5.4.9 For single-engine installations and multi-engine installations, where a separate master valve is provided for each engine, the master gas fuel valve and the double block and bleed valve functions can be combined.

9.5.4.10 For each main gas supply line entering an ESD protected machinery space, and each gas supply line to high pressure installations means shall be provided for rapid detection of a rupture in the gas line in the machinery space. When rupture is detected a valve shall be automatically shut off, the shutdown shall be time delayed to prevent blackout due to abrupt load variations. This valve shall be located in the gas supply line before it enters the machinery space or as close as possible to the point of entry inside the machinery space. It can be a separate valve or combined with other functions, e.g. the master valve.

9.5.4.11 Fuel pipes passing through enclosed spaces outside the machinery spaces shall be protected by a secondary enclosure. This enclosure can be a ventilated duct or a double wall piping system. The duct or double wall piping system shall be mechanically ventilated with 30 air changes per hour, and gas detection as required in 9.10.4 shall be provided. This requirement may be omitted for fully welded fuel gas vent pipes passing through mechanically ventilated spaces.

9.5.5 Fuel supply in gas-safe machinery spaces.

9.5.5.1 Fuel piping in gas-safe machinery spaces shall be completely enclosed in external pipes or ducts fulfilling one of the following conditions:

.1 the gas piping shall be a double wall piping system with the gas fuel contained in the inner pipe. The space between the concentric pipes shall be pressurized with inert gas at a pressure greater than the gas fuel pressure. Suitable alarms shall be provided to indicate a loss of inert gas pressure between the pipes. When the inner pipe contains high pressure gas, the system shall be so arranged that the pipe between the master gas valve and the engine is automatically purged with inert gas when the master gas valve is closed; or

.2 the gas fuel piping shall be installed within a ventilated pipe or duct. The air space between the gas fuel piping and the wall of the outer pipe or duct shall be equipped with mechanical underpressure ventilation having a capacity of at least 30 air changes per hour.

This ventilation capacity may be reduced to 10 air changes per hour provided automatic filling of the duct with nitrogen upon detection of gas is arranged for. The fan motors shall comply with the required explosion protection in the installation area. The ventilation outlet shall be screened and placed in a position where there are no flammable sources.

9.5.5.2 Pipes other than fuel pipelines including cable protection pipes may be made with double walls or enclosed in the ducts specified in 9.5.5.1.1 provided that they are not a flammable source and do not affect the integrity of double-wall pipes or duct. Double-wall pipes or duct shall contain only pipes or cables required for operation of gas fuel supply installation and test devices.

9.5.5.3 The connecting of gas piping and ducting of internal combustion engines leading to the gas injection valves shall be completely covered by the ducting. The arrangement of ducting shall facilitate replacement and maintenance of injection valves and cylinder covers. The double ducting is also required for all gas pipes on the engine itself, until gas is injected into the chamber. If gas is supplied into the air inlet directly on each individual cylinder during air intake to the cylinder on a low pressure engine, such that a single failure will not lead to release of fuel gas into the machinery space, double ducting may be omitted on the air inlet pipes.

9.5.6 Gas fuel supply in ESD protected machinery spaces.

9.5.6.1 The pressure in the gas fuel supply system pipelines in ESD protected machinery spaces shall not exceed 1 MPa.

9.5.6.2 The gas fuel supply lines shall have a design pressure not less than 1 MPa.

9.5.7 Regulations for the design of ventilated duct, outer pipe against inner pipe gas leakage.

9.5.7.1 The design pressure of the outer pipe or duct of fuel systems shall not be less than the maximum working pressure of the inner pipe. Alternatively, for fuel piping systems with a working pressure greater than 1 MPa, the design pressure of the outer pipe or duct shall not be less than the maximum built-up pressure arising in the annular space considering the local instantaneous peak pressure in way of any rupture and the ventilation arrangements.

9.5.7.2 For high-pressure fuel piping, the design pressure of the ducting shall be taken as the higher of the following:

1 the maximum built-up pressure: static pressure in way of the rupture resulting from the gas flowing in the annular space;

2 local instantaneous peak pressure in way of the rupture: this pressure shall be taken as the critical pressure determined by the following formula:

$$p = p_0 \left(\frac{2}{k+1} \right)^{k/(k-1)} \quad (9.5.7.2.2)$$

where p_0 = maximum working pressure of the inner pipe;

$k = C_p/C_v$ — constant pressure specific heat divided by the constant volume specific heat;
 $k = 1,31$ for CH_4 .

The tangential membrane stress of a straight pipe shall not exceed the tensile strength divided by 1,5 ($R_m/1,5$) when subjected to the above pressure. The pressure ratings of all other piping components shall reflect the same level of strength as straight pipes.

As an alternative to using the peak pressure in accordance with Formula (9.5.7.2.2), the peak pressure resulted from the tests conducted can be used.

9.5.7.3 Verification of the strength shall be based on calculations demonstrating the duct or pipe integrity. As an alternative to calculations, the strength can be verified by tests.

9.5.7.4 For low pressure fuel piping the duct shall be dimensioned for a design pressure not less than the maximum working pressure of the fuel pipe. The duct shall be pressure tested to show that it can withstand the expected maximum pressure at fuel pipe rupture.

9.5.8 Requirements for compressors and pumps.

9.5.8.1 If compressors or pumps are driven by shafting passing through a bulkhead or deck, the bulkhead penetration shall be of gastight type.

9.5.8.2 Compressors and pumps shall undergo special tests to ensure their suitability for use within a marine environment. The following, at least, shall be considered:

- 1** environmental conditions;
- 2** shipboard vibrations and accelerations;
- 3** effects of pitch heave and roll motions;
- 4** gas composition.

9.5.8.3 Arrangements shall be made to ensure that under no circumstances liquefied gas can be introduced in the gas control section or gas-fuelled machinery, unless the machinery is designed to operate with gas in liquid state.

9.5.8.4 Compressors and pumps shall be fitted with accessories and instrumentation necessary for efficient and reliable function.

9.6 GAS FUEL CONSUMERS ON BOARD SHIP

9.6.1 General requirements for internal combustion engines.

9.6.1.1 The exhaust gas system shall be equipped with explosion relief ventilation sufficiently dimensioned to prevent excessive explosion pressures in the event of ignition failure of one cylinder followed by ignition of the unburned gas in the system.

9.6.1.2 For engines where the space below the piston is in direct communication with the crankcase, a detailed evaluation regarding the hazard potential of fuel gas accumulation in the crankcase shall be carried out and reflected in the safety concept of the engine.

9.6.1.3 Each engine other than two-stroke cross-head type diesel engines shall be fitted with vent systems independent of other engines for crankcases and sumps.

9.6.1.4 Where gas can leak directly into the working media of auxiliary system (lubricating oil, cooling water), appropriate means shall be fitted after the engine outlet to extract gas in order to prevent gas dispersion. The gas extracted from the working media of auxiliary systems shall be vented to a safe location in the atmosphere.

9.6.1.5 For engines fitted with ignition systems, prior to admission of gas fuel, correct operation of the ignition system on each unit shall be verified.

9.6.1.6 A means shall be provided to monitor and detect poor combustion or misfiring. In the event that it is detected, gas operation may be allowed provided that the gas fuel supply to the concerned cylinder is shut off and provided that the operation of the engine with one cylinder cut-off is acceptable with respect to torsional vibrations.

9.6.1.7 For engines starting on fuels in accordance with 9.1.1, if combustion has not been detected by the engine monitoring system within an engine specific time after the opening of the fuel supply valve, the fuel supply valve shall be automatically shut off. Means to ensure that any unburnt fuel mixture is purged away from the exhaust system shall be provided.

9.6.2 Requirements for dual fuel internal combustion engines.

9.6.2.1 In case of shutoff of the gas fuel supply, the engines shall be capable of continuous operation by oil fuel only, without interruption.

9.6.2.2 An automatic system shall be fitted to change over from gas fuel operation to oil fuel operation and vice versa with minimum deviations of the engine power from the mean value. Acceptable reliability shall be demonstrated through testing. In case of unstable operation on engines when gas firing, the engine shall automatically change to oil fuel mode. Manual activation of gas system shutdown shall always be possible.

9.6.2.3 In case of a normal stop or an emergency shutdown, the gas fuel supply shall be shut off not later than the ignition source. It shall not be possible to shut off the ignition source without first or simultaneously closing the gas supply to each cylinder or to the complete engine.

9.6.3 Requirements for gas-only engines.

9.6.3.1 In case of a normal stop or an emergency shutdown, the gas fuel supply shall be shut off not later than the ignition source. It shall not be possible to shut off the ignition source without first or simultaneously closing the gas supply to each cylinder or to the complete engine.

9.6.4 Requirements for multi-fuel engines

9.6.4.1 In case of shutoff of one fuel supply, the engines shall be capable of continuous operation by an alternative fuel with minimum deviations of the engine power.

9.6.4.2 An automatic system shall be fitted to change over from one fuel operation to an alternative fuel operation with minimum deviations of the engine power from the mean value. Acceptable reliability shall be demonstrated through testing. In the case of unstable operation on an engine when using a particular fuel, the engine shall automatically change to an alternative fuel mode. Manual activation shall always be possible.

Table 9.6.4.2

	Gas only		Dual fuel	Multi fuel
Ignition medium	Spark	Pilot fuel	Pilot fuel	N/A
Main fuel	Gas	Gas	Gas and/or oil fuel	Gas and/or liquid

9.6.5 Requirements for main and auxiliary boilers.

9.6.5.1 Each boiler shall have a dedicated forced draught system. A crossover between boiler force draught systems may be fitted for emergency use providing that any relevant safety functions are maintained.

9.6.5.2 Combustion chambers and uptakes of boilers shall be designed to prevent any accumulation of gaseous fuel.

9.6.5.3 Burners shall be designed to maintain stable combustion after ignition under all operational conditions.

9.6.5.4 For main propulsion boilers an automatic system shall be provided to change from gas fuel operation to oil fuel operation without interruption of boiler firing.

9.6.5.5 Gas nozzles and the burner control system shall be configured such that gas fuel can only be ignited by an established oil fuel flame, unless the boiler and ignition system is designed and approved by the Administration to light on gas fuel.

9.6.5.6 There shall be arrangements to ensure that gas fuel flow to the burner is automatically cut off unless satisfactory ignition has been established and maintained.

9.6.5.7 On the fuel pipe of each gas burner a manually operated shut-off valve shall be fitted.

9.6.5.8 Provisions shall be made for automatically purging the gas supply piping to the burners by means of an inert gas after the extinguishing of these burners.

9.6.5.9 The automatic fuel changeover system in accordance with 9.6.5.4 shall be monitored with alarms to ensure continuous availability.

9.6.5.10 Arrangements shall be made that, in case of flame failure of all operating burners, the combustion chambers of the boilers are automatically purged before relighting.

9.6.5.11 Arrangements shall be made to enable the boilers purging sequence to be manually activated.

9.6.6 Requirements for gas turbines.

9.6.6.1 Unless designed with the strength to withstand the worst-case overpressure due to ignited gas leaks, pressure relief systems shall be suitably designed and fitted to the exhaust system, taking into considera-

tion the explosions due to gas leaks. Pressure relief systems within the exhaust uptakes shall be lead to a safe location, away from personnel.

9.6.6.2 The gas turbine may be fitted in a gastight enclosure arranged in accordance with the ESD principle (refer to 9.2.4.3 and 9.5.6), however a pressure above 1 MPa in the gas supply piping may be accepted within this enclosure.

9.6.6.3 Gas detection systems and shutdown functions shall be as outlined for ESD protected machinery spaces.

9.6.6.4 Ventilation for the enclosure shall be as specified in 9.8 for ESD protected machinery spaces, but shall in addition be arranged with full redundancy ($2 \times 100\%$ capacity fans from different electrical circuits).

9.6.6.5 For other than single-fuel gas turbines, an automatic system shall be fitted to change over easily and quickly from gas fuel operation to oil fuel operation and vice-versa with minimum deviations of the engine power from the mean value.

9.6.6.6 Means shall be provided to monitor and detect poor combustion that may lead to unburnt fuel gas in the exhaust gas system during operation. In the event that it is detected, the fuel gas supply shall be shutdown.

9.6.6.7 Each turbine shall be fitted with an automatic shutdown device when maximum exhaust temperatures are exceeded.

9.7 FIRE PROTECTION

9.7.1 General.

9.7.1.1 Fire protection shall comply with the requirements of this Section of Part VI "Fire Protection" depending on the purpose of the ship.

9.7.2 Structural fire protection.

9.7.2.1 Any boundary of accommodation spaces, service spaces, control stations, escape routes, machinery spaces facing gas fuel storage tanks on the open deck, shall be shielded by A-60 class divisions. These A-60 class divisions shall extend up to the underside of the deck of the navigation bridge. Any structures above these including navigation bridge windows shall be A-0 class divisions. Gas fuel storage tanks shall be segregated from cargo and arranged in accordance with the requirements of the International Maritime Dangerous Goods (IMDG) Code where these tanks are considered a class 2.1 package.

9.7.2.2 Gas fuel tank rooms and ventilation ducts serving these spaces shall be separated from accommodation, service, cargo and machinery spaces by class A-60 fire structures. They may be separated from other spaces with low fire risk by class A-0 fire structures. The space containing fuel containment system shall be separated from the machinery spaces of category A or

other rooms with high fire risks by a cofferdam of at least 900 mm wide insulated to A-60 class. Where this space is adjacent to spaces with low fire risk, it shall be considered as a machinery space of category A and may be separated by both a cofferdam at least 900 mm long and A-60 class division. For type C tanks, the fuel storage space may be considered as a cofferdam.

9.7.2.3 Gas pipes led through ro-ro spaces on open deck shall be provided with special guards to prevent vehicle collision damage.

9.7.2.4 Where more than one machinery space is arranged on board the ship, they shall be separated by class A-60 divisions.

9.7.2.5 Any space containing equipment for the fuel preparation such as pumps, compressors, heat exchangers, vaporizers and pressure vessels shall be considered as a machinery space of category A for fire protection purposes.

9.7.2.6 The bunkering station shall be separated by class A-60 divisions towards machinery spaces of category A, accommodation spaces, control stations and high fire risk spaces, except for spaces such as tanks, voids, auxiliary machinery spaces of little or no fire risk, sanitary and other similar spaces where the insulation standard may be reduced to class A-0.

9.7.2.7 The gas fuel hold space shall not be used for machinery or equipment that may have a fire risk (refer also to 9.7.2.2).

9.7.2.8 If an ESD protected machinery spaces is separated by a single boundary, the boundary shall be of A-60 class division.

9.7.3 Water fire main system.

9.7.3.1 The water fire main system shall comply with the requirements of 3.2, Part VI "Fire Protection" with due regard to the purpose of the ship.

9.7.3.2 Where fire main pumps are used for the water spray system, the required pump capacity shall be determined for the case of both the water fire main system and the water spray system being in operation.

9.7.3.3 Where FST are located on open deck, the fire water mains shall be provided with a shut-off valve to isolate the damaged pipe section with the system remaining operable all the time.

9.7.4 Water spray system.

9.7.4.1 A water spray system shall be installed for cooling and fire prevention to cover exposed parts of FSTs located on open deck. The water spray system shall also provide coverage for exposed structures of super-structures, compressor rooms and pump rooms, cargo control rooms, bunkering stations and any other normally occupied spaces that face the FST on the open decks if the distance between them does not exceed 10 m.

9.7.4.2 The system shall be designed to cover all areas specified in 9.7.4.1 with an application rate as follows:

- .1 10 l/min/ per 1 m² for horizontal surfaces;
- .2 4 l/min/ per 1 m² for vertical surfaces.

9.7.4.3 Stop valves shall be fitted in the water spray application main supply line, at intervals not exceeding 40 m for the purpose of isolating damaged sections. Alternatively, the system may be divided into two or more sections that may be operated independently, provided the necessary controls are located together in a readily accessible position not likely to be inaccessible in case of fire in the areas protected.

9.7.4.4 Connection of the the water spray system to the water spray system shall be provided through a stop valve fitted on the exposed deck area in a safe position outside the bunkering station area.

9.7.4.5 Remote start of pumps supplying the water spray system and remote operation of valves shall be located in a readily accessible safe position which is not likely to be cut off in case of fire.

9.7.4.6 The nozzles of the water spray system shall be of a full bore type and ensure an effective distribution of water throughout the areas being protected.

9.7.5 Dry chemical powder fire-extinguishing system.

9.7.5.1 To protect the bunkering station area and cover all possible leak points a dry chemical powder system complying with the requirements of Part VI "Fire Protection" shall be provided. The capacity of the dry chemical powder fire-extinguishing system shall be at least 3,5 kg/s and the power capacity shall be sufficient for a minimum of 45 s discharges.

9.7.6 Fire detection and alarm system.

9.7.6.1 In gas fuel storage spaces and in ventilation ducts leading thereto, a fire detection system of an approved type shall be provided.

The system shall ensure clear identification of the activated detector and determine its location.

9.7.6.2 A smoke detection system cannot be considered as an efficient and quick-acting means of fire detection in accordance with **9.7.6.1**, unless other fire detecting equipment is provided additionally.

9.7.7 Fire-fighting outfit.

9.7.7.1 Two portable dry chemical powder fire extinguishers, each of at least 5 kg capacity shall be provided, one of which shall be located in the vicinity of the bunkering station.

9.7.7.2 The machinery space where the gas fuel is heavier than air shall be provided with two dry chemical powder extinguishers of at least 5 kg capacity each, located at the entrance.

9.8 VENTILATION

9.8.1 General.

9.8.1.1 Any ducting used for the ventilation of hazardous spaces shall be separate from that used for the ventilation of non-hazardous spaces. The ventilation

shall be operable at all temperatures and environmental conditions the ship will be operating in.

9.8.1.2 Electric motors for ventilation fans shall not be located in ventilation ducts for hazardous spaces unless the motors are certified for the same hazard zone as the space served.

9.8.1.3 Design of ventilation fans serving spaces containing gas sources shall comply with the following:

.1 ventilation fans shall not produce a source of vapour ignition in either the ventilated space or the ventilation system associated with the space. Ventilation fans and fan ducts, in way of fans only, shall be intrinsically safe defined as follows:

.1 for impellers or housings of non-metallic material, due regard being paid to the elimination of static electricity;

.2 impellers and housings of non-ferrous metals;

.3 impellers and housings of austenitic stainless steel;

.4 impellers of aluminum alloys or magnesium alloys and a ferrous (including austenitic stainless steel) housing on which a ring of suitable thickness of non-ferrous materials is fitted in way of the impeller, due regard being paid to static electricity and corrosion between ring and housing; or

.5 any combination of ferrous (including austenitic stainless steel) impellers and housings with not less than 13 mm tip design clearance;

.2 under no circumstances shall the radial air gap between the impeller and the casing be less than 0,1 of the diameter of the impeller shaft in way of the bearing but not less than 2 mm. The gap need not be more than 13 mm;

.3 any combination of an aluminium or magnesium alloy fixed or rotating component and a ferrous fixed or rotating component, regardless of tip clearance, is considered a sparking hazard and shall not be used in hazardous areas.

9.8.1.4 Ventilation systems required to avoid any gas accumulation shall consist of independent fans, each of sufficient capacity, unless otherwise specified in these requirements.

9.8.1.5 Air inlets for hazardous enclosed spaces shall be taken from areas that, in the absence of the considered inlet, would be non-hazardous. Air inlets for non-hazardous enclosed spaces shall be taken from non-hazardous areas at least 1,5 m away from the boundaries of any hazardous area. Where the inlet duct passes through a more hazardous space, the duct shall be gastight and have overpressure relative to this space.

9.8.1.6 Air outlets from non-hazardous spaces shall be located outside hazardous areas.

9.8.1.7 Air outlets from hazardous enclosed spaces shall be located in an open area that, in the absence of the considered outlet, would be of the same or lesser hazard than the ventilated space.

9.8.1.8 The required capacity of the ventilation plant is normally based on the total volume of the room.

An increase in required ventilation capacity may be necessary for rooms having a complicated form.

9.8.1.9 Non-hazardous spaces with entry openings to a hazardous area shall be arranged with an air lock and be maintained at overpressure relative to the external hazardous area. The overpressure ventilation shall be arranged according to the following:

.1 during initial start-up or after loss of overpressure ventilation, before energizing any electrical installations not certified safe for the space in the absence of pressurization, it shall be required to:

.1.1 proceed with purging (at least 5 air changes) or confirm by measurements that the space is non-hazardous; and

.1.2 pressurize the space;

.2 operation of the overpressure ventilation shall be monitored and in the event of failure of the overpressure ventilation the following shall be performed:

.2.1 an audible and visual alarm shall be given at a manned location; and

.2.2 if overpressure cannot be immediately restored, automatic or programmed disconnection of electrical installations shall be required.

9.8.1.10 Non-hazardous spaces with entry openings to a hazardous enclosed space shall be arranged with an air lock and the hazardous space shall be maintained at underpressure relative to the non-hazardous space. Operation of the exhaust ventilation in the hazardous space shall be monitored and in the event of failure of the exhaust ventilation the following shall be performed:

.1 an audible and visual alarm shall be given at a manned location; and

.2 if underpressure cannot be immediately restored, automatic or programmed disconnection of electrical installations according to a recognized standard shall be required at a non-hazardous area.

9.8.2 Requirements for ventilation of tank connection spaces.

9.8.2.1 The tank connection space shall be provided with an effective mechanical forced exhaust ventilation system. A ventilation capacity of at least 30 air changes per hour shall be provided. The rate of air changes may be reduced if other adequate means of explosion protection are installed. The equivalence of alternative installations shall be demonstrated by a risk assessment.

9.8.2.2 Approved automatic fail-safe fire dampers shall be fitted in the ventilation duct for the tank connection space.

9.8.3 Requirements for ventilation of machinery spaces.

9.8.3.1 The ventilation system for machinery spaces containing gas-fuelled consumers shall be independent of all other ventilation systems.

9.8.3.2 ESD protected machinery spaces shall have ventilation with a capacity of at least 30 air changes per hour. The ventilation system shall ensure a good air

circulation in all spaces, and in particular ensure that any formations of gas pockets in the room are detected. As an alternative, arrangements whereby under normal operation the machinery spaces are ventilated with at least 15 air changes an hour are acceptable provided that if gas is detected in the machinery space, the number of air changes will automatically be increased to 30 per hour.

9.8.3.3 For ESD protected machinery spaces the ventilation arrangements shall provide sufficient redundancy to ensure a high level of ventilation availability as defined in a standard agreed upon with the Register.

9.8.3.4 The number and power of the ventilation fans for ESD protected machinery spaces and for double pipe ventilation systems for gas-safe machinery spaces shall be such that the capacity is not reduced by more than 50 % of the total ventilation capacity if a fan with a separate circuit from the main switchboard or emergency switchboard or a group of fans with common circuit from the main switchboard or emergency switchboard, is inoperable.

9.8.4 Requirements for ventilation of fuel preparation rooms.

9.8.4.1 Fuel preparation rooms shall be fitted with effective mechanical ventilation system of the underpressure type providing a ventilation capacity of at least 30 air changes per hour.

9.8.4.2 The number and power of the ventilation fans shall be such that the capacity is not reduced by more than 50 per cent, if a fan with a separate circuit from the main switchboard or emergency switchboard or a group of fans with common circuit from the main switchboard or emergency switchboard, is inoperable.

9.8.4.3 Ventilation systems for fuel preparation rooms shall be in operation when pumps or compressors are working.

9.8.5 Requirements for ventilation of bunkering stations.

Bunkering stations that are not located on the open deck shall be suitably ventilated to ensure that any vapour being released during bunkering operations will be removed outside. If the natural ventilation is not sufficient, mechanical ventilation shall be provided in accordance with the risk assessment as specified in 9.5.2.1.

9.8.6 Requirements for ventilation of ducts and double pipes.

9.8.6.1 Ducts and double pipes containing fuel piping shall be fitted with effective mechanical ventilation system of the extraction type providing a ventilation capacity of at least 30 air changes per hour. This requirement is not applicable to double pipes in the machinery space if the requirements of 9.5.5.1.1 are complied with.

9.8.6.2 The ventilation system for double piping and for gas valve unit spaces in gas-safe machinery spaces shall be independent of all other ventilation systems.

9.8.6.3 The ventilation inlets for the double pipes or ducts shall always be located in a non-hazardous area

away from ignition sources. The inlet openings shall be fitted with suitable wire mesh guards and protected from ingress of water.

9.8.6.4 The capacity of the ventilation for a pipe duct or double pipes may be below 30 air changes per hour if a flow velocity of minimum 3 m/s is ensured. The flow velocity shall be calculated for the duct with fuel pipes and other components installed.

9.9 INERTING AND ATMOSPHERE CONTROL

9.9.1 Inerting of fuel tanks.

9.9.1.1 A piping system shall be arranged to enable each fuel tank to be safely gas-freed, and to be safely filled with fuel from a gas-free condition. The system shall be arranged to minimize the possibility of gas or air pockets remaining after changing the atmosphere.

9.9.1.2 The system shall be designed to eliminate the possibility of a flammable mixture existing in the fuel tank during any part of the atmosphere change operation by utilizing an inerting medium as an intermediate step.

9.9.1.3 Gas sampling points shall be provided for each fuel tank to monitor the progress of atmosphere change.

9.9.1.4 Inert gas utilized for gas freeing of fuel tanks may be provided externally to the ship.

9.9.2 Atmosphere control within fuel storage hold spaces (other than type C tanks).

9.9.2.1 Interbarrier and fuel storage hold spaces associated with liquefied gas fuel containment systems requiring full or partial secondary barriers shall be inerted with a suitable dried inert gas and kept inerted with make-up gas provided by a shipboard inert gas generation plant, or by shipboard storage, which shall be sufficient for normal consumption for at least 30 days.

9.9.2.2 The spaces referred to in 9.9.2.1 requiring only a partial secondary barrier may be filled with dry air provided that the ship maintains a stored charge of inert gas or is fitted with an inert gas generation plant sufficient to inert the largest of these spaces, and provided that the configuration of the spaces and the relevant vapour detection systems, together with the capability of the inerting arrangements, ensures that any leakage from the LNG tanks will be rapidly detected and inerting effected before a dangerous condition can develop.

Equipment to produce sufficient amount of suitable quality dry air shall be provided to satisfy the expected demand.

9.9.3 Environmental control of spaces surrounding type C tanks.

9.9.3.1 Spaces surrounding LNG tanks shall be filled with suitable dry air and be maintained in this condition with dry air provided by suitable air drying equipment. This requirement is only applicable for LNG tanks where

condensation and icing due to cold surfaces is are possible.

9.9.4 Requirements for inerting.

9.9.4.1 Arrangements to prevent back-flow of fuel vapour into the inert gas system shall be provided. To prevent the return of flammable gas to any gas-safe spaces the inert gas supply line shall be fitted with two shutoff valves in series with a venting valve in between (double block and bleed valves). In addition, a closable non-return valve shall be installed between the double block and bleed arrangement and the fuel system. These valves shall be located outside gas-safe spaces.

9.9.4.2 Where the connections to the fuel piping systems are non-permanent, two non-return valves may be substituted for the valves specified in 9.9.4.1

9.9.4.3 The arrangements shall be such that each space being inerted can be isolated and the necessary controls and relief valves, etc. shall be provided for controlling pressure in these spaces.

9.9.4.4 Where insulation spaces are continually supplied with an inert gas as part of a leak detection system, means shall be provided to monitor the quantity of gas being supplied to individual areas and spaces.

9.9.5 Inert gas production and storage on board.

9.9.5.1 Inert gas generation plant shall be capable of producing inert gas with at no time greater than 5 per cent oxygen content by volume.

A continuous-reading oxygen content meter shall be provided at the inert gas generator output and shall be fitted with an alarm set at a maximum of 5 per cent oxygen content by volume.

9.9.5.2 An inert gas system shall be fitted with pressure controls and monitoring arrangements appropriate to the fuel containment system.

9.9.5.3 Where a nitrogen generator or nitrogen storage facilities are installed in a separate compartment outside the machinery space, this compartment shall be fitted with a mechanical extraction ventilation system with the capacity of at least 6 air changes per hour. A low oxygen alarm shall be fitted.

9.9.5.4 Inert gas pipelines shall only be laid through well ventilated spaces. Pipelines in enclosed spaces shall:

- be fully welded;
- have only a minimum of flange connections as needed for fitting of valves; and
- be as short as possible.

9.10 MONITORING, CONTROL AND AUTOMATION SYSTEMS

9.10.1 General.

9.10.1.1 Monitoring, control and automation systems shall comply with the requirements of 2.4, Part XV "Automation".

9.10.2 Pressure, level and temperature monitoring.

9.10.2.1 Each gas fuel tank shall be provided with devices for remote monitoring from the bridge and local monitoring of fuel pressure and temperature. The devices shall be clearly marked with upper and lower range values of allowable working pressure. Provision shall be made for upper and lower pressure alarms in the tank (where vacuum protection is required by tank design) which shall be activated before safety valve operation.

9.10.2.2 The gas fuel inlet pipe shall be fitted with a device for pressure control between the inlet valve and shore connection.

9.10.2.3 On the gas fuel outlet piping following the pump and on the gas fuel inlet piping following the inlet valve shall be provided with a pressure control device.

9.10.2.4 In the drain well of LNG tank storage space, level indicators and temperature indicating devices shall be fitted. As a result of temperature sensor activation, the main gas valve of the tank shall be automatically closed. Upper level indicator shall activate an alarm.

9.10.2.5 The LNG tanks shall be provided with level indicators as well as arrangements giving visual and audible lower liquid level signals and ensuring automatic shutdown of motors of fixed and submersible fuel pumps with subsequent visual and audible alarm. These signals shall be given at the navigation bridge, continuously manned central control station or onboard safety centre.

9.10.3 Gas tank overflow prevention.

9.10.3.1 Each LNG tank shall be provided with means of overflow prevention in compliance with the requirements for cargo tanks of gas carriers specified in 3.1, Part VIII "Instrumentation" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk. Overflow prevention means shall be independent of level indicators specified in 9.10.2.4.

9.10.3.2 Each CNG tank shall be provided with means of overpressure prevention during bunkering with an alarm to be activated when reaching 95 per cent of design pressure.

9.10.4 Gas leaks control in spaces.

9.10.4.1 All enclosed gas-dangerous spaces shall be provided with effective gas detection systems in areas of its possible accumulation and leakage. The number of detectors to be fitted in each space is subject to special consideration in each case with due regard to the size and configuration of the space. When the gas concentration equal to 20 % of the lower explosion limit is reached in the controlled space, visual and audible alarm is to be given on the bridge. In ventilation ducts containing gas-fuel pipes, the alarm shall be given when the concentration equal to 30 % of the lower explosion limit is reached. If the concentration equal to 40 % of the lower explosion limit is reached, measures (at least those stated in Table 9.10.4.4) to automatically shut down gas-fuel supply to the space shall be taken.

9.10.4.2 In the gas-dangerous machinery spaces, two independent systems are required to control gas supply to the machinery space.

9.10.4.3 In gas-safe machinery spaces at least two detectors of the gas supply control system shall be fitted to activate alarm at reaching 30 % of the lower explosion limit.

9.10.4.4 Where gas-fuel leakage is found and in case of system failure, the safety system shall automatically activate regulating functions stated in Table 9.10.4.4.

9.11 ELECTRICAL EQUIPMENT**9.11.1 General.**

9.11.1.1 Electrical equipment shall comply with the requirements of Part VII "Electrical Equipment" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk. The hazardous zones shall be classified in accordance with 9.11.2.

9.11.2 Classification of hazardous zones, spaces and areas.

9.11.2.1 The classification of hazardous zones shall be in compliance with IEC 60079-10 and IEC 60092-502. If a dangerous space is not covered by 9.11.2, refer to the above standards.

9.11.2.2 Zone 0: the internal areas of gas fuel storage tanks, gas fuel pipelines, pipelines from safety valves of gas fuel storage tanks and any air pipelines from equipment containing gas.

9.11.2.3 Zone 1: gas fuel tank storage rooms; gas compressor spaces; area on open deck or semi-enclosed spaces on the open deck within 3 m of safety valve outlet, covers or manholes of gas fuel storage tank on open deck as well as its sounding pipes, flanges and valves of gas inlet piping and other gas fittings, inlets and ventilation openings leading to compressor and pump rooms, gas fuel tank storage rooms; area on open deck or semi-enclosed spaces on open deck within 1,5 m of gas compressor and pump room entrances, ventilation outlets and inlets serving these and any other rooms classified as zone 1; area on open deck within a coaming surrounding bunkering station and within a radius of 3 m around the coaming up to a height of 2,4 m; enclosed or semi-enclosed spaces surrounding pipes containing gas and ventilation ducts around gas pipes; gas-dangerous machinery spaces are considered as non-hazardous areas during normal operation and as zone 1 after actuation of gas leakage alarm.

9.11.2.4 Zone 2: Area on open deck within 1,5 m surrounding zone 1.

9.11.3 Electrical equipment required for ship's propulsion, power generation, manoeuvring, anchorage and mooring, emergency fire pumps shall not be located within spaces separated from hazardous zones by air locks or shall be of a certified safe type.

Table 9.10.4.4

Monitored parameter	Alarm	Automatic closure of master gas fuel valve ⁷	Automatic shutdown of gas supply to consumers in machinery space	Notes	
Gas detection in gas fuel tank storage room above 20 % LEL	×			If double pipes are provided for gas supply to consumers If double pipes are provided for gas supply to consumers Gas detectors are required for protection of gas-dangerous machinery spaces only Gas detectors are required only for protection of gas-dangerous machinery spaces containing gas consumers. The non-explosion proof equipment in the machinery spaces with gas consumers shall be also disconnected If double pipes are provided for gas supply to consumers For protection of gas-dangerous machinery spaces only Time delay as found necessary	
Gas detection by two detectors ¹ in gas fuel tank storage room above 40 % LEL	×	×			
Fire detection in gas fuel tank storage room	×	×			
Bilge well high level in gas fuel tank storage room	×				
Bilge well low temperature in gas fuel tank storage room	×	×			
Gas detection in the duct between gas fuel tank and machinery space containing gas consumers above 20 % LEL	×				
Gas detection by two detectors ¹ in the duct between gas fuel tank and machinery space containing gas consumers above 40 % LEL	×	×	×		
Gas detection in gas compressor room above 20 % LEL	×				
Gas detection by one of two detectors ¹ in gas compressor room above 40 % LEL	×				
Gas detection in the duct inside machinery space containing gas consumers above 30 % LEL	×				
Gas detection by two detectors ¹ in a duct inside machinery space containing gas consumers above 40 % LEL	×		×		
Gas detection in machinery space containing gas consumers above 20 % LEL	×				
Gas detection by one of two detectors ¹ in machinery space containing gas consumers above 40% LEL	×		×		
Loss of ventilation in the duct between tank and machinery space containing gas consumers ⁶	×		×		
Loss of ventilation in the duct inside machinery space containing gas consumers ⁶	×		×		
Loss of ventilation in machinery space containing gas consumers	×		×		
Fire detection in machinery space containing gas consumers	×		×		
Abnormal gas pressure in gas supply pipe	×		×		
Failure in valve control system	×		×		
Automatic shutdown of engine (engine failure)	×		×		
Emergency shutdown of engine (manually or by operator)	×		×		
¹ Two independent gas detectors located close to each other are required for redundancy reasons. If gas detectors are of self-monitoring type, the installation of a single gas detector is permitted. ² If the gas fuel tank is supplying gas to more than one consumer and different supply pipes are completely separated and fitted in separate ducts with an individual master valve fitted outside of the duct, only the master valve leading into the duct where gas or loss of ventilation is detected shall close. ³ If the gas fuel is supplied to more than one consumer and different supply pipes are completely separated and fitted in separate ducts with an individual master valve fitted outside of the duct and machinery space, only the master valve leading into the duct where gas or loss of ventilation is detected shall close. ⁴ This parameter shall not lead to shutdown of gas supply for single-fuel gas engines. Applicable for dual-fuel gas engines only. ⁵ Only for the case of 3 valves activation, as specified in 9.5.4.4. ⁶ If the duct is protected by inert gas (refer to 9.5.5.1.1), then loss of inert gas pressure shall lead to the same actions, as specified in this table. ⁷ Valves specified in 9.5.4.1.					

9.12 PERSONNEL PROTECTION

9.12.1 Where the equipment of the gas containing system is installed in enclosed spaces of the ship, provision shall be made for at least two sets of protective equipment each permitting personnel to enter and work in spaces filled with natural gas.

9.12.2 A set of protective equipment, specified in **9.12.1** shall include the following:

- .1** one self-contained breathing apparatus not using stored oxygen with a capacity of at least 1200 l of free air;
- .2** tight-fitting goggles, gloves, intrinsically safe protective clothing and boots;
- .3** steel-cored rescue line with an intrinsically safe belt;
- .4** explosion-proof lamp.

9.12.3 For breathing apparatuses mentioned in **9.12.2.1**, fully charged air bottles with a total free air

capacity of 3600 l for each breathing apparatus shall be provided.

9.12.4 Medicines and medical first-aid equipment shall be available on board for persons suffering from burns, frostbites (including cryogenic ones) as well as intoxication with natural gas or products of incomplete fuel burning.

9.12.5 The following operating documentation shall be available on board:

- .1** gas fuel bunkering instructions;
- .2** inerting and gas freeing instructions;
- .3** instructions for using gas fuel;
- .4** instructions describing the crew actions in emergencies which may arise during operations with gas fuel.

9.12.6 A plan of periodic audits and maintenance of equipment related to the use of gas as fuel shall be provided on board.

10 REQUIREMENTS TO BALTIC ICE CLASS SHIPS

10.1 GENERAL

10.1.1 Requirements for the Baltic ice class ships comply with the requirements of the Finnish-Swedish Ice Class Rules, 2010 and apply to the ships operating in the Baltic Sea area in winter and water areas of other seas with similar ice conditions.

10.2 BALTIC ICE CLASSES

10.2.1 Ships complying with the requirements of the present Section may be assigned to the Baltic ice classes as follows:

.1 ice class **IA Super**: ships with such structure, engine output and other properties that they are normally capable of navigating in difficult ice conditions without the assistance of icebreakers;

.2 ice class **IA**: ships with such structure, engine output and other properties that they are capable of navigating in difficult ice conditions, with the assistance of icebreakers when necessary;

.3 ice class **IB**: ships with such structure, engine output and other properties that they are capable of navigating in moderate ice conditions, with the assistance of icebreakers when necessary;

.4 ice class **IC**: ships with such structure, engine output and other properties that they are capable of navigating in light ice conditions, with the assistance of icebreakers when necessary;

.5 ice class **II**: ships that have a steel hull and that are structurally fit for navigation in the open sea and that, despite not being strengthened for navigation in ice, are capable of navigating in very light ice conditions with their own propulsion machinery;

.6 ice class **III**: ships that do not belong to the ice classes referred to in 10.2.1.1 — 10.2.1.5.

10.3 ICE CLASS DRAUGHT

10.3.1 Upper and lower ice waterlines.

10.3.1.1 The upper ice waterline (UIWL) shall be the envelope of the highest points of the waterlines at which the ship is intended to operate in ice. The line may be a broken line.

The lower ice waterline (LIWL) shall be the envelope of the lowest points of the waterlines at which the ship is intended to operate in ice. The line may be a broken line.

10.3.2 Maximum and minimum draught fore and aft.

10.3.2.1 The maximum and minimum ice class draughts at fore and aft perpendiculars shall be determined in accordance with UIWL and LIWL.

Restrictions on draughts when operating in ice shall be documented and kept on board readily available to the master. The maximum and minimum ice class draughts fore, amidships and aft shall be indicated in the Annex to Classification Certificate (form 3.1.2-1). If the summer load line in fresh water is anywhere located at a higher level than the UIWL, the ship's sides are to be provided with a warning triangle and with an ice class draught mark at the maximum permissible ice class draught amidships (refer to Appendix), which are also specified in the Annex to Classification Certificate (form 3.1.2-1).

The draught and trim, limited by the UIWL, must not be exceeded when the ship is navigating in ice. The salinity of the sea water along the intended route shall be taken into account when loading the ship.

The ship shall always be loaded down at least to the LIWL when navigating in ice. Any ballast tank, situated above the LIWL and needed to load down the ship to this water line, shall be equipped with devices to prevent the water from freezing. In determining the LIWL, regard shall be paid to the need for ensuring a reasonable degree of ice-going capability in ballast. The propeller shall be fully submerged, if possible entirely below the ice. The forward draught shall be at least $(2 + 0,00025\Delta)h_0$ but need not exceed $4h_0$

where Δ = displacement of the ship, in t, on the maximum ice-class draught according to 10.3.1.1;

h_0 = level ice thickness, in m, according to 10.5.2.1.

10.4 ENGINE OUTPUT

10.4.1 Definitions and explanations.

10.4.1.1 The engine output P is the maximum output the propulsion machinery can continuously deliver to the propellers.

The dimensions of the ship and some other parameters are defined below (refer to Fig. 10.4.1.1):

L — length of the ship between the perpendiculars, in m;

L_{BOW} — length of the bow, in m;

L_{PAR} — length of the parallel midship body, in m;

B — breadth of the ship, in m;

T — draught of the ship, in m;

A_{wf} — area of the waterline of the bow, in m²;

α — the angle of the waterline at B/4, in deg.;

φ_1 — the rake of the stem at the centerline, in deg.

$\varphi_1 = 90^\circ$ for a ship with a bulbous bow;

φ_2 — the rake of the bow at $B/4$, in deg.;
 ψ — flare angle calculated as $\psi = \arctan(\tan\varphi/\sin\alpha)$, in deg., φ using angles α and φ . For 10.4.3 flare angle is calculated using $\varphi = \varphi_2$;

D_p — diameter of the propeller, in m;
 H_M — thickness of the brash ice in mid channel, in m;
 H_F — thickness of the brash ice layer displaced by the bow, in m.

10.4.2 The engine output shall not be less than that determined in 10.4.3.

Irrespective of the engine output determination by Formula (10.4.3-1), The engine output shall not be less than 1000 kW for ice classes **IA**, **IB** and **IC** and not less than 2800 kW for ice class **IA Super**.

10.4.3 The engine output requirement shall be calculated for two draughts. The engine output shall not be less than the greater of these two outputs.

In the calculations the ship's parameters specified in 10.4.1.1 which depend on the draught are to be determined at the appropriate draught, but L and B shall be determined only at the UIWL.

$$P = K_e \frac{(R_{CH}/1000)^{3/2}}{D_p}, \text{ in kW}, \quad (10.4.3-1)$$

where K_e shall be taken according to Table 10.4.3;

R_{CH} — is the ice resistance in Newton of the ship in a channel with brash ice and a consolidated surface layer, in N.

Table 10.4.3

Number of propellers	CP propeller or electric or hydraulic propulsion machinery	FP propeller
1	2,03	2,26
2	1,44	1,60
3	1,18	1,31

$$R_{CH} = C_1 + C_2 + C_3 C_\mu (H_F + H_M)^2 (B + C_\psi H_F) + C_4 L_{PAR} H_F^2 + C_5 \left(\frac{LT}{B^2} \right)^3 \frac{A_{wf}}{L} \quad (10.4.3-2)$$

where $C_\mu = 0,15 \cos\varphi_2 + \sin\psi \sin\alpha$, C_μ shall be taken equal or larger than 0,45;
 $C_\psi = 0,047\psi - 2,115$, and $C_\psi = 0$, if $\psi < 45^\circ$;
 $H_F = 0,26 + (H_M B)^{0,5}$;
 $H_M = 1,0$ m for ice classes **IA** and **IA Super**;
 $H_M = 0,8$ m for ice class **IB**;
 $H_M = 0,6$ m for ice class **IC**;
 $C_1 = 0$ for ice classes **IA**, **IB** and **IC**;

$$C_1 = f_1 \frac{BL_{PAR}}{2(T/B) + 1} + (1 + 0,021\varphi_1)(f_2 B + f_3 L_{BOW} + f_4 L_{BOW}) \quad \text{for ice class IA Super};$$

$$f_1 = 23 \text{ N/m}^2;$$

$$f_2 = 45,8 \text{ N/m};$$

$$f_3 = 14,7 \text{ N/m};$$

$$f_4 = 29 \text{ N/m}^2.$$

$$C_2 = 0 \text{ for ice classes IA, IB and IC};$$

$$C_2 = (1 + 0,063\varphi_1)(g_1 + g_2 B) + g_3(1 + 1,2 \frac{T}{B}) \frac{B^2}{\sqrt{L}}$$

for ice class **IA Super**;

$$g_1 = 1530 \text{ N};$$

$$g_2 = 170 \text{ N/m};$$

$$g_3 = 400 \text{ N/m}^{1,5}.$$

Value $\left(\frac{LT}{B^2} \right)^3$ in Formula (10.4.3-2) shall not be taken as less than 5 and shall not be taken as more than 20.

10.4.4 Formula (10.4.3-2) may be used when the conditions given in Table 10.4.4 are fulfilled.

Table 10.4.4

Applicability conditions of Formula (10.4.3-2)

Parameter	Minimum value	Maximum value
α , in deg.	15	55
φ_1 , in deg.	25	90
φ_2 , in deg.	10	90
L , m	65,0	250,0
B , m	11,0	40,0
T , m	4,0	15,0
L_{BOW}/L	0,15	0,40
L_{PAR}/L	0,25	0,75
D_p/T^1	0,45	0,75
$A_{wf}/(L \cdot B)$	0,09	0,27

¹When calculating the parameter D_p/T , T shall be measured at the largest draught amidships.

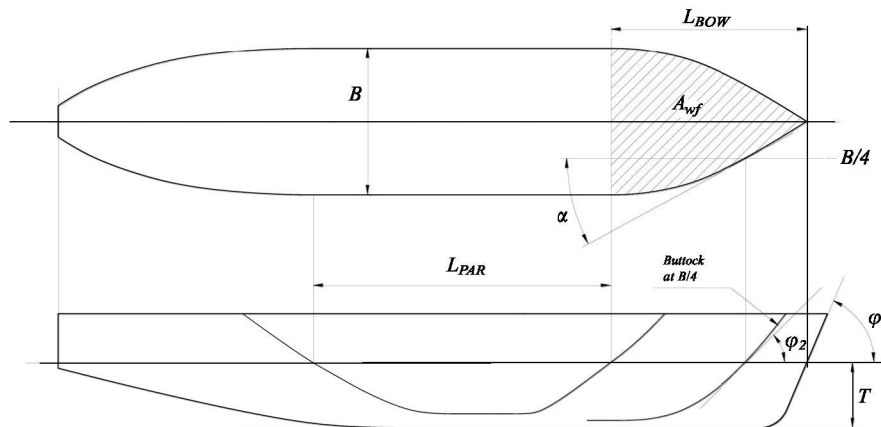


Fig. 10.4.1.1 Determination of the geometric quantities of the hull

The use of K_e or R_{CH} values based on more exact calculations or values based on model tests may be approved. Such an approval will be given on the understanding that it can be revoked if experience of the ship's performance in practice motivates this. The design requirement for ice classes is a minimum speed of 5 knots in the following brash ice channels:

$H_M = 0,6$ m for ice class **IC**;

$H_M = 0,8$ m for ice class **IB**;

$H_M = 1,0$ m for ice class **IA**;

$H_M = 1,0$ m and a 0,1 m thick consolidated layer of ice for ice class **IA Super**.

10.5 HULL STRUCTURAL DESIGN

10.5.1 General.

The method for determining the hull scantlings is based on certain assumptions concerning the nature of the ice load on the structure. These assumptions are from full scale observations made in the northern Baltic.

It has thus been observed that the local ice pressure on small areas can reach rather high values. This pressure may be well in excess of the normal uniaxial crushing strength of sea ice. The explanation is that the stress field in fact is multiaxial.

Further, it has been observed that the ice pressure on a frame can be higher than on the shell plating at midspacing between frames. The explanation for this is the different flexural stiffness of frames and shell plating. The load distribution is assumed to be as shown in Fig. 10.5.1-1.

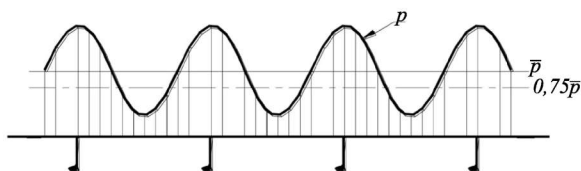


Fig. 10.5.1-1 Ice load distribution on a ship's side

The formulae and values given in this section may be substituted by direct analysis if they are deemed by the administration or the classification society to be invalid or inapplicable for a given structural arrangement or detail. Otherwise, direct analysis is not to be utilized as an alternative to the analytical procedures prescribed by explicit requirements in 10.5.3 — 10.5.5.

Direct analyses shall be carried out using the load patch defined in 10.5.2 (p , h and l_a). The pressure to be used is $1,8p$ where p is determined according to 10.5.2.2. The load patch shall be applied at locations where the capacity of the structure under the combined effects of bending and shear are minimized. In particular, the structure is to be checked with load centred at the UIWL,

$0,5h_0$ below the LIWL, and positioned several vertical locations in between. Several horizontal locations shall also be checked, especially the locations centred at the mid-span or -spacing. Further, if the load length l_a cannot be determined directly from the arrangement of the structure, several values of l_a shall be checked using corresponding values for c_a .

The acceptance criterion for designs is that the combined stresses from bending and shear, using the von Mises yield criterion, are lower than the yield point σ_y . When the direct calculation is using beam theory, the allowable shear stress is not to be larger than $0,9\tau_y$, where $\tau_y = \sigma_y/\sqrt{3}$.

If scantlings derived from these regulations are less than those required by the Register for a not ice strengthened ship, the latter shall be used.

Notes: 1. The frame spacings and spans defined in the following text are normally (in compliance with the requirements of the Register normative documents for the ship in question) assumed to be measured along the plate and perpendicular to the axis of the stiffener for plates, along the flange for members with a flange, and along the free edge for flat bar stiffeners. For curved members the span (or spacing) is defined as the chord length between span (or spacing) points. The span points are defined by the intersection between the flange or upper edge of the member and the supporting structural element (stringer, web frame, deck or bulkhead). Fig. 10.5.1-2 illustrates the determination of span and spacing for curved members.

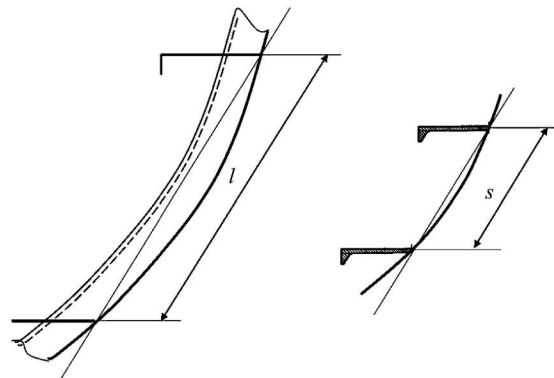


Fig. 10.5.1-2 Definition of the frame span (left) and frame spacing (right) for curved members

2. The effective breadth of the attached plate to be used for calculating the combined section modulus of the stiffener, stringer and web frame and attached plate shall be taken as the applicable requirements of the Register normative documents require. The effective breadth shall in no case be more than what is stated in the applicable requirements of the Register normative documents for the ship in question.

3. The requirements for the section modulus and shear area of the frames, stringers and web frames in 10.5.4 — 10.5.6, are with respect to the effective member cross section. For such cases where the member is not normal to the plating, the section properties shall be calculated in accordance with the applicable requirements of the Register normative documents for the ship in question.

10.5.1.1 Hull regions.

The ship's hull is divided into regions as follows (refer also to Fig. 10.5.1.1).

Bow region: from the stem to a line parallel to and 0,04L aft of the forward borderline of the part of the hull where the waterlines run parallel to the centerline. For ice classes **IA Super** and **IA** the overlap over the borderline need not exceed 6 m, for ice classes **IB** and **IC** this overlap need not exceed 5 m.

Midbody region: from the aft boundary of the bow region to a line parallel to and 0, For ice classes **IA Super** and **IA** the overlap over the borderline need not exceed 6 m, for ice classes **IB** and **IC** this overlap need not exceed 5 m.

Stern region: From the aft boundary of the midbody region to the stern.

L shall be taken as the ship's design length in compliance with the requirements of the Register normative documents.

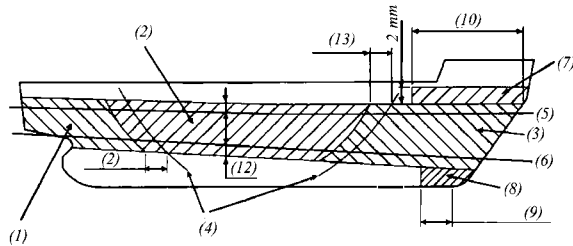


Fig. 10.5.1.1 Ice strengthened regions of the hull:
1 — ice belt, stern region; 2 — ice belt, midbody region;
3 — ice belt, bow region; 4 — border of the part
of the side where waterlines are parallel to the centerline;
5 — UIWL; 6 — LIWL;
7 — upper bow ice belt; 8 — fore foot;
9 — 5 frame spacings; 10 — 0,2L;
11 — refer to 10.5.1; 12 — refer to 10.5.3.1;
13 — refer to 10.5.1

10.5.2 Ice load.

10.5.2.1 Height of the ice load area.

An ice-strengthened ship is assumed to operate in open sea conditions corresponding to a level ice thickness not exceeding h_0 . The design ice load height h of the area actually under ice pressure at any particular point of time is, however, assumed to be only a fraction of the ice thickness. The values for h_0 and h are given in the following Table:

Ice class	h_0 , in m	h , in m
IA Super	1,0	0,35
IA	0,8	0,30
IB	0,6	0,25
IC	0,4	0,22

10.5.2.2 Ice pressure.

The design ice pressure is determined by the following formula:

$$p = c_d c_p c_a p_0, \text{ in MPa,} \quad (10.5.2.2)$$

where c_d = is a factor which takes account of the influence of the size and engine output of the ship. The factor c_d is taken as maximum 1,0 and is determined by the following formula:

$$c_d = \frac{ak + b}{1000}$$

$$\text{where } k = \frac{\sqrt{\Delta P}}{1000};$$

a and b are given in the following Table:

	Region			
	bow		midbody and stern	
	$k \leq 12$	$k > 12$	$k \leq 12$	$k > 12$
a	30	6	8	2
b	230	518	214	286

Δ = displacement of the ship at maximum ice class draught, in t (refer to. 10.3.1);

P = actual continuous engine output of the ship, in kW (refer to 10.4.2);

c_p = factor which takes account of the probability that the design ice pressure occurs in a certain region of the hull for the ice class in question.

The value of c_p is given in the following Table:

Ice class	Region		
	bow	midbody	stern
IA Super	1,0	1,0	0,75
IA	1,0	0,85	0,65
IB	1,0	0,70	0,45
IC	1,0	0,50	0,25

c_a = factor which takes account of the probability that the full length of the area under consideration will be under pressure at the same time. It is calculated by the following formula:

$$c_a = \sqrt{l_0/l_a}, \quad 0,35 \leq c_a \leq 1,0$$

where $l_0 = 0,6$ m;

l_a shall be taken as follows:

Structure	Type of framing	l_a , in m
Shell	transverse	Frame spacing
	longitudinal	1,7 frame spacing
Frames	transverse	Frame spacing
	longitudinal	Span of frame
Ice stringer		Span of stringer
Web frame		2 web frame spacing

p_0 = nominal ice pressure; the value 5,6 MPa shall be used.

10.5.3 Shell plating.

10.5.3.1 Vertical extension of ice strengthening for plating (ice belt).

The vertical extension of the ice belt shall be as follows (refer to Fig. 10.5.1.1):

Ice class	Hull region	Above UIWL	Below LIWL
IA Super	bow	0,60 m	1,20 m
	midbody		
	stern		1,0 m
IA	bow	0,50 m	0,90 m
	midbody		0,75 m
	stern		
IB и IC	bow	0,40 m	0,70 m
	midbody		0,60 m
	stern		

In addition, the following areas shall be strengthened.

Fore foot. For ice class **IA Super**, the shell plating below the ice belt from the stern to a position five main frame spaces abaft the point where the bow profile departs from the keel line shall have at least the thickness required in the ice belt in the midbody region.

Upper bow ice belt. For ice classes **IA Super** and **IA** on ships with an open water service speed equal to or exceeding 18 knots, the shell plate from the upper limit of the ice belt to 2 m above it and from the stern to a position at least 0,2L abaft the forward perpendicular, shall have at least the thickness required in the ice belt in the midbody region.

A similar strengthening of the bow region is advisable also for a ship with a lower service speed, when it is, e.g. on the basis of the model tests, evident that the ship will have a high bow wave.

Side scuttles shall not be situated in the ice belt. If the weather deck in any part of the ship is situated below the upper limit of the ice belt (e.g. in way of the well of a raised quarter decker), the bulwark shall be given at least the same strength as is required for the shell in the ice belt. The strength of the construction of the freeing ports shall meet the same requirements.

10.5.3.2 Plate thickness in the ice belt.

For transverse framing the thickness of the shell plating shall be determined by the following formula:

$$t = 667s \sqrt{\frac{f_1 p_{PL}}{\sigma_y}} + t_c, \text{ in mm.} \quad (10.5.3.2-1)$$

For longitudinal framing the thickness of the shell plating shall be determined by the following formula:

$$t = 667s \sqrt{\frac{p}{f_2 \sigma_y}} + t_c, \text{ in mm,} \quad (10.5.3.2-2)$$

where s = frame spacing, in m;

$p_{PL} = 0,75p$, in MPa;

p as given in 10.5.2.2;

$$f_1 = 1,3 - \frac{4,2}{(h/s + 1,8)^2}; \text{ maximum } 1,0;$$

$$f_2 = 0,6 + \frac{0,4}{(h/s)} \text{ when } h/s \leq 1;$$

$$f_2 = 1,4 - 0,4(h/s) \text{ when } 1 \leq h/s < 1,8$$

where h as given in 10.5.2.1;

σ_y = yield stress of the material, in MPa, for which the following values shall be used:

$\sigma_y = 235$ MPa for normal-strength hull structural steel;

$\sigma_y = 315$ MPa or higher for high-strength hull structural steel.

If steels with different yield stress are used, the actual values may be substituted for the above ones upon agreement with the Register.

t_c = increment for abrasion and corrosion, in mm; normally t_c shall be 2 mm; if a special surface coating, by experience shown capable to withstand the abrasion of ice, is applied and maintained, lower values may be agreed with the Register.

10.5.4 Frames.

10.5.4.1 Vertical extension of ice strengthening for framing.

The vertical extension of the ice strengthening of the framing shall be at least as follows:

Ice class	Hull region	Above UIWL	Below LIWL
IA Super	bow	1,2 m	Down to double bottom or below top of the floors
	midbody		2,0 m
	stern		1,6 m
IA, IB и IC	bow	1,0 m	1,6 m
	midbody		1,3 m
	stern		1,0 m

Where an upper bow ice belt is required (refer to 10.5.3.1), the ice-strengthened part of the framing shall be extended at least to the top of this ice belt.

Where the ice-strengthening would go beyond a deck or a tanktop (or tank bottom) by no more than 250 mm, it can be terminated at that deck or tanktop (or tank bottom).

10.5.4.2 Transverse frames.

10.5.4.2.1 Section modulus and shear area.

The section modulus of a main or intermediate transverse frame shall be determined by the following formula:

$$Z = \frac{pshl}{m_t \sigma_y}, \text{ in cm}^3. \quad (10.5.4.2.1-1)$$

The effective shear area is calculated from the formula

$$A = \frac{\sqrt{3} f_3 phs}{2 \sigma_y} 10^4, \text{ in cm}^2, \quad (10.5.4.2.1-2)$$

where p = ice pressure as given in 10.5.2.2, in MPa;

s = frame spacing, in m;

h = height of load area as given in 10.5.2.1, in m;

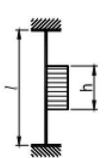
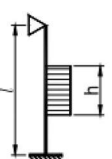
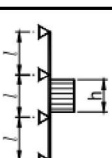
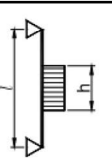
l = span of the frame, in m;

$$m_t = \frac{7m_0}{7-5h/l};$$

f_3 = factor which takes into account the maximum shear force versus the load location and the shear stress distribution, $f_3 = 1,2$;

σ_y = yield stress as in 10.5.3.2, in MPa;

m_0 = takes the boundary conditions into account. The values are given in the following Table:

Boundary condition	m_0	Example
	7	Frames in a bulk carrier with top wing tanks
	6	Frames extending from the tank top to a single deck
	5,7	Continuous frames between several decks or stringers
	5	Frames extending between two decks only

The boundary conditions are those for the main and intermediate frames. Load is applied at mid span.

Where less than 15 per cent of the span l of the frame is situated within the ice-strengthening zone, ordinary frame scantlings may be used.

10.5.4.2.2 Upper end of transverse framing.

The upper end of the strengthened part of a main frame and of an intermediate ice frame shall be attached to a deck, tanktop (or tank bottom) or an ice stringer (refer to 10.5.5).

Where a frame terminates above a deck or a stringer which is situated at or above the upper limit of the ice belt, the part above the deck or stringer may have the scantlings required by the requirements of the appropriate normative documents of the Register for an

non ice-strengthened ship and the upper end of an intermediate frame may be connected to the adjacent frames by a horizontal member having the same scantlings as the main frame.

10.5.4.2.3 Lower end of transverse framing.

The lower end of the strengthened part of a main frame and of an intermediate ice frame shall be attached to a deck, tanktop (or tank bottom) or an ice stringer (refer to 10.5.5).

Where an intermediate frame terminates below a deck, tanktop (or tank bottom) or ice stringer which is situated at or below the lower limit of the ice belt, the lower end may be connected to the adjacent main frames by a horizontal member of the same scantlings as the main frames. Note that the main frames below the lower edge of ice belt must be ice strengthened, refer to 10.5.4.1.

10.5.4.3 Longitudinal frames.

The requirements of the present Section are intended for longitudinal frames with all end conditions.

10.5.4.3.1 Frames with and without brackets.

The section modulus of a longitudinal frame shall be not less than determined by the following formula:

$$Z = \frac{f_4 phl^2}{m \sigma_y} 10^6, \text{ in cm}^3, \quad (10.5.4.3.1-1)$$

and effective shear area of a longitudinal frame shall be not less than determined by the following formula:

$$A = \frac{\sqrt{3} f_4 f_5 phl}{2 \sigma_y} 10^4, \text{ in cm}^2. \quad (10.5.4.3.1-2)$$

In calculating the actual shear area of the frames, the shear area of the brackets shall not be taken into account.

In the formulae given above:

f_4 = factor which takes account of the load distribution to adjacent frames: $f_4 = (1 - 0,2h/s)$;

f_5 = factor which takes into account the maximum shear force versus load location and the shear stress distribution; $f_5 = 2,16$;

p = ice pressure as given in 10.5.2.2, in MPa;

h = height of load area as given in 10.5.2.1, in m;

s = frame spacing, in m;

l = total span of frame, in m;

m = boundary condition factor; $m = 13,3$ for a continuous beam; where the boundary conditions deviate significantly from those of a continuous beam, e.g. in an end field, a smaller boundary factor may be required. For frames without brackets a value $m = 11,0$ shall be used;

σ_y = yield stress as in 10.5.3.2, in MPa.

10.5.4.4 General on framing.

10.5.4.4.1 The attachment of frames to supporting structures.

Within the ice-strengthened area all frames shall be effectively attached to all the supporting structures. A longitudinal frame shall be attached to all the supporting web frames and bulkheads by brackets. When a transversal frame terminates at a stringer or deck, a

bracket or similar construction is to be fitted. When a frame is running through the supporting structure, both sides of the web plate of the frame are to be connected to the structure (by direct welding, collar plate or lug). When a bracket is installed, it has to have at least the same thickness as the web plate of the frame and the edge has to be appropriately stiffened against buckling.

10.5.4.4.2 Support of frames against tripping for ice class IA Super, for ice class IA in the bow and midbody regions and for ice classes IB and 1C in the bow region of the ice-strengthened area.

All the frames shall be attached to the shell by double continuous weld. No scalloping is allowed.

The web thickness of the frames shall be at least the maximum of the following:

$$\frac{h_w \sqrt{\sigma_y}}{C}$$

where h_w = web height;
 C = 805 for profiles; and
 C = 282 for flat bars;

2,5 per cent of the frame spacing for transverse frames;

half of the net thickness of the shell plating, $t - t_c$. For the purpose of calculating the web thickness of frames, the required thickness of the shell plating is to be calculated according to 10.5.3.2 using the yield strength σ_y of the frames;

9 mm.

Where there is a deck, tanktop (or tank bottom) or bulkhead in lieu of a frame, the plate thickness of this shall be as above, to a depth corresponding to the height of the adjacent frames.

Frames that are not normal to the plating or the profile is unsymmetrical, and the span exceeds 4,0 m, shall be supported against tripping by brackets, intercostals, stringers or similar at a distance not exceeding 1,3 m. If the span is less than 4,0 m, the supports against tripping are required for unsymmetrical profiles and stiffeners the web of which is not normal to plating in the following regions:

- all hull regions for ice class IA Super;
- bow and midbody regions for ice class IA;
- bow region for ice classes IB and 1C.

10.5.5 Ice stringers.

10.5.5.1 Stringers within the ice belt.

The section modulus of a stringer situated within the ice belt (refer to 10.5.3.1), shall be taken not less than determined by the formula

$$Z = \frac{f_5 f_7 p h l^2}{m \sigma_y} 10^6, \text{ in cm}^3. \quad (10.5.5.1-1)$$

The effective shear area shall be taken not less than determined by the formula

$$A = \frac{\sqrt{3} f_9 f_7 f_3 p h l}{2 \sigma_y} 10^4, \text{ in cm}^2, \quad (10.5.5.1-2)$$

where p = ice pressure as given in 10.5.2.2, in MPa;

h = height of load area as given in 10.5.2.1, in m.

The product $p h$ shall not be taken as less than 0,15;

l = span of the stringer, in m;

m = boundary condition factor as defined in 10.5.4.3;

f_5 = factor which takes account of the distribution of load to the transverse frames; to be taken as 0,9;

f_7 = safety factor of stringers; to be taken as 1,8;

f_8 = a factor that takes into account the maximum shear force versus load location and the shear stress distribution, ;

σ_y = yield stress as in 10.5.3.2, in MPa.

10.5.5.2 Stringers outside the ice belt.

The section modulus of a stringer situated outside the ice belt but supporting ice-strengthened frames shall be taken not less than determined by the formula

$$Z = \frac{f_9 f_{10} p h l^2}{m \sigma_y} (1 - h_s/l_s) 10^6, \text{ in cm}^3. \quad (10.5.5.2-1)$$

The effective shear area shall be taken not less than determined by the formula

$$A = \frac{\sqrt{3} f_9 f_{10} f_{11} p h l}{2 \sigma_y} (1 - h_s/l_s) 10^4, \text{ in cm}^2 \quad (10.5.5.2-2)$$

where p = ice pressure as given in 10.5.2.2, in MPa;

h = height of load area as given in 10.5.2.1, in m.

The product $p h$ shall not be taken as less than 0,15;

l = span of stringer, in m;

m = boundary condition factor as defined in 10.5.4.3;

l_s = distance to the adjacent ice stringer, in m;

h_s = distance to the ice belt, in m;

f_9 = factor which takes account of the distribution of load to the transverse frames; to be taken as 0,80;

f_{10} = safety factor of stringers; to be taken as 1,8;

f_{11} = factor that takes into account the maximum shear force versus load location and the shear stress distribution, $f_{11} = 1,2$;

σ_y = yield stress of material as in 10.5.3.2, in MPa.

10.5.5.3 Deck strips.

Narrow deck strips abreast of hatches and serving as ice stringers shall comply with the section modulus and shear area requirements in 10.5.5.1 and 10.5.5.2 respectively. In the case of very long hatches, upon agreement with the Register, the product $p h$ may be taken as less than 0,15 but in no case as less than 0,10.

Regard shall be paid to the deflection of the ship's sides due to ice pressure in way of very long (more than $B/2$) hatch openings when designing weather deck hatch covers and their fittings.

10.5.6 Web frames.

10.5.6.1 Ice load.

The ice load transferred to a web frame from an ice stringer or from longitudinal framing shall be determined by the following formula:

$$F = f_{12} p h S, \text{ in MN} \quad (10.5.6.1)$$

where p = ice pressure as given in 10.5.2.2, in MPa, in calculating c_a , however, l_a shall be taken 2S.

h = height of load area as given in 10.5.2.1, in m.

The product ph shall not be taken as less than 0,15;
 S = distance between web frames, in m;
 f_{12} = safety factor of web frames; to be taken as 1,8.
 In case the supported stringer is outside the ice belt, the force F shall be multiplied by $(1 - h_s/l_s)$ where h_s and l_s shall be taken as defined in 10.5.5.2.

10.5.6.2 Section modulus and shear area.

The section modulus and shear area of web frames shall be calculated by the following formulae.

The effective shear area

$$A = \frac{\sqrt{3}\alpha f_{13} Q 10^4}{2\sigma_y}, \text{ in cm}^2, \quad (10.5.6.2-1)$$

where Q = maximum calculated shear force under the ice load F as given in 10.5.6.1;

f_{13} = factor that takes into account the shear force distribution,

$f_{13} = 1,1$;

α = as given in the Table below;

σ_y = yield stress of material as in 10.5.3.2, in MPa.

Section modulus

$$Z = \frac{M}{\sigma_y} \sqrt{\frac{1}{1 - (\gamma A/A_a)^2}} 10^6, \text{ in cm}^3, \quad (10.5.6.2-2)$$

where M = maximum calculated bending moment under the ice load F .

$M = 0,193Fl$;

γ = given in the Table below;

A = required shear area;

A_a = actual cross sectional area of the web frame, $A_a = A_f + A_w$.

Factors α and γ can be obtained from the Table below:

A_f/A_w	0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
α	1,5	1,23	1,16	1,11	1,09	1,07	1,06	1,05	1,05	1,04	1,04
γ	0	0,44	0,62	0,71	0,76	0,80	0,83	0,85	0,87	0,88	0,89

where A_f = actual cross section area of free flange;

A_w = actual effective cross section area of web plate.

10.5.7 Stem.

10.5.7.1 The stem shall be made of rolled, cast or forged steel or of shaped steel plates as shown in Fig. 10.5.7.1.

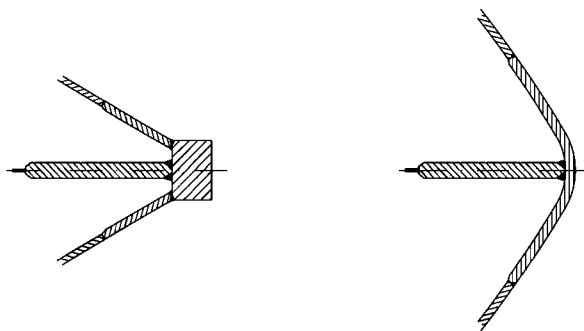


Fig. 10.5.7.1 Examples of suitable stems

The plate thickness of a shaped plate stem given in Fig 10.5.7.1, and in the case of a blunt bow, any part of the shell where $\alpha \geq 30^\circ$ and $\psi \geq 75^\circ$ (refer to 10.4.1.1 for angle definitions), shall be not less than determined in 10.5.3.2, assuming that

s = spacing of elements supporting the plate, in m;

$p_{PL} = p$, in MPa (refer to 10.5.3.2);

l_a = spacing of vertical supporting elements, in m.

The stem and the part of a blunt bow defined above shall be supported by floors or brackets spaced not more than 0,6 m apart and having a thickness of at least half the plate thickness. The reinforcement of the stem shall extend from the keel to a point 0,75 m above UIWL or, in case an upper bow ice belt is required (refer to 10.5.3.1), to the upper limit of this.

10.5.8 Stern.

The introduction of new propulsion arrangements with azimuthing thrusters or "podded" propellers, which provide an improved manoeuvrability, will result in increased ice loading of the Stern region and the stern area. This fact should be considered in the design of the aft/stern structure.

In order to avoid very high loads on propeller blade tips, the minimum distance between propeller(s) and hull (including stern frame) should not be less than h_0 (refer to 10.5.2.1).

On twin and triple screw ships the ice strengthening of the shell and framing shall be extended to the double bottom for 1,5 m forward and aft of the side propellers.

Shafting and stern tubes of side propellers shall normally be enclosed within plated bossings. If detached struts are used, their design, strength and attachments to the hull shall be approved by the Register.

10.6 RUDDER AND STEERING ARRANGEMENTS

10.6.1 The scantlings of rudder post, rudder stock, pintles, steering engine etc. as well as the capability of the steering engine shall be determined in compliance with the applicable requirements of the Register. The maximum service speed of the ship to be used in these calculations shall, however, not be taken as less than stated below:

for ice class **IASuper** — 20 knots;

for ice class **IA** — 18 knots;

for ice class **IB** — 16 knots;

for ice class **IC** — 14 knots.

If the actual maximum service speed of the ship is higher, that speed shall be used.

The local scantlings of rudders shall be determined assuming that the whole rudder belongs to the ice belt. Further, the rudder plating and frames shall be designed using the ice pressure p for the plating and frames in the midbody region.

For ice classes **IA** and **IA Super** the rudder (rudder stock and the upper part of the rudder) shall be protected from direct contact with intact ice by an ice knife that extends below the LIWL, if practicable (or equivalent means). When using flap-type rudders, the design of the

ice knife shall ensure necessary strength of the rudder.

For ice classes **IA** and **IA Super** due regard shall be paid to the large loads that arise when the rudder is forced out of the midship position while going astern in ice or into ice ridges. Suitable arrangement such as rudder stoppers shall be installed to absorb these loads.

Relief valves for hydraulic pressure in rudder turning mechanism(s) shall be installed. The components of the steering gear (e.g. rudder stock, rudder coupling, rudder horn etc.) shall be dimensioned to withstand loads causing yield stresses in the rudder stock.

10.7 PROPULSION MACHINERY

10.7.1 Scope.

These regulations apply to propulsion machinery covering open- and ducted-type propellers with controllable pitch or fixed pitch design for the ice classes **IA Super**, **IA**, **IB** and **IC**.

The given loads are the expected ice loads for the whole ship's service life under normal operational conditions, including loads resulting from the changing rotational direction of FP propellers. However, these loads do not cover off-design operational conditions, for example when a stopped propeller is dragged through ice.

The regulations also apply to azimuthing and fixed thrusters for main propulsion, considering loads resulting from propeller/ice interaction. However, the load models of the regulations do not include propeller/ice interaction loads when ice enters the propeller of a turned azimuthing thruster from the side (radially) or load cases when ice block hits on the propeller hub of a pulling propeller.

Ice loads resulting from ice impacts on the body of thrusters have to be estimated, but ice load formulae are not available.

10.7.2 Definitions.

D — propeller diameter, in m.

R — propeller radius, in m.

c — chord length of blade section, in m.

$c_{0,7}$ — chord length of blade section at propeller radius $r = 0,7R$, in m.

d — external diameter of propeller hub (at propeller plane), in m.

D_{limit} — limit value for propeller diameter, in m.

F_b — maximum backward blade force for the ship's service life, in kN.

F_{ex} — ultimate blade load resulting from blade loss through plastic bending, in kN.

F_f — maximum forward blade force for the ship's service life, in kN.

F_{ice} — ice load, in kN.

$(F_{ice})_{max}$ — maximum ice load for the ship's service life, in kN.

h_0 — depth of the propeller centreline from LIWL, in m.

H_{ice} — thickness of maximum design ice block entering to propeller, in m.

I — equivalent mass moment of inertia of all parts on engine side of component under consideration, in kgm^2 .

I_t — equivalent mass moment of inertia of the whole propulsion system, in kgm^2 .

k — shape parameter for Weibull distribution.

m — slope for SN curve in log/log scale.

M_{BL} — blade bending moment, in kNm.

n — propeller rotational speed, in rev/s.

n_n — nominal propeller rotational speed at MCR in free running condition, in rev/s.

N_{class} — reference number of impacts per propeller rotational speed per ice class.

N_{ice} — total number of ice loads on propeller blade for the ship's service life.

N_R — reference number of load for equivalent fatigue stress (108 cycles).

N_Q — number of propeller revolutions during a milling sequence.

$P_{0,7}$ — propeller pitch at radius $r = 0,7R$, in m.

$P_{0,7n}$ — propeller pitch at radius $r = 0,7R$ at MCR in free running condition, in m.

$P_{0,7b}$ — propeller pitch at radius $r = 0,7R$ at MCR in bollard condition, in m.

Q — torque, in kNm.

Q_{emax} — maximum engine torque, in kNm.

Q_{max} — maximum torque on the propeller resulting from propeller/ice interaction, in kNm.

Q_{motor} — electric motor peak torque, in kNm.

Q_n — nominal torque at MCR in free running condition, in kNm.

Q_r — maximum response torque along the propeller shaft line, in kNm.

Q_{smax} — maximum spindle torque of the blade for the ship's service life, in kNm.

r — propeller radius, in m.

T — propeller thrust, in kN.

T_b — maximum backward propeller ice thrust for the ship's service life, in kN.

T_f — maximum forward propeller ice thrust for the ship's service life, in kN.

T_n — propeller thrust at MCR in free running condition, in kN.

T_r — maximum response thrust along the shaft line, in kN.

t — maximum blade section thickness, in m.

Z — number of propeller blades.

α_t — duration of propeller blade/ice interaction expressed in rotation angle, in deg.

γ_e — reduction factor for fatigue; scatter and test specimen size effect.

γ_v — reduction factor for fatigue; variable amplitude loading effect.

γ_m — reduction factor for fatigue; mean stress effect.

p — reduction factor for fatigue correlating the maximum stress amplitude to the equivalent fatigue stress for 10^8 stress cycles.

$\sigma_{0,2}$ — proof yield strength (at 0,2 per cent offset) of blade material, in MPa.

σ_{exp} — mean fatigue strength of blade material at 108 cycles to failure in sea water, in MPa.

σ_{fat} — equivalent fatigue ice load stress amplitude for 108 stress cycles, in MPa.

σ_R — characteristic fatigue strength for blade material, in MPa.

σ_u — ultimate tensile strength of blade material, in MPa.

$\sigma_{ref} = \sigma_{ref} = 0,6\sigma_{0,2} + 0,4\sigma_u$, in MPa.

$\sigma_{ref2} = \sigma_{ref2} = 0,7\sigma_u$ or

$\sigma_{ref2} = 0,6\sigma_{0,2} + 0,4\sigma_u$, whichever is less, in MPa.

σ_{st} — maximum stress resulting from F_b or F_f , in MPa.

$(\sigma_{ice})_{b_{max}}$ — principal stress caused by the maximum backward propeller ice load, in MPa.

$(\sigma_{ice})_{f_{max}}$ — principal stress caused by the maximum forward propeller ice load, in MPa.

$(\sigma_{ice})_{max}$ — maximum ice load stress amplitude, in MPa.

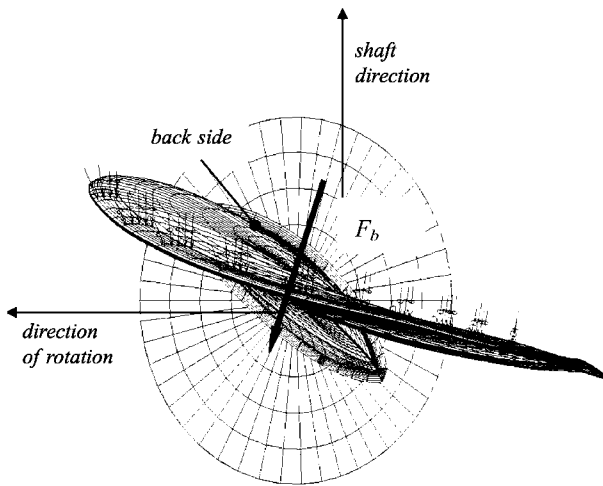
10.7.3 Design ice conditions.

In estimating the ice loads of the propeller for ice classes, different types of operation as given in Table 10.7.3-1 were taken into account. The maximum design ice block entering the propeller is a rectangular ice block with the dimensions $H_{ice} \cdot 2H_{ice} \cdot 3H_{ice}$. The thickness of the ice block H_{ice} is given in Table 10.7.3-2.

Table 10.7.2

Definition of loads

	Definition	Use of the load in design process
F_b	The maximum lifetime backward force on a propeller blade resulting from propeller/ice interaction, including hydrodynamic loads on that blade. The direction of the force is perpendicular to 0,7R chord line (refer to Fig. 10.7.2)	Design force for strength calculation of the propeller blade.
F_f	The maximum lifetime forward force on a propeller blade resulting from propeller/ice interaction, including hydrodynamic loads on that blade. The direction of the force is perpendicular to 0,7R chord line.	Design force for calculation of strength of the propeller blade.
Q_{max}	The maximum lifetime spindle torque on a propeller blade resulting from propeller/ice interaction, including hydrodynamic loads on that blade.	In designing the propeller strength, the spindle torque is automatically taken into account because the propeller load is acting on the blade as distributed pressure on the leading edge or tip area.
T_b	The maximum lifetime thrust on propeller (all blades) resulting from propeller/ice interaction. The direction of the thrust is the propeller shaft direction and the force is opposite to the hydrodynamic thrust.	Is used for estimation of the response thrust T_r . T_b can be used as an estimate of excitation for axial vibration calculations.
T_f	The maximum lifetime thrust on propeller (all blades) resulting from propeller/ice interaction. The direction of the thrust is the propeller shaft direction acting in the direction of hydrodynamic thrust.	Is used for estimation of the response thrust T_r . T_f can be used as an estimate of excitation for axial vibration calculations.
Q_{max}	The maximum ice-induced torque resulting from propeller/ice interaction on one propeller blade, including hydrodynamic loads on that blade.	Is used for estimation of the response torque along the propulsion shaft line and as excitation for torsional vibration calculations.
F_{ex}	Ultimate blade load resulting from blade loss through plastic bending. The force is acting on 0,8R. Spindle arm shall be taken as 2/3 of the distance between the axis of blade rotation and leading/trailing edge (whichever is the greater) at the 0,8R radius.	Blade failure load is used to dimension the blade bolts, pitch control mechanism, propeller shaft, propeller shaft bearing and trust bearing. The objective is to guarantee that total propeller blade failure should not cause damage to other components.
Q_r	Maximum response torque along the propeller shaft line, taking into account the dynamic behavior of the shaft line for ice excitation (torsional vibration) and hydrodynamic mean torque on propeller.	Design torque for propeller shaft line components.
T_r	Maximum response thrust along shaft line, taking into account the dynamic behavior of the shaft line for ice excitation (axial vibration) and hydrodynamic mean thrust on propeller.	Design thrust for propeller shaft line components.

Fig.10.7.2 Direction of force F_b .

Ice contact pressure at leading edge is shown with small arrows

Table 10.7.3-1

Operation characteristics	
Ice class	Operation of the ship
IA Super	Operation in ice channels and in level ice The ship may proceed by ramming
IA, IB, IC	Operation in ice channels

Table 10.7.3-2

Thickness of the design maximum ice block entering the propeller

Ice class	IA Super	IA	IB	IC
H_{ice}	1,75 m	1,5 m	1,2 m	1,0 m

10.7.4 Materials.

10.7.4.1 Materials exposed to sea water.

Materials of components exposed to sea water, such as propeller blades, propeller hubs, and thruster body, shall have an elongation of not less than 15 per cent on a test specimen, the gauge length of which is five times the diameter.

A Charpy V-notch impact test shall be carried out for materials other than bronze and austenitic steel. An average impact energy value of 20 J taken from three tests shall be obtained at $-10\text{ }^{\circ}\text{C}$.

10.7.4.2 Materials exposed to sea water temperature.

Materials exposed to sea water temperature shall be of steel or other ductile material. An average impact energy value of 20 J taken from three tests shall be obtained at $-10\text{ }^{\circ}\text{C}$.

This requirement applies to blade bolts, CP mechanisms, shaft bolts, strut-pod connecting bolts etc. This does not apply to surface hardened components, such as bearings and gear teeth.

10.7.5 Design loads.

The loads specified in the Section are intended for

component strength calculations only and are total loads including ice-induced loads and hydrodynamic loads during propeller/ice interaction.

The values of the parameters in the formulae in this section shall be given in the units shown in 10.7.2.

If the propeller is not fully submerged when the ship is in ballast condition, the propulsion system shall be designed according to ice class **IA** for ice classes **IB** and **IC**.

10.7.5.1 Design loads on propeller blades.

F_b is the maximum force experienced during the lifetime of the ship that bends a propeller blade backwards when the propeller mills an ice block while rotating ahead.

F_f is the maximum force experienced during the lifetime of the ship that bends a propeller blade forwards when the propeller mills an ice block while rotating ahead.

F_b and F_f originate from different propeller/ice interaction phenomena, not acting simultaneously. Hence they shall be applied to one blade separately.

10.7.5.1.1 Force F_b for open propellers.

$$F_b = 27[nD]^{0,7} \left[\frac{EAR}{Z} \right]^{0,3} D^2, \text{ in kN, when } D \leq D_{limit}; \quad (10.7.5.1.1-1)$$

$$F_b = 27[nD]^{0,7} \left[\frac{EAR}{Z} \right]^{0,3} DH_{ice}^{1,4}, \text{ in kN, when } D \leq D_{limit} \quad (10.7.5.1.1-2)$$

where $D_{limit} = 0,85H_{ice}^{1,4}$, in m;
 $n = n_n$ for a CP propeller;
 $n = 0,85n_n$ for a FP propeller.

10.7.5.1.2 Force F_f for open propellers.

$$F_f = 250 \left[\frac{EAR}{Z} \right] D^2, \text{ in kN, when } D \leq D_{limit}; \quad (10.7.5.1.2-1)$$

$$F_f = 500 \left[\frac{EAR}{Z} \right] D \left(\frac{1}{1 - \frac{d}{D}} \right) H_{ice}, \text{ in kN, when } D \leq D_{limit} \quad (10.7.5.1.2-2)$$

where $D_{limit} = \left(\frac{2}{1 - \frac{d}{D}} \right) H_{ice}$, in m.

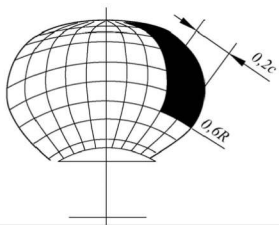
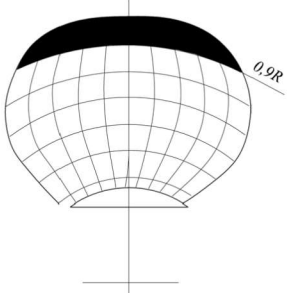
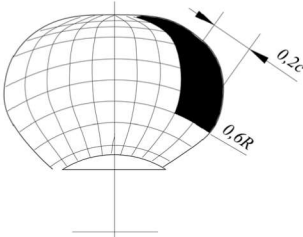
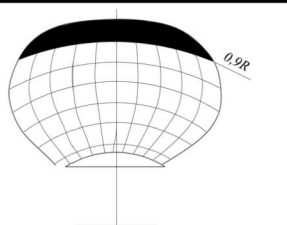
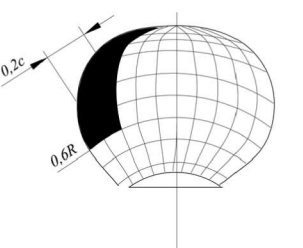
10.7.5.1.3 Loaded area on the blade for open propellers.

Load cases 1 — 4 have to be covered, as given in Table 10.7.5.1.3, for CP and FP propellers.

In order to obtain blade ice loads for a reversing propeller, load case 5 also has to be covered for FP propellers.

Table 10.7.5.1.3

Load cases for open propellers

	Force	Loaded area	Right-handed propeller blade seen from behind
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 2	50 per cent of F_b	Uniform pressure applied on the back of the blade (suction side) on the propeller tip area outside $0,9R$ radius	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length.	
Load case 4	50 per cent of F_f	Uniform pressure applied on propeller face (pressure side) on the propeller tip area outside $0,9R$ radius.	
Load case 5	60 per cent of F_f or F_b , whichever is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

10.7.5.1.4 Maximum backward blade ice force F_b for ducted propellers.

$$F_b = 66[nD]^{0,7} \left[\frac{EAR}{Z} \right]^{0,3} D^{0,6} H_{ice}^{1,4}, \text{ in kN, when } D \leq D_{limit},$$

$$F_b = 9,5[nD]^{0,7} \left[\frac{EAR}{Z} \right]^{0,3} D^2, \text{ in kN, when } D \leq D_{limit};$$

(10.7.5.1.4-1)

where $D_{limit} = 4H_{ice}$, in m;
 $n = n_n$ for a CP propeller;
 $n = 0,85n_n$ for a FP propeller.

(10.7.5.1.4-2)

10.7.5.1.5 Maximum forward blade ice force F_f for ducted propellers.

$$F_f = 250 \left[\frac{EAR}{Z} \right] D^2, \text{ in kN, when } D \leq D_{limit}; \quad (10.7.5.1.5-1)$$

$$F_f = 500 \left[\frac{EAR}{Z} \right] D \left(\frac{1}{1 - \frac{d}{D}} \right) H_{ice}, \text{ in kN, when } D \leq D_{limit} \quad (10.7.5.1.5-2)$$

$$\text{where } D_{limit} = \frac{2}{\left(1 - \frac{d}{D}\right)} H_{ice}, \text{ in m.}$$

10.7.5.1.6 Loaded area on the blade for ducted propellers.

Load cases 1 and 3 shall be covered as given in Table 10.7.5.1.6 for CP and FP propellers. Load case 5 shall be covered for FP propeller, to cover ice loads when the propeller is reversed.

10.7.5.1.7 Torque Q_{smax} .

The spindle torque Q_{smax} around the axis of the blade fitting shall be determined both for the maximum

backward blade force F_b and forward blade force F_f , which are applied as in Tables 10.7.5.1.3 and 10.7.5.1.6.

If the above method gives a value, which is less than the default value given by Formula (10.7.5.1.7), the default value shall be used:

$$Q_{smax} = 0,25 F c_{0,7}, \text{ in kNm}, \quad (10.7.5.1.7)$$

where F — F_b or F_f , whichever is greater.

10.7.5.1.8 Load distributions for blade loads.

The Weibull-type distribution (probability that F_{ice} exceeds $(F_{ice})_{max}$) is used for the fatigue design of the blade.

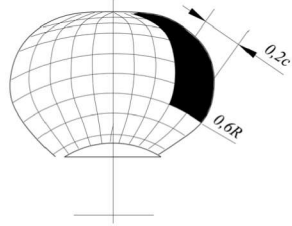
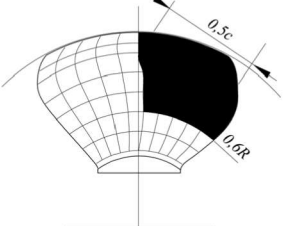
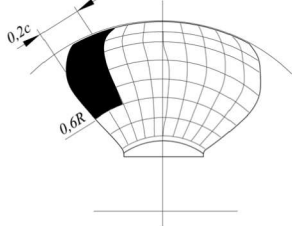
$$P\left(\frac{F_{ice}}{(F_{ice})_{max}} \geq \frac{F}{(F_{ice})_{max}}\right) = e^{\left(-\left(\frac{F}{(F_{ice})_{max}}\right)^k \ln(N_{ice})\right)} \quad (10.7.5.1.8)$$

where $k = 0,75$ shall be used for the ice force distribution of an open propeller;

$k = 1,0$ for that of a ducted propeller blade;

F_{ice} = random variable for ice loads on the blade, $0 < F_{ice} < (F_{ice})_{max}$.

Table 10.7.5.1.6

Load cases for ducted propellers			
	Force	Loaded area	Right handed propeller blade seen from behind
Load case 1	F_b	Uniform pressure applied on the back of the blade (suction side) to an area from $0,6R$ to the tip and from the leading edge to $0,2$ times the chord length	
Load case 3	F_f	Uniform pressure applied on the blade face (pressure side) to an area from $0,6R$ to the tip and from the leading edge to $0,5$ times the chord length	
Load case 5	60 per cent of F_f or F_b , whichever is greater	Uniform pressure applied on propeller face (pressure side) to an area from $0,6R$ to the tip and from the trailing edge to $0,2$ times the chord length	

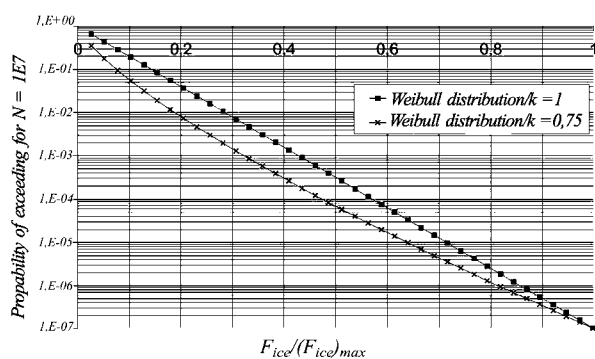


Fig. 10.7.5.1.8 The Weibull-type distribution

10.7.5.1.9 Number of ice loads.

The number of load cycles per propeller blade in the load spectrum shall be determined by the following formula:

$$N_{ice} = k_1 k_2 k_3 k_4 N_{class} n \quad (10.7.5.1.9)$$

where

Ice class	IA Super	IA	IB	IC
Impacts in life n	$9 \cdot 10^6$	$6 \cdot 10^6$	$3,4 \cdot 10^6$	$2,1 \cdot 10^6$

Propeller location	Centre propeller	Wing propeller
Propeller location factor k_1	1	1,35

Propeller type	open	ducted
Propeller type factor k_2	1	1,1

Type	fixed	azimuthing
Propulsion type factor k_3	1	1,2

The submersion factor k_4 is determined from the following equation:

$$\begin{aligned} k_4 &= 0,8 - f \text{ when } f < 0; \\ k_4 &= 0,8 - 0,4f \text{ when } 0 \leq f \leq 1; \\ k_4 &= 0,6 - 0,2f \text{ when } 1 < f \leq 2,5; \\ k_4 &= 0,1 \text{ when } f > 2,5 \end{aligned}$$

where the immersion function $f = \frac{h_0 - H_{ice}}{D/2} - 1$.

For components that are subject to loads resulting from propeller/ice interaction with all the propeller blades, the number of load cycles N_{ice} shall be multiplied by the number of propeller blades Z .

10.7.5.2 Axial design loads for open and ducted propellers.

10.7.5.2.1 Maximum thrusts T_f and T_b :

$$T_f = 1,1 F_f, \text{ in kN};$$

$$T_b = 1,1 F_b, \text{ in kN}.$$

10.7.5.2.2 Design thrust along the propulsion shaft line.

The design thrust along the propeller shaft line T_r shall be calculated with the formulae below; the greater value of the forward and backward direction loads shall be taken as the design load for both directions. The factors 2,2 and 1,5 take into account the dynamic magnification resulting from axial vibration.

$$T_r = T + 2,2 T_f, \text{ in kN}; \quad (10.7.5.2.2-1)$$

$$T_r = 1,5 T_b, \text{ in kN}. \quad (10.7.5.2.2-2)$$

If the hydrodynamic bollard thrust, T_b is not known, T shall be taken as follows:

Propeller type	T
CP propellers (open)	$1,25 T_n$
CP propellers (ducted)	$1,1 T_n$
FP propellers driven by turbine or electric motor	T_n
FP propellers driven by diesel engine (open)	$0,85 T_n$
FP propellers driven by diesel engine (ducted)	$0,75 T_n$

Here T_n = nominal propeller thrust at MCR in the free running open water condition.

10.7.5.3 Torsional design loads.

10.7.5.3.1 Maximum torque on a propeller Q_{max} for open propellers.

$$Q_{max} = 10,9 \left[1 - \frac{d}{D} \right] \left[\frac{P_{0,7}}{D} \right]^{0,16} (nD)^{0,17} D^3, \text{ in kNm},$$

when $D \leq D_{limit}$;

$$Q_{max} = 20,7 \left[1 - \frac{d}{D} \right] \left[\frac{P_{0,7}}{D} \right]^{0,16} (nD)^{0,17} D^{1,9} H_{ice}^{1,1}, \text{ in kNm},$$

when $D > D_{limit}$

where $D_{limit} = 1,8 H_{ice}$, in m;

n = rotational propeller speed in bollard condition. If not known, n shall be taken as follows:

Тип движителя	n
CP propellers	n_n
FP propellers driven by turbine or electric motor	n_n
FP propellers driven by diesel engine	$0,85 n_n$

For CP propellers, the propeller pitch, $P_{0,7}$ shall correspond to MCR in bollard condition. If not known, $P_{0,7}$ shall be taken as $0,7 P_{0,7n}$, where $P_{0,7n}$ — propeller pitch at MCR in free running condition.

10.7.5.3.2 Maximum torque on a propeller Q_{max} for ducted propellers.

$$Q_{max} = 7,7 \left[1 - \frac{d}{D} \right] \left[\frac{P_{0,7}}{D} \right]^{0,16} (nD)^{0,17} D^3, \text{ in kNm},$$

when $D \leq D_{limit}$;

$$Q_{\max} = 14,6 \left[1 - \frac{d}{D} \right] \left[\frac{P_{0,7}}{D} \right]^{0,16} (nD)^{0,17} D^{1,9} H_{ice}^{1,1}, \text{ in kNm,}$$

when $D > D_{limit}$

where $D_{limit} = 1,8H_{ice}$, in m;

for n and $P_{0,7}$ — refer to 10.7.5.3.1.

10.7.5.3.3 Ice torque excitation for open and ducted propellers.

The propeller ice torque excitation for shaft line transient torsional vibration analysis shall be described by a sequence of blade impacts which are of a half sine shape (refer to Fig. 10.7.5.3.3). The torque resulting from a single blade ice impact as a function of the propeller rotation angle is then

$$Q(\varphi) = C_4 Q_{\max} \sin(\varphi(180/\alpha_i)) \text{ when } \varphi = 0 \dots \alpha_i;$$

$$Q(\varphi) = 0 \text{ when } \varphi = \alpha_i \dots 360^\circ$$

where C_4 and α_i parameters are given in Table 10.7.5.3.3.

Table 10.7.5.3.3

Torque excitation	Propeller/ice interaction	C_4	α_i
Case 1	Single ice block	0,75	90
Case 2	Single ice block	1,0	135
Case 3	Two ice blocks (phase shift $360/2Z$, in deg.)	0,5	45

The total ice torque is obtained by summing the torque of single blades, taking into account the phase shift $360^\circ/Z$. In addition, at the beginning and at the end of the milling sequence a linear ramp functions for 270° of rotation angle shall be used.

The number of propeller revolutions during a milling sequence shall be obtained from the formula

$$N_Q = 2H_{ice}$$

The number of impacts is $Z \cdot N_Q$ for blade order excitation.

10.7.5.3.4 Design torque along propeller shaft line.

If there is not any relevant first blade order torsional resonance within the designed operating rotational speed range extended 20 per cent above the maximum and 20 per cent below the minimum operating speeds, the following estimation of the maximum torque Q_r can be used.

$$Q_r = Q_{\max} \frac{I}{I_t}, \text{ in kNm.}$$

All the torques and the inertia moments shall be reduced to the rotation speed of the component being examined.

If the maximum torque Q_{\max} is not known, it shall be taken as follows:

Propeller type	Q_{\max}
Propellers driven by electric motor	Q_{motor}
CP propellers not driven by electric motor	Q_n
FP propellers driven by turbine	Q_n
FP propellers driven by diesel engine	$0,75Q_n$

If there is a first blade order torsional resonance within the designed operating rotational speed range extended 20 per cent above the maximum and 20 per cent below the minimum operating speeds, the design torque Q_r of the shaft component shall be determined by means of torsional vibration analysis of the propulsion line.

10.7.5.4 Blade failure load

$$F_{ex} = \frac{300ct^2\sigma_{ref}}{0,8D - 2r}, \text{ in kN,}$$

where c , t , and r are determined for the weakest blade section outside the root fillet.

10.7.6 Design.

10.7.6.1 Design principle.

The strength of the propulsion line shall be designed according to the pyramid strength principle. This means that the loss of the propeller blade shall not cause any significant damage to other propeller shaft line components.

10.7.6.2 Propeller blade.

10.7.6.2.1 Calculation of blade stresses.

The blade stresses shall be calculated for the design loads given in 10.7.5.1.

Finite element analysis shall be used for stress analysis for final approval for all propellers. The following simplified formulae can be used in estimating the blade

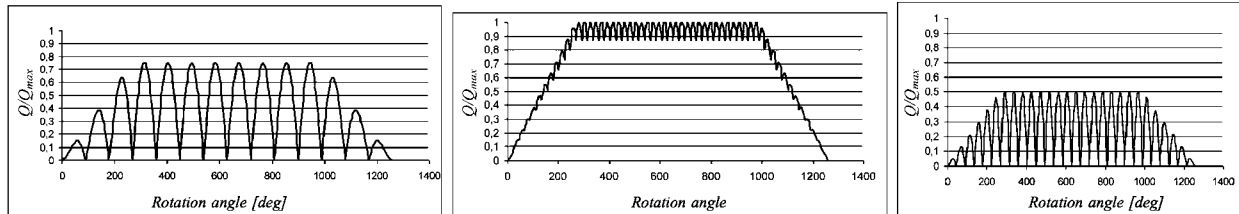


Fig. 10.7.5.3.3 The shape of the propeller ice torque excitation for 90° and 135° single-blade impact sequences and 45° double blade impact sequence. Figures apply for propellers with 4 blades

stresses for all propellers at the root area ($r/R < 0,5$). The root area dimensions based on Formula (10.7.6.2.1) can be accepted even if the FEM analysis would show greater stresses at the root area.

$$\sigma_{st} = C_1 \frac{M_{BL}}{100ct^2}, \text{ in MPa,} \quad (10.7.6.2.1)$$

where $C_1 = \frac{\text{actual stress}}{\text{stress obtained with beam equation}}$. If the actual value is not available, C_1 shall be taken as 1,6.

$M_{BL} = (0,75 - r/R) \cdot R \cdot F$
where $F = F_b$ or F_f , whichever is greater.

10.7.6.2.2 Acceptability criterion.

The following criterion for calculated blade stresses has to be fulfilled:

$$\frac{\sigma_{ref2}}{\sigma_{st}} \geq 1,5.$$

If FEM analysis is used in estimating the stresses, von Mises stresses shall be used.

10.7.6.2.3 Fatigue design of propeller blade.

The fatigue design of the propeller blade is based on an estimated load distribution for the service life of the ship and the S-N curve for the blade material. An equivalent stress that produces the same fatigue damage as the expected load distribution shall be calculated and the acceptability criterion for fatigue shall be fulfilled. The equivalent stress is normalised for 10^8 cycles.

If the following criterion is fulfilled, fatigue calculations according to this chapter are not required.

$$\sigma_{exp} \geq B_1 \sigma_{ref2}^{B_2} \log(N_{ice})^{B_3}$$

where B_1 , B_2 and B_3 = coefficients for open and ducted propellers are given in Table 10.7.6.2.3-1.

Table 10.7.6.2.3-1

	Open propeller	Ducted propeller
B_1	0,00270	0,00184
B_2	1,007	1,007
B_3	2,101	2,470

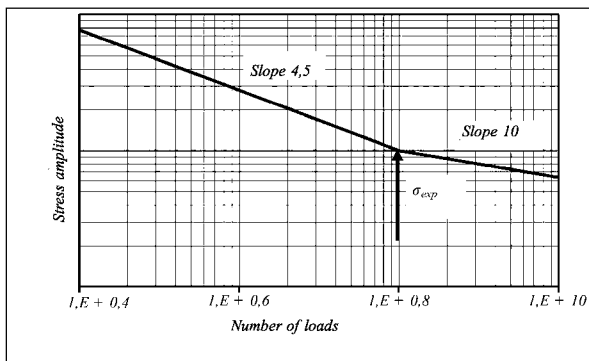


Fig. 10.7.6.2.3-1 Two-slope SN-curve

For calculation of equivalent stress two types of SN-curves are available:

two slope SN-curve (slopes 4,5 and 10), refer to Fig. 10.7.6.2.3-1;

one slope SN-curve (the slope can be chosen), refer to Fig. 10.7.6.2.3-2.

The type of the SN-curve shall be selected to correspond to the material properties of the blade. If the SN-curve is not known, the two slope SN-curve shall be used.

10.7.6.2.3.1 Equivalent fatigue stress.

The equivalent fatigue stress for 10^8 stress cycles which produces the same fatigue damage as the load distribution is:

$$\sigma_{fat} = \rho(\sigma_{ice})_{\max} \quad (10.7.6.2.3.1)$$

where $(\sigma_{ice})_{\max} = 0,5((\sigma_{ice})_{f\max} - (\sigma_{ice})_{b\max})$.

In calculation of $(\sigma_{ice})_{\max}$, case 1 and case 3 (or case 2 and case 4) are considered as a pair for $(\sigma_{ice})_{f\max}$ and $(\sigma_{ice})_{b\max}$ calculations. Case 5 is excluded from the fatigue analysis.

10.7.6.2.3.2 Calculation of parameter ρ for two-slope SN-curve.

The parameter ρ relates the maximum ice load to the distribution of ice loads according to the regression formula

$$\rho = C_1(\sigma_{ice})_{\max} C_2 \sigma_{fl} C_3 \log(N_{ice}) C_4 \quad (10.7.6.2.3.2)$$

where $\sigma_{fl} = \gamma_e \gamma_v \gamma_m \sigma_{exp}$.

The following values shall be used for the reduction factors if actual values are not available: $\gamma_e = 0,67$, $\gamma_v = 0,75$ и $\gamma_m = 0,75$.

The coefficients C_1 , C_2 , C_3 and C_4 are given in Table 10.7.6.2.3.2.

Table 10.7.6.2.3.2

	Open propeller	Ducted propeller
C_1	0,000711	0,000509
C_2	0,0645	0,0533
C_3	— 0,0565	— 0,0459
C_4	2,22	2,584

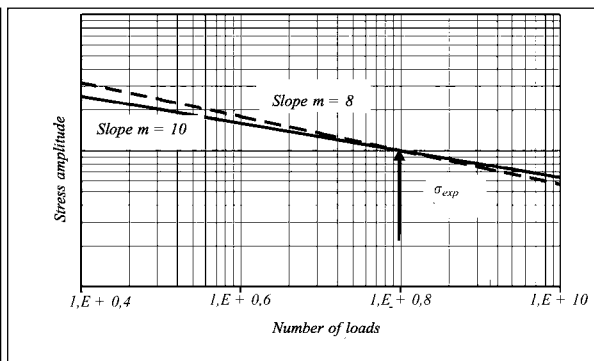


Fig. 10.7.6.2.3-2 Constant-slope SN-curve

10.7.6.2.3.3 Calculation of parameter p for constant-slope SN-curve.

For materials with a constant-slope SN-curve, the factor p shall be calculated from the formula

$$p = \left(G \frac{N_{ice}}{N_R} \right)^{1/m} (\ln(N_{ice}))^{-1/k} \quad (10.7.6.2.3.3)$$

where $k = 1,0$ for ducted propellers;
 $k = 0,75$ for open propellers.

Values for the parameter G are given in Table 10.7.6.2.3.3. Linear interpolation may be used to calculate the value for other m/k ratios than given in Table 10.7.6.2.3.3.

10.7.6.2.4 Acceptability criterion for fatigue.

The equivalent fatigue stress at all locations on the blade has to fulfil the following acceptability criterion

$$\frac{\sigma_{fl}}{\sigma_{fat}} \geq 1,5$$

where $\sigma_{fl} = \gamma_\varepsilon \gamma_v \gamma_m \sigma_{exp}$.

The following values shall be used for the reduction factors if actual values are not available: $\gamma_\varepsilon = 0,67$, $\gamma_v = 0,75$ и $\gamma_m = 0,75$.

10.7.6.3 Propeller bossing and CP mechanism.

The blade bolts, the CP mechanism, the propeller boss, and the fitting of the propeller to the propeller shaft shall be designed to withstand the maximum and fatigue design loads, as defined in 10.7.5. The safety factor against yielding shall be greater than 1,3 and that against fatigue greater than 1,5. In addition, the safety factor for loads resulting from loss of the propeller blade through plastic bending as defined in 10.7.5.4 shall be greater than 1,0 against yielding.

10.7.6.4 Propulsion shaft line.

The shafts and shafting components, such as the thrust and stern tube bearings, couplings, flanges and sealings, shall be designed to withstand the propeller/ice interaction loads as given in 10.7.5. The safety factor is to be at least 1,3.

10.7.6.4.1 Shafts and shafting components.

The ultimate load resulting from total blade failure as defined in 10.7.5.4 shall not cause yielding in shafts and shaft components. The loading shall consist of the combined axial, bending, and torsion loads, wherever this is significant. The minimum safety factor against yielding shall be not less than 1,0 for bending and torsional stresses.

10.7.6.5 Azimuthing main propulsors.

In addition, special consideration shall be given to those loading cases which are extraordinary for propulsion units when compared with conventional propellers. The estimation of loading cases has to reflect the way of operation of the ship and the thrusters. In this respect, for example, the loads caused by the impacts of ice blocks on the propeller hub of a pulling propeller have to be considered. Furthermore, loads resulting from the thrusters operating at an oblique angle to the flow have to be considered.

The steering mechanism, the fitting of the unit, and the body of the thruster shall be designed to withstand the loss of a blade without damage. The loss of a blade shall be considered for the propeller blade orientation which causes the maximum load on the component being studied. Typically, top-down blade orientation places the maximum bending loads on the thruster body.

Azimuth thrusters shall also be designed for estimated loads caused by thruster body/ice interaction. The thruster body has to stand the loads obtained when the maximum ice blocks, which are given in 10.7.3, strike the thruster body when the ship is at a typical ice operating speed. In addition, the design situation in which an ice sheet glides along the ship's hull and presses against the thruster body should be considered. The thickness of the sheet shall be taken as the thickness of the maximum ice block entering the propeller, as defined in section 10.7.3.

10.7.6.6 Calculation of shaft line vibrations.

The propulsion system shall be designed in such a way that the complete dynamic system is free from harmful torsional, axial, and bending resonances at a 1-order blade frequency within the designed running speed range, extended by 20 per cent above and below the maximum and minimum operating rotational speeds. If this condition cannot be fulfilled, a detailed vibration analysis has to be carried out in order to determine that the acceptable strength of the components can be achieved.

10.7.7 Alternative design procedure.

10.7.7.1 Scope.

As an alternative to 10.7.5 and 10.7.6, a comprehensive design study may be carried out upon agreement with the Register. The study may be based on ice conditions given for different ice classes in 10.7.3, include fatigue and maximum load design calculations and fulfil the pyramid strength principle, as given in 10.7.6.1.

Table 10.7.6.2.3.3

Value for the parameter G for different m/k ratios

m/k	3	3,5	4	4,5	5	5,5	6	6,5	7	7,5	8	8,5	9	9,5	10
G	6	11,6	24	52,3	120	287,9	720	1871	5040	14034	40320	119292	362880	1,133·10 ⁶	3,623·10 ⁶

10.7.7.2 Loading.

Loads on the propeller blade and propulsion system shall be based on an acceptable estimation of hydrodynamic and ice loads.

10.7.7.3 Design levels.

The analysis shall indicate that all components transmitting random (occasional) forces, excluding propeller blade, are not subjected to stress levels in excess of the yield stress of the component material, with a reasonable safety margin. Cumulative fatigue damage calculations shall indicate a reasonable safety factor. Due account shall be taken of material properties, stress raisers, and fatigue enhancements.

Vibration analysis shall be carried out and shall indicate that the complete dynamic system is free from harmful torsional resonances resulting from propeller/ice interaction.

10.8 MISCELLANEOUS MACHINERY REQUIREMENTS**10.8.1 Starting arrangements.**

The capacity of the air receivers shall be sufficient to provide without reloading not less than 12 consecutive starts of the propulsion engine, if this has to be reversed for going astern, or 6 consecutive starts if the propulsion engine does not have to be reversed for going astern.

If the air receivers serve any other purposes than starting the propulsion engine, they shall have additional capacity sufficient for these purposes.

The capacity of the air compressors shall be sufficient for charging the air receivers from atmospheric

to full pressure in 1 h, except for a ship with the ice class **IA Super**, if its propulsion engine shall be reversed for going astern, in which case the compressor shall be able to charge the receivers in 30 min.

10.8.2 Cooling water system.

The cooling water system shall be designed to ensure supply of cooling water when navigating in ice.

For this purpose at least one cooling water inlet chest shall be arranged as follows:

.1 the sea inlet shall be situated near the centreline of the ship and well aft if possible;

.2 as guidance for design the volume of the chest shall be about 1 m³ for every 750 kW engine output of the ship including the output of auxiliary engines necessary for the ship's service;

.3 the chest shall be sufficiently high to allow ice to accumulate above the inlet pipe;

.4 a pipe for discharge cooling water, allowing full capacity discharge, shall be connected to the chest;

.5 the open area of the strainer plates shall not be less than four times the inlet pipe sectional area.

If there are difficulties to meet the requirements of 10.8.2.2 and 10.8.2.3, two smaller chests may be arranged for alternating intake and discharge of cooling water, at that the requirements in 10.8.2.1, 10.8.2.4 and 10.8.2.5 shall be met.

Heating coils may be installed in the upper part of the sea chest.

Arrangements for using ballast water for cooling purposes may be useful as a reserve in ballast condition but cannot be accepted as a substitute for sea inlet chest as described above.

11 REQUIREMENTS FOR LNG BUNKERING SHIPS

11.1 GENERAL PROVISIONS AND SCOPE OF APPLICATION

11.1.1 These requirements apply to the gas carriers engaged in transportation of liquefied natural gas (LNG) and intended to ensure the transfer of LNG on board the ships using LNG as a fuel (hereinafter referred to as "LNG bunkering ships").

A descriptive notation and distinguishing marks specified in 2.2.37, Part I "Classification" may be added to LNG bunkering ships complying with these requirements.

11.1.2 Descriptive notations and distinguishing marks in the class notation of LNG bunkering ships.

For gas carrier complying with the requirements of this Section, except Chapter 11.13, the descriptive notation **LNG bunkering ship** may be added to the class notation after the descriptive notation **Gas carrier**.

When additional functions related to servicing of ships using LNG as a fuel are available on board the ship and when the ship meets the requirements specified in 11.13, the one of the following (or several) distinguishing marks may be added to the character of classification. When additional functions related to servicing of ships using LNG as a fuel are available on board and when the LNG bunkering ship meets the requirements specified in 11.13, one of the following (or several) distinguishing marks shall be introduced in the class notation **LNG bunkering ship**:

RE — where the ship is designed to receive LNG from a gas fuelled ship for which the LNG fuel tanks shall be emptied;

IG-Supply — where the ship is designed to supply inert gas and dry air, to ensure gas-freeing and aeration in compliance with 6.10.4 of the International Code of Safety for Ships Using Gases or Other Low Flashpoint Fuels (IGF Code);

BOG — where boil-off gas generated during the bunkering operation are provided on board the ship.

11.1.3 Definitions.

LNG bunkering station means room or space fitted with the following equipment:

hoses and piping connections used for liquid and vapour return lines, including the isolation shut-off valves and the emergency shut-down valves;

automation and alarms systems;

drip tray with its draining arrangement and other arrangements and systems intended for the ship structure protection;

gas and LNG leak detection systems;

associated firefighting systems.

LNG bunkering control room means a control room positioned in a safe location and intended for control of cargo pumps and valves, as well as where indication of fuel tank level and overfill alarm are provided.

Emergency shutdown system (ESD) means a system that safely and effectively stops the transfer of LNG and cargo vapour between the receiving ship and the bunkering ship in the event of an emergency during the bunkering operation, and puts the system in a safe condition.

Bunkering connections mean liquid and vapour connections between ships used for liquid product transfer to receiving ship and product vapour return to the LNG bunkering ship (i.e. manifold for a system with flexible hose and before the swivel for a system with transfer arm).

Emergency release coupling (ERC) means a coupling located on the receiving ship bunkering manifold or on the LNG transfer system, which separates at a predetermined section, when required, each separated section containing a self-closing shut-off valve, which seals automatically. An emergency release coupling can be activated:

by maximal allowable forces applied to the predetermined section;

by manual or automatic control, in case of emergency.

Quick connect/disconnect coupler (QCDC) means a manual or hydraulic mechanical device used to connect the LNG transfer system to the receiving ship manifold.

Sloshing means liquid oscillations effect at significant free surface in cargo and fuel tanks.

11.2 TECHNICAL DOCUMENTATION

11.2.1 In addition to technical documentation specified in 3.2, Part I "Classification" of these Rules and 6.1, Part I "Classification" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk, the following technical documentation shall be submitted:

.1 general arrangement of the ship with indication of LNG bunkering station, bunkering control station and escape routes;

.2 diagram and description of the cargo system; drawings of hose lines, swivels and transfer arms (where applicable);

.3 diagram and description of LNG vapour return transfer system; documentation for the reliquefaction

system (where applicable); calculation of maximum allowable bunkering flow;

.4 technical documentation for ESD bunkering system;

.5 electrical single line diagrams for all intrinsically-safe circuits;

.6 general arrangement plan of electrical equipment in hazardous areas related to bunker operations;

.7 technical documentation for fire detection and alarm system as well as gas detection system of the bunkering installation, including location of gas detectors, connection lines, valves and sampling points on board the ship;

.8 technical documentation for gauging, alarm and pressure indication system in the cargo tanks and piping;

.9 technical documentation for control and alarm system of cargo pumps.

11.2.2 The following operating documentation shall be submitted:

.1 risk analysis related to gas fuel bunkering operations and potential consequences of leakage according to the procedure agreed with the Register. The analysis shall consider risks of damage of hull structural members and failure of any equipment due to the accident related to gas fuel leakage. The results of risk analysis shall be included in the ship's Operating manual;

.2 operating instructions containing the procedures of bunkering, interting and control of cargo vapour return.

11.3 ARRANGEMENT OF LNG BUNKERING SHIP

11.3.1 LNG bunkering ship shall comply with the requirements of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk and the International Code for the Construction and Equipment of Ships Carrying Liquefied Gases in Bulk (IGC Code).

11.3.2 The LNG bunkering station shall be located on the open deck in the area with sufficient natural ventilation. The LNG bunkering station shall be physically separated or structurally shielded from accommodation and control stations.

11.3.3 Escape routes shall have safe access for crew engaged in operation. The LNG bunkering station shall be sufficiently illuminated from two floodlights located to minimize shadow areas on deck and high enough to minimize dazzle effect to personnel involved in bunkering operations.

11.3.4 The bunker connections shall be clearly visible from the navigation bridge and bunker operation control position where continuous watch is kept during the transfer. CCTV can be accepted as substitute for the

direct view when it provides unobstructed view of the bunker connections.

11.3.5 Arrangement of work platforms in areas where liquid spill may occur shall exclude liquid spill accumulation at the platform surface. Gratings used in this location shall be suitable for low temperatures. Area under the gratings shall be equipped with spill collecting trays with drainage arrangements suitable for draining the accumulated spill overboard. The drain shall be fitted with a shut-off valve.

11.3.6 Drip trays and drainage arrangements shall be fitted below bunkering connections where LNG leakage may occur leading to the ship structure damage. Thermal sensors shall be positioned in way of bunkering connections in the drip tray.

The drip trays shall be made of stainless steel, and capable of being remotely drained over the ship's side without risk of structural damage to the ships involved in bunkering operations.

11.3.7 When bunker boiling point is lower than allowable temperature of the hull steel, the hull structure in the possible area of LNG spill shall be effectively protected from low temperature in case of a major bunker spill. Where water curtain is used for hull protection, the pumps shall be arranged with redundancy.

11.4 HULL AND STABILITY

11.4.1 The hull structure and stability of the LNG bunkering ship shall comply with the requirements of Part II "Gas Carrier Design" and Part III "Stability, Subdivision, Freeboard" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk and the following additional requirements:

.1 LNG bunkering ship shall be able to abort bunkering operation at any stage in case of emergency. Therefore, cargo tanks on the ship shall not have restrictions on intermediate filling;

.2 internal transfer between cargo tanks within short period of time to avoid dangerous sloshing zone may be accepted during cargo and bunkering operations.

11.5 FIRE PROTECTION

11.5.1 Structural fire protection of LNG bunkering ship shall meet the requirements of Part V "Fire Protection" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk and the following additional requirements.

When applicable, the bunkering station shall be separated by fire-fighting divisions of class A-60 from other spaces. Fire integrity may be reduced to class A-0

for spaces and areas with low fire risk such as tanks with non-combustible medium, voids, auxiliary machinery spaces of no fire risk, sanitary and similar spaces.

11.5.2 Fire extinguishing systems of LNG bunkering ship shall meet the requirements of Part V "Fire Protection" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases and the following additional requirements:

.1 water spray system shall be fitted to protect the bunkering manifolds, associated piping, arms, loading hoses and the transfer area. The system capacity shall not be less than those specified in 3.3.2 of Part V "Fire Protection" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk;

.2 in the bunkering station area a permanently installed dry powder system shall cover all possible LNG leak points. The capacity shall be at least 3,5 kg/s for a maximum of 45 s discharges. The manual release shall be located at easily accessible and safe position outside the protected area;

.3 one dry powder fire-extinguisher of at least 5 kg capacity shall be located near the bunkering station.

11.5.3 Exhaust gas system shall meet the requirements of Part VIII "Systems and Piping" of these Rules, therewith, the outlets of the exhaust gas pipes of the internal combustion engines, boilers and incinerators shall be provided with spark arresters.

11.5.4 Use of equipment for disposing the evaporated cargo by thermal oxidation method not complying with the requirements of 4.3, Part VI "Systems and Piping" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk shall be prohibited during bunkering operations.

11.6 CARGO SYSTEM

11.6.1 The following components shall be obligatory included in the cargo system:

- bunkering hoses and/or mechanical loading arms;
- quick connect/disconnect coupler (QCDC);
- emergency release coupling (ERC);
- electrical insulating joint.

11.6.2 Cargo system and the bunkering fuel transfer procedure shall be so designed to avoid the release of gas or liquid to the atmosphere both from bunkering and receiving ships during bunkering operations.

11.6.3 Bunker transfer piping system for products with boiling point below -55°C shall be thermally insulated to minimize heat leaks to transferred gas bunker and protect personnel from direct contact with cold surfaces.

11.6.4 Bunkering hoses.

11.6.4.1 Bunkering hoses shall meet the requirements of 5.11.7 of the IGC Code, applicable require-

ments of 6.2, Part VIII "Systems and Piping" of these Rules and shall have Type Approval Certificate (CTO). In addition to the above requirements, the requirements specified in 11.6.4.2 — 11.6.4.10 shall be complied with during the type testing of bunkering hoses.

11.6.4.2 All the applicable materials shall be compatible with each other and transported medium (LNG and LNG vapors). The end fittings shall be manufactured of stainless steel and comply with the IGC Code requirements.

11.6.4.3 The following characteristics shall be defined by the manufacturer of the bunkering hose and confirmed during type tests:

- minimum working temperature;
- maximum working load;
- maximum design pressure;
- minimum bend radius (MBR);
- maximum allowable applied twist (MAAT).

11.6.4.4 Each hose type shall be subjected to a pressure cycle test at ambient temperature to demonstrate that the hose is capable of withstanding 2 000 pressure cycle test from zero to at least twice the specified maximum working pressure. The hose assembly shall be also subjected to a cryogenic temperature and pressure cycle test with a minimum of 200 combined test cycles. After the cycling test, the crushing test shall be carried out at the pressure at least 5 times exceeding the maximum working pressure at the minimum working temperature.

11.6.4.5 Each hose type shall be subjected to a bending cycle fatigue test, at ambient and cryogenic temperature (with 400 000 cycles without failure). In such case, the fatigue bend radius shall be accepted in accordance with the manufacturer's recommendation.

11.6.4.6 Each hose type shall be subjected to a crushing test at ambient temperature and cryogenic temperature. The hose assembly shall be held between two rigid plates at the length equivalent to the diameter of the hose and a force of 1000N shall be applied ten times at the same location in the middle of each flexible hose.

11.6.4.7 Each hose type shall be subjected to a tensile test at ambient and minimum working temperature for determining the maximum working load.

11.6.4.8 Each hose type shall be subjected to a bending test at room and cryogenic temperature to ensure that the hose is capable of withstanding the maximum working pressure at MBR. Hose shall be gradually bent to the MBR and then pressurized to the maximum working pressure. Hose shall be examined for leaks whilst being held for 15 min at MBR. After pressure relief and hose unbending, it shall be examined for visual damage.

11.6.4.9 Each hose type shall be subjected to a tensile test at room and cryogenic temperature to ensure that the hose is capable of withstanding the maximum

working pressure at MAAT. The hose assembly shall be gradually twisted to the MAAT and then pressurized to the maximum working pressure. The hose shall be examined for leaks whilst being held for 15 min at MAAT. After pressure relief and hose unbending, it shall be examined for visual damage.

11.6.4.10 Electrical resistance between the two end fittings of the hose shall be measured, and the hose assembly shall be drained and supported above ground by non-conductive means. Electrically conductive hoses shall have a resistance of less than 10 Ohm. Electrically non-conductive hoses shall have a resistance of at least 25 kOhm.

11.6.5 Quick connect/disconnect coupler (QCDC).

11.6.5.1 QCDC shall have Type Approval Certificate (CTO). The QCDC shall be subjected to a hydraulic pressure test, at ambient temperature, to a pressure not less than 1,5 times the design pressure, to demonstrate that the QCDC is capable of withstanding its pressure without leaking.

11.6.5.2 Controls of QCDC shall be fitted with mechanical interlocking device to prevent unintended operation. In case of supply failure the QCDC shall not change the position (shall stay in "as-is" position).

11.6.6 Emergency release coupling (ERC).

11.6.6.1 Emergency release coupling (ERC) or break-away coupling shall be provided in the bunkering line. Adequacy shall be observed regarding the compatibility with hoses and the maximum axial and shear forces likely to be exerted on the break-away or the ERC during the bunkering operations. The ERC and break-away coupling shall have Type Approval Certificate (CTO).

11.6.6.2 ERC used in bunker connection shall be of "dry-break" type and be capable to self-disconnect upon application of force at any direction of ship's relative motion, which exceeds design loads, and at pressure surge exceeding the coupling design pressure.

ERC fitted in lines for transfer of gas fuel shall be capable to break-away through the ice accumulated on the coupling during the LNG transfer.

11.6.7 Electrical insulating joint.

Each electrical insulating joint shall be air tested. In this case, the resistance shall be at least 10 kOhm. Resistance of each insulating flange shall be measured when the LNG tank is completely filled and amounted to at least 1000 Ohm, but not exceed 1000 kOhm.

11.6.8 Cargo swivel.

Cargo swivel having Type Approval Certificate (CTO) shall be provided in the bunkering line. Swivels shall be subject to static and dynamic hydraulic pressure tests at the maximum working pressure. During the dynamic tests, at least two complete rotations in each direction shall be performed at normal conditions and minimum working temperature.

11.6.9 The bunkering line shall be suitably supported in such a way that to prevent the hose abrasion and to observe that the allowable bending radius is satisfied.

11.6.10 The cargo system shall be subjected in assembly to a hydraulic pressure test, at ambient temperature, to a pressure not less than 1,5 times the maximum design pressure of the system.

11.6.11 All welds of cargo system and hose line items shall be made with full penetration welding with 100 % inspection of welds by non-destructive examination.

11.6.12 The allowable LNG bunkering speed shall be determined by the characteristics of the receiving ship. The maximum LNG transfer velocity in the piping system and bunkering line shall not exceed 10 m/s in order to avoid the generation of static electricity and to limit the heat transfer due to friction inside the pipes.

The maximum LNG transfer velocity shall be determined considering the following:

- management of the BOG generated during bunkering operation;
- temperature and pressure of the LNG supplied to the receiving ship;
- characteristics of the receiving tank;
- maximum flow permitted by the ERC;
- maximum flow permitted by the hose;
- maximum flow permitted by the QCDC.

11.7 INERT GAS SYSTEM

11.7.1 Prior to the bunkering operations, the possibility shall be provided for tightness test of connections between the LNG bunkering and receiving ships. The procedure thereof shall be specified in the ship's Operating manual.

11.7.2 The relevant measures and procedures shall be provided for inerting the hose lines prior to filling them with bunkering fuel or LNG vapors, as well as inert-gas pressurization of bunkering fuel or LNG vapors from bunkering lines upon completion of cargo operations prior to disconnection. The cargo residuals shall be leading back to the cargo tanks.

11.8 GAS DETECTION SYSTEM

11.8.1 Installed onboard gas detection system shall be capable to measure gas concentration in the manifold connections area in addition to arrangements specified in Section 6, Part VIII "Instrumentation and Automation System" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk. Such system shall also provide a remote gas detection point for receiving ship.

11.8.2 Gas detection system at the manifold connection area shall provide continuous monitoring and activate alarm when concentration of hydrocarbons reaches 30 % of lower flammable limit (LFL).

11.8.3 Audible and visible alarm from the permanently installed gas detection system shall be located on the navigation bridge, in the bunkering operation control position and at the gas detector location.

11.9 ELECTRICAL EQUIPMENT

The requirements of this Chapter apply to electrical equipment of LNG bunkering ships and are addition to the requirements of Part XI "Electrical Equipment" of these Rules and Part VII "Electrical Equipment" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk.

11.9.1 The following systems of generation and distribution of electric energy are allowed:

- .1 direct current:
 - .1.1 two-wire insulated;
- .2 alternating current:
 - .2.1 single-phase, two-wire insulated;
 - .2.2 three-phase, three-wire insulated;
 - .2.3 three-phase, four-wire insulated.

11.9.1.3 In insulated distribution systems, no current-carrying part shall be earthed, other than the following:

- .1 arrangements and systems for insulation resistance monitoring;
- .2 components used for the radio interference suppression.

11.9.2 Earthed systems with hull return.

11.9.2.1 Earthed systems with hull return are not permitted, with the following exceptions:

- .1 impressed-current cathodic protection systems;
- .2 local earthed systems, such as starting and ignition systems of internal combustion engines, provided that any possible current does not flow directly through any hazardous areas and spaces;

.3 arrangements and systems for insulation resistance monitoring, provided that the circulation current of the device does not exceed 30 mA under the most unfavourable conditions.

.4 earthed intrinsically safe circuits;

.5 power supplies, control circuits and instrumentation circuits in non-hazardous areas where technical or safety reasons preclude the use of a system with no connection to earth, provided the current in the hull is limited to not more than 5 A in both normal and fault conditions;

.6 local earthed systems, such as power distribution systems in galleys and laundries to be fed through isolating transformers with the secondary windings earthed, provided that any possible resulting hull current does not flow directly through any hazardous areas and spaces.

11.9.3 Monitoring of circuits in hazardous areas.

11.9.3.1 The devices intended to continuously monitor the insulation resistance level of all separate

distribution systems shall also monitor all circuits, other than intrinsically safe circuits, connected to apparatus in hazardous areas or passing through such areas.

11.9.3.2 An audible and visual alarm shall be given, at a manned position, in the event of an abnormally low level of insulation.

11.10 EMERGENCY SHUT-DOWN SYSTEM (ESD)

11.10.1 The requirements of Part VIII "Instrumentation and Automation System" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk shall apply in a full scope to emergency shut-down systems (ESD). The ESD system shall stop the applied pumps and vapour return compressors (if any) before the manifold valves are closed. Any activation of the ESD systems shall be implemented simultaneously on both bunkering facility and receiving ship.

11.10.2 Pendant with means of control for local manual activation position for the ESD system shall be provided on board the receiving ship. When a LNG bunkering ship may connect on board ESD system to those of the receiving ship, pendant is not required.

11.10.3 The ESD function shall be initiated in following circumstances:

- .1 automatically, if the distance between a receiving ship and LNG bunkering ship exceeds safe operational envelope for transfer arrangement;
- .2 when activating manual ESD button on ESD pendant;
- .3 automatically at ERS activation.

11.10.4 Opening of main transfer valves shall not be possible unless ERS is re-assembled.

11.11 TRANSFER CONTROL SYSTEM

11.11.1 The transfer control system shall have provisions of automatic control of flow rate and limiting pressure in the transfer system. Parameters of the control system critical for the safe transfer shall have adjustable settings.

11.11.2 Deviations from set values specified in 11.11.1 shall activate audible and visual alarms at the bunker operations control position and on the navigation bridge.

11.11.3 The LNG transfer control system shall automatically reduce the LNG transfer rate when set values for pressure in the vapour return and/or vapour recovery system is exceeded.

11.11.4 If the LNG transfer rate exceeds a maximum value, alarm and automatic stop of transfer shall be activated and manifold valves closed.

11.11.5 The receiving ship shall have possibility to control LNG transfer flow rate by means of a ship-to-ship link, e.g. flexible cable and pendant with means of control.

11.11.6 Alarms and safety actions required for the LNG transfer system are specified in Table 11.11.6.

Table 11.11.6
Alarms and safety actions required for the LNG transfer system

Parameters	Alarm	Activation of the ESD systems	Automatic activation of ERC
Low pressure in the supply tank	×	×	
Sudden pressure drop at the fuel transfer pump	×	×	
High level in the receiving tank	×	×	
High pressure in the receiving tank	×	×	
LNG leak detection or vapour detection (anywhere)	×	×	
Gas detection around the bunkering pipe	×	×	
Manual activation of the ERC	×		
Safe working envelope of the loading arm exceeded	×	×	×
Disconnection of the ERC	×	×	

11.12 COMMUNICATION SYSTEMS

11.12.1 A communication system with back-up shall be provided between the LNG bunkering ship and the receiving ship.

11.12.2 Communications shall be maintained between the LNG bunkering ship and the receiving ship at all times during the bunkering operation. In the event that communications cannot be maintained, bunkering shall be stopped and not resumed until communications are restored.

11.12.3 The components of the communication system located in hazardous and safety zones shall be of a suitable framproof type.

11.13 ADDITIONAL SERVICE FEATURES RELATED TO SERVICING OF SHIPS USING LNG AS FUEL

11.13.1 When the additional features related to ships servicing are provided on board the LNG bunkering ship using LNG as fuel and indicated by the distinguishing mark **RE** added to the character of classification, the BOG handling system of the LNG bunkering ship shall have the capacity allowing to handle the extra vapours

generated during the cargo operation taking into account the increasing level in the receiving cargo tanks.

To confirm the ship compliance with the requirements applicable to ships with the distinguishing mark **RE**, the bunkering procedure for LNG receiving from a gas fueled ship with the required calculations shall be submitted.

11.13.2 When the additional features related to ships servicing are provided on board the LNG bunkering ship using LNG as fuel and indicated by the distinguishing mark **IG-Supply** added to the character of classification, the LNG bunkering ship shall be fitted with supply of inert gas and/or dry air to ensure gas freeing and aeration of fuel tanks in compliance with 6.10.4 of the IGF Code. The lines used for the inert gas shall be independent from the LNG liquid and vapour lines used for normal operation.

To confirm the ship compliance with the requirements applicable to ships with the distinguishing mark **IG-Supply**, a diagram of gas freeing system and procedure for gas freeing shall be submitted.

11.13.3 When the additional features related to ships servicing are provided on board the LNG bunkering ship using LNG as fuel and indicated by the distinguishing mark **BOG** added to the character of classification, the boil-off-gas system (BOG) generated during bunkering shall be provided. In such case, the LNG bunkering ship shall be capable of handling all or part of the boil-off gas from receiving ship, in addition to its own boil-off, generated during the LNG bunkering operation without release to the atmosphere. The boil-off gas handling capacity of the bunkering ship shall be indicated and justified by relevant calculations.

The following ways or their combination to the BOG dispose are allowed:

- reliquefaction;
- using gas as fuel in the ships fuel engine or boilers;
- burning in the gas flaring unit in compliance with 4.3, Part VI "Systems and Piping" of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk.

To confirm the ship compliance with the requirements applicable to ships with the distinguishing mark **BOG**, the following documents shall be submitted:

- bunkering procedure for boil-off gas management indicating the operations;
- calculation of the maximum LNG vapour flow rate possible to be generated during the bunkering to be less than the capacity of boil-off gas unit specified in the bunkering procedure.

12 REQUIREMENTS FOR SHIPS FOR COMPLIANCE WITH THE DISTINGUISHING MARK IWS IN THE CLASS NOTATION

12.1 GENERAL PROVISIONS AND SCOPE OF APPLICATION

12.1.1 For the ships constructed in compliance with this Chapter, the distinguishing mark **IWS** (in-water survey) is added to the character of classification denoting the ship is fit for in-water survey.

12.1.3 The conditions for in-water survey are specified in 2.5 of Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service.

12.2 TECHNICAL DOCUMENTATION

Drawing of the marking on the side and bottom plating to identify the tanks shall be submitted in the scope of plan approval documentation for a ship under construction.

12.3 TECHNICAL REQUIREMENTS

The distinguishing mark **IWS** may be assigned to the ships complying with the following additional requirements.

12.3.1 A ship shall have distinguishing mark **TMS** in the class notation or propeller and shafting arrangement shall comply with the requirements of 2.10.2, Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service for the minimum interval between surveys of 5 years.

12.3.2 Interval between the complete survey of main AMSS (if installed on board) shall not be less than 5 years in accordance with 2.10.8, Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service.

12.3.3 Underwater hull shall be fitted with an effective corrosion protective system consisting of combination of coating and cathodic protection systems.

12.3.4 Possible underwater washing of sea chests shall be provided, where necessary. For this purpose, closures of intake gratings shall have such a structure to ensure safe opening and closure by a diver.

12.3.5 For the water-lubricated rudder bearings, shall be provided to enable the in-water measurement of clearance in the rudder stock and pintles.

12.3.6 Underwater hull shall be marked.

Transverse and longitudinal reference lines of about 300 m in length and 25 mm in width shall be indicated as marking. The marks shall be permanent and made by welding or similar way, of contrasting colour to the hull.

As a rule, the marks shall be placed as follows:

at the flat bottom in the regions of tank bulkhead intersection or integrity of floors of the bottom longitudinal girders;

on board in the areas of transverse framing (marking shall not be higher than 1 m above the hopper plating);

at the double bottom intersection with watertight floor in the area of the ship sides;

at all suction and exhaust sea inlets.

Letter and numeric codes shall be placed on the plating for identification of tank, suction and exhaust sea inlets.

13 REQUIREMENTS FOR OFFSHORE SERVICE VESSELS

13.1 MODU/FOP SUPPLY VESSELS

13.1.1 General.

For vessels intended to supply MODU/FOP and complying with the requirements of this Chapter, a descriptive notation **Supply vessel (OS)** may be added to the character of classification.

13.1.2 Hull.

The hull structure shall comply with 3.8, Part II "Hull".

13.1.3 Equipment, arrangements and outfit.

13.1.3.1 Access means to the spaces located under the open cargo deck shall comply with 7.1.6, Part III "Equipment, Arrangements and Outfit".

13.1.3.2 Access means to machinery and boiler spaces shall comply with 7.6.6 of Part III "Equipment, Arrangements and Outfit".

13.1.3.3 Location of ventilators shall comply with 7.8.4 of Part III "Equipment, Arrangements and Outfit".

13.1.4 Stability.

The ship's stability shall comply with 3.11 of Part IV "Stability".

13.1.5 Subdivision.

As regards the subdivision, the vessel shall comply with 3.4.9 of Part V "Subdivision".

13.1.6 Systems and piping.

Uptakes of boilers, exhaust pipes of main and auxiliary engines and incinerators shall comply with 11.1.3 of Part VIII "Systems and Piping".

13.2 STANDBY VESSELS

13.2.1 General.

For ships intended to carry out rescue and standby services in offshore areas of hydrocarbon production and complying with the requirements of this Chapter, a descriptive notation **Standby vessel** may be added to the character of classification.

13.2.2 Hull.

The hull structure shall comply with the applicable requirements of 3.8, Part II "Hull".

13.2.3 Equipment, arrangements and outfit.

13.2.3.1 Access means to the spaces located under the open cargo deck shall comply with 7.1.6 of Part III "Equipment, Arrangements and Outfit".

13.2.3.2 Access means to machinery and boiler spaces shall comply with 7.6.6 of Part III "Equipment, Arrangements and Outfit".

13.2.3.3 Location of ventilators shall comply with 7.8.4 of Part III "Equipment, Arrangements and Outfit".

13.2.3.4 The ship shall be arranged on each side with a clearly marked rescue zone with a length of not less than 5 m. Rescue zones shall be located well clear of the propellers as well as any discharges extended at least 2 m below the load waterline.

13.2.3.5 In the rescue zones area the ship's sides shall be free of appendages (fenders, etc.).

13.2.3.6 The access routes from rescue zones to survivors' accommodation as well as to helicopter winching area, where provided, shall have non-slip surface or wooden sheathings.

13.2.3.7 Deck in way of the rescue zone shall be free of any obstruction (air pipes, valves, small hatches, etc.), as far as practical. If any, proper arrangement shall be provided as protection against personnel injury.

13.2.3.8 Bulwark or railings in way of the rescue zone shall be of a type easy to open or remove.

13.2.3.9 Each rescue zone shall be provided with a scrambling net made of corrosion resistant in the marine environment and non-slip material of at least 5 m wide and length enough to extend at least 1 m from the deploying area in the rescue zone till the minimal service waterline.

13.2.3.10 The ship shall be provided with power assisted means capable of ensuring careful recovery of injured persons from the sea.

13.2.3.11 The ship shall be equipped with gears for towing of liferafts and rescue boats.

13.2.3.12 Bridge front and side windows shall be equipped with efficient storm shutters installed at any side of bulkhead. Strength of these shutters shall be equivalent to strength of the bulkhead. Storm shutters shall provide visibility from the bridge; they may be portable and stowed in an accessible position, so as to be readily mounted.

13.2.4 Life-saving appliances.

13.2.4.1 The ship shall be equipped with at least one fast rescue boat of type complying with LSA Code, permanently ready for use. The emergency source of power of the launching arrangement of a fast rescue boat shall provide operation of the launching arrangement for at least 4 h.

13.2.4.2 Type approved lifejackets shall be provided for 25 per cent of the number of survivors for which the ship is intended to carry.

13.2.5 Survivors' spaces.

13.2.5.1 The ship shall have a treatment room for casualties, a recovery room with beds, and enclosed space to accommodate survivors. These spaces shall be provided with lighting and means to control temperature and humidity suitable for the area of operation.

13.2.5.2 The designed capacity of survivor's spaces shall be determined considering 0,75 m² per person. This includes free floor space and floor space with loose furniture, fixed seating and/or fixed beds. Other fixed furniture, toilets and bathrooms shall be excluded.

13.2.5.3 At least one installation comprising a toilet, a wash basin and shower shall be provided for each group of 50 survivors.

13.2.6 Stability.

The ship's stability shall comply with 3.11 of Part IV "Stability".

13.2.7 Subdivision.

As regards the subdivision, the ship shall comply with 3.4.3 of Part V "Subdivision".

13.2.8 Systems and piping.

13.2.8.1 Uptakes of boilers, exhaust pipes of main and auxiliary engines and incinerators shall comply with 11.1.3 of Part VIII "Systems and piping".

13.2.8.2 A decontamination area equipped with a shower system shall be arranged before entering to deckhouse accommodations from rescue zones.

13.2.9 Machinery installations.

The ship shall be fitted with at least two propulsion systems capable of moving the ship in the forward and aft direction.

13.2.10 Electrical equipment.

13.2.10.1 A searchlight shall be available on each side and adjustable from inside the navigation bridge. Each searchlight shall be able to provide an illumination level of 50 lx in clear air, within an area not less than 10 m diameter, to a distance of at least 250 m.

13.2.10.2 In addition to 6.7.1 of Part XI "Electrical equipment", illumination of the following spaces shall be at least:

.1 150 lx of total illumination level for overboard spaces, at a distance of within 5 m from the ship side in the rescue zone and reception areas for survivors;

.2 50 lx of total illumination level for overboard spaces at a distance within 20 m from the ship side along the rescue zone and survivors reception area.

13.2.10.3 In addition to 6.1.1 of Part XI "Electrical equipment" lighting with power from the main and emergency source shall be provided for the following spaces:

.1 storage spaces for rescue boats and their launching arrangements, reception areas for survivors and rescue zones;

.2 overboard spaces in the rescue zone, survivors' reception areas, in areas of rescue boats launching;

.3 helicopter winching areas and routes to this area from survivors' reception areas.

Time of lighting source from emergency source shall be at least 30 min.

13.3 ANCHOR HANDLING VESSELS

13.3.1 General.

For ships equipped for servicing (handling, heaving up and shifting) anchors and complying with the requirements of this Chapter, the descriptive notation **Anchor handling vessel** may be added to the character of classification.

For ships, equipped for anchor servicing and towing of floating facilities, the descriptive notation **Anchor handling vessel, Tug** may be added to the character of classification.

13.3.2 Documentation.

In addition to documentation specified in Section 3, Part I "Classification" the following documents shall be submitted (A — for approval; AG — for agreement, FI — for information):

13.3.2.1 Arrangement plan of anchor handling equipment: anchor handling winches, shark jaws, towing pins, stern rollers, cargo handling gear, where available, including standard cargo placing on the deck (anchors, cables, chains, etc.) indicating the towing line path, extreme sectors, maximum design towing pull, maximum design load for each component (FI).

13.3.2.2 For anchor handling winches:

.1 design criteria, including design loads and characteristics of emergency quick release system of towing line indicating the response time and remaining holding force after release) (FI);

.2 strength calculation of winch drum with flanges, shaft couplings, housing and brakes (AG);

.3 assembly drawings and general view (A).

13.3.2.3 For shark jaw:

.1 design criteria, including design loads and characteristics of emergency quick release system in operational and dead ship conditions (FI);

.2 strength calculation (AG);

.3 assembly drawings and general view (A).

13.3.2.4 For towing pins:

.1 design criteria, including design loads and characteristics of emergency release capabilities in operational and dead ship conditions (FI);

.2 strength calculation (AG);

.3 assembly drawings and general view (A).

13.3.2.5 For stern rollers:

.1 design criteria, including design loads (FI);

.2 strength calculation (AG);

.3 assembly drawings and general view (A).

13.3.2.6 Drawings of foundations and supports for winches, shark jaws, stern rollers and towing pins indicating the maximum design load (A).

13.3.2.7 Electrical power supply circuits and control system configuration of towing equipment and anchor handling equipment (A).

13.3.2.8 Arrangement plan (A) and technical specification of operator control stands (user interface) of towing equipment control systems and anchor handling equipment (AG).

13.3.2.9 Arrangement plan (A) and technical specification of communication means between the anchor operations control station and wheelhouse (AG).

13.3.2.10 Bollard pull estimation (FI).

13.3.2.11 Bollard pull test procedure (A).

13.3.3 Hull.

The hull structure shall comply with the applicable requirements of **3.8**, Part II "Hull".

13.3.4 Equipment, Arrangements and Outfit.

13.3.4.1 Design loads of arrangements specified in **13.3.2.3** to **13.3.2.5** shall be assumed in compliance with **5.4.2.2**, Part III "Equipment, Arrangements and Outfit". In such case, the stress in these components shall not exceed 0,8 yield strength of their material.

13.3.4.2 Anchor handling winch shall be fitted with towing line tension measuring means.

13.3.5 Stability.

13.3.5.1 Stability of ships with the descriptive notation **Anchor handling vessel** shall comply with the requirements of **3.7.3**, Part IV "Stability".

13.3.6 Subdivision.

13.3.6.1 Ships with the descriptive notation **Anchor handling vessel** shall comply with the requirements of **3.4.9**, Part V "Subdivision".

13.3.6.2 In addition to **3.4.9**, the ships with the descriptive notations **Anchor handling vessel**, **Tug** shall also comply with the requirements of **3.4.4**, Part V "Subdivision".

13.3.7 Machinery.

13.3.7.1 Anchor handling winches shall comply with the applicable requirements of **6.1** and **6.5.5**, Part IX "Machinery".

13.3.8 Electrical equipment.

13.3.8.1 Anchor handling winches shall be controlled from control stations where sufficient visibility of the winch drums is provided. Controls shall ensure single action control by one operator; therewith the selected operating mode shall be clearly distinguished from other modes provided. In case of control system failure, the arrangement shall be set in safe position.

13.3.8.2 Anchor handling winch shall be controlled both in anchor hoisting and dropping modes.

13.3.8.3 In compliance with **13.3.4.2**, the information of towing line tension shall be displayed at the winch control panels or in the close vicinity thereof, as well as the data of the maximum permissible towing line tension, relevant vertical and horizontal angles to determine the towing line position according to the calculations made for each loading condition. The above

information may be duplicated at ship steering position.

13.3.8.4 Controls (handles, buttons, etc.) for emergency disconnecting shall be protected against unintentional action of the personnel.

13.3.9 Bollard pull testing.

13.3.9.1 The following shall subject to testing for bollard pull measurement:

.1 the first ship out of the series, then every fifth ship of the series (i.e. sixth, eleventh, etc.) provided the propulsion plant is identical;

.2 every ship of non-series construction.

13.3.9.2 Prior to bollard pull tests, the test program, approved Stability Booklet, as well as the results of design assessment of bollard pull shall be submitted to the Register.

13.3.9.3 During the stationary pull tests the main engine(s) shall be operated at maximum torque corresponding to the maximum free running condition.

Actual output shall be checked during the testing.

13.3.9.4 During the normal operation of the ship, all auxiliary equipment, such as pumps, generators and other equipment driven by the main engine(s) or propeller shaft(s) shall be connected while testing.

13.3.9.5 Towing line measured between the ship's stern and the mooring bollard shall be at least 300 m in length. When the above towing line length may not be provided in the test place, the towing line length equal to at least two ship's length may be accepted.

13.3.9.6 At least 20 m depth shall be provided at the test place within a radius of 100 m around the ship. When 20 m depth may not be provided at the test place, the maximum depth equal to twice maximum ship's draught may be accepted.

13.3.9.7 The test shall be carried out with the ship's displacement corresponding to full ballast condition and half fuel capacity.

13.3.9.8 During the tests the ship shall be trimmed on an even keel or shall have a trim by stern not exceeding 2 per cent of the ship's length.

13.3.9.9 The tests shall be conducted at wind velocity not exceeding 5 m/s. Current speed at the test place shall not exceed 0,5 m/s in any direction.

13.3.9.10 The ship shall demonstrate the ability to keep to the heading set for at least 10 min developing power at the conditions specified in **13.3.9.3**. The verified continuous bollard pull is the mean value of readings for 10-minute period.

13.3.9.11 Load cell that used during the tests shall be calibrated in the presence of the RS representative. The load cell error shall be at least $\pm 2\%$ at the temperature and range of loads applicable to the testing conditions.

13.3.9.12 An instrument for the continuous readout and a recording device for registration of bollard pull in graph form as function on time shall be both connected to the load cell.

Where practicable, both devices shall be located and continuously monitored from the shore.

13.3.9.13 The load cell shall be placed between the eye splice of the towing line and the bollard.

13.3.9.14 The towing line position during the tests shall have the minimum affect on the measuring results due to its friction with the towing arrangement components.

13.3.9.15 For the testing period, the communication system shall be installed between the ship and ashore personnel performing the continuous monitoring of the loading cell and the recording device ashore using VHF-communication or telephone.

13.3.10 Records.

13.3.10.1 Bollard pull testing report.

13.3.10.2 Report on Survey of the Ship (form 6.3.10).

13.3.10.3 Based on results of the bollard pull testing, the following entry shall be introduced in the Classification Certificate (form 3.1.2) in the Section "Other Characteristics": "Permanent static towing pull at the maximum free running condition of the propulsion plant...kW is...t".

13.3.10.4 Upon the shipowner's request, Bollard Pull Certificate (form 6.3.45) may be issued for a ship with the descriptive notation **Anchor handling vessel** or **Anchor handling vessel, Tug**.

14 REQUIREMENTS FOR SHIPS PREPARED FOR CONVERSION FOR THE USE OF GAS FUEL

14.1 GENERAL PROVISIONS AND APPLICATION

The requirements of this Section apply to ships prepared for conversion for the use of gas fuel. A distinguishing mark **GRS** (Gas Ready Ship) may be assigned to ships other than LNG gas carriers with the developed design aspects required to prepare the ship for the use of gas fuel.

Ship conversion project to be developed for assigning the ship the distinguishing mark **GRS** shall be aimed at reduction of expenses while converting the ship for the use of gas fuel, minimizing of hull works, maintenance of the existing hull structures and machinery to the maximum extent.

By the date of assignment the distinguishing mark **GRS**, the ship shall use only liquid fuel with the flashpoint above 60°C, and the ship shall be prepared for conversion for the use of gas fuel. Where conversion is over, such ship shall meet the requirements of the International Code for Safety for Ships Using Gases or Other Low Flashpoint Fuels (IGF Code) and the requirements specified in Section 9 of this Part.

Upon completion of the ship conversion for the use of gas fuel, the ship shall be assigned the distinguishing mark **GFS**, therewith the distinguishing mark **GRS** shall be withdrawn.

14.2 DISTINGUISHING MARKS IN THE CLASS NOTATION

14.2.1 Ships prepared for the use of gas fuel in compliance with this Section shall be assigned with the distinguishing mark **GRS** added to the character of classification. Minimum extent of the requirements to be complied with for assigning the distinguishing mark **GRS** are related to design only and are specified in 14.5.

14.2.2 Apart from the distinguishing mark **GRS**, distinguishing marks specifying the ship's readiness for conversion to use gas fuel are provided when the following additional requirements, other than those specified in 14.5, are complied with on board the ship:

GRS-D — design of ship conversion is approved by the Register and the requirements specified in 14.6 are complied with on board the ship;

GRS-H — necessary hull reinforcements have been provided during the ship construction in the areas of GFST and other additional equipment installation in the extent specified in 14.7;

GRS-T — LNG tank has been installed on board during the ship construction and the requirements specified in 14.8 are complied with;

GRS-P — gas fuel piping and other special systems are installed on the ship and the requirements specified in 14.9 are complied with;

GRS-E — gas fuel consumers installed on board the ship are dual fuel and the requirements specified in 14.10 are complied with.

Where the appropriate requirements are complied with, a number of distinguishing marks, e.g. **GRS-D-H-T**, may be also assigned simultaneously in addition to the distinguishing mark **GRS**.

14.3 TERMS AND DEFINITIONS

In addition to the definitions specified in Section 9 of this Part and 1.2, Part I "Classification" of the Rules for the Classification and Construction for Ships Carrying Liquefied Gases in Bulk, the following definition has been adopted.

Conversion means re-equipment of a ship not initially intended for the use of gas fuel in order to comply with the requirements of the IGF Code being in force at the date of conversion.

14.4 TECHNICAL DOCUMENTATION

In addition to technical documentation specified in Section 3 "Technical Documentation", the documentation listed in 9.1.4 for ships with the distinguishing mark **GFS** (Gas Fuelled Ship) shall be submitted to the Register.

Additionally, information related to the ship's conversion shall be submitted in the technical background or any other document indicating at least the following:

general ship's data after conversion;

components of systems and machinery required for the use of gas fuel to be installed during the ship's conversion;

components of systems and machinery required for the use of gas fuel to be installed during the ship's construction;

drawings of hull structures with necessary calculations that may be changed during the ship's conversion;

drawings of hull structures and foundations required for machinery subject to installation during the ship's conversion.

14.5 MINIMUM REQUIREMENTS FOR SHIPS WITH THE DISTINGUISHING MARK GRS IN THE CLASS NOTATION

.1 conversion design shall be approved for the ship to comply with the IGF Code requirements and RS Rules for ships with the distinguishing mark GFS. The design shall include approval of the technical documentation for GFST;

.2 area for installation of GFST shall be provided on board the ship according to 9.2.2. In case of an enclosed space, the design of systems to ensure explosion safety (ventilation, gas leaks control etc.) shall be provided;

.3 GFSTs shall be taken into account in the stability calculations;

.4 necessary calculations of hull reinforcements for GFST installation and fuel preparation shall be made;

.5 ship engine shall permit conversion to gas fuel. Gas fuelled engine shall be type approved.

14.6 REQUIREMENTS FOR SHIPS WITH THE DISTINGUISHING MARK GRS-D IN THE CLASS NOTATION

.1 requirements of 14.5 shall be complied with;

.2 requirements of 9.2 shall be complied with at the extent allowing conversion without replanning of ship's spaces;

.3 requirements of 9.7.2 shall be complied with to the extent allowing the ship's conversion without changing the fire integrity class of hull structures;

.4 pump capacity of water fire main system shall comply with the requirements of 9.7.3 and 9.7.4;

.5 ventilation system shall comply with the requirements of 9.8.1 — 9.8.5;

.6 bilge system shall comply with the requirements of 9.2.5;

.7 electrical equipment shall comply with the requirements of 9.11.

14.7 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK GRS-H IN THE CLASS NOTATION

.1 requirements of 14.6 for ships with distinguishing mark GRS-D in the class notation shall be complied with;

.2 necessary hull reinforcements shall be made in the areas of GFST installation and other additional equipment required for the use of gas fuel. Hull reinforcements, supports and foundations shall be calculated for the loads specified in 6.4.4 of the IGF Code.

14.8 REQUIREMENTS FOR SHIPS WITH DISTINGUISHING MARK GRS-T IN THE CLASS NOTATION

.1 requirements of 14.7 for ships with distinguishing mark GRS-H in the class notation shall be complied with;

.2 GFST complying with the requirements of 9.3 is installed on board the ship;

.3 Filling and vent pipes from relief valves shall be installed on board the ship. Prior to conversion, the piping may be stored disassembled on board the ship.

14.9 REQUIREMENTS FOR SHIPS WITH THE DISTINGUISHING MARK GRS-P IN THE CLASS NOTATION

.1 requirements of 14.6 for ships with distinguishing mark GRS-D shall be complied with;

.2 gas fuel piping and other special systems are installed on board the ship and the requirements specified in 9.4, 9.5 and 9.8 are complied with.

14.10 REQUIREMENTS FOR SHIPS WITH THE DISTINGUISHING MARK GRS-E IN THE CLASS NOTATION

.1 requirements of 14.6 for ships with distinguishing mark GRS-D in the class notation;

.2 all gas fuel consumers shall be installed on board the ship and comply with the requirements of 9.6;

.3 control, alarm and automation systems shall comply with the requirements of 9.10 and 9.7.6.

APPENDIX

ICE CLASS DRAUGHT MARKING

Subject to 10.3.2, the ship's sides shall be provided with a warning triangle and with a draught mark at the maximum permissible ice class draught amidships (refer to Fig.). The purpose of the warning triangle is to provide information on the draught limitation of the vessel when it is sailing in ice for masters of icebreakers and for inspection personnel in ports.

Notes: 1. The upper edge of the warning triangle shall be located vertically above the "ICE" mark, 1000 mm higher than the summer load line in fresh water but in no case higher than the deck line. The sides of the triangle shall be 300 mm in length.

2. The ice class draught mark shall be located 540 mm abaft the centre of the load line ring or 540 mm abaft the vertical line of the timber load line mark, if applicable.

3. The marks and figures shall be cut out of 5 — 8 mm plate and then welded to the ship's side. The marks and figures shall be painted in a red or yellow reflecting colour in order to make the marks and figures plainly visible even in ice conditions.

4. The dimensions of all letters shall be the same as those used in the summer load line mark.

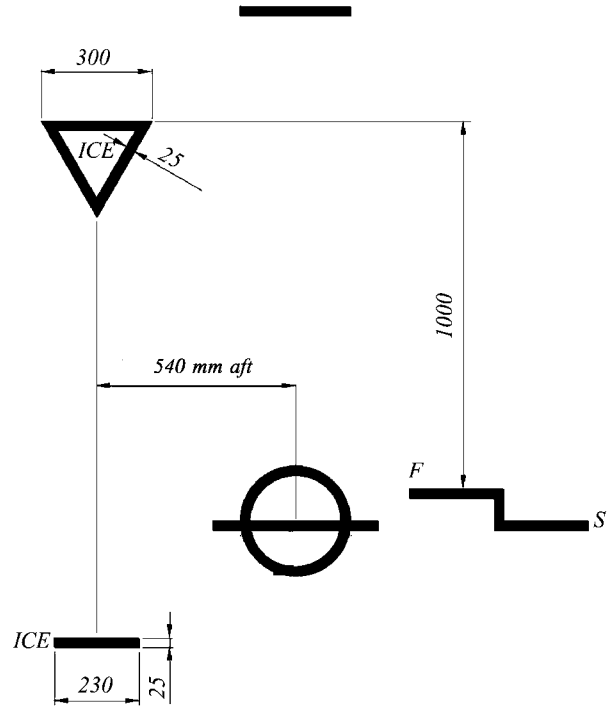


Fig. Ice class draught marking

**LIST OF CIRCULAR LETTERS AMENDING/SUPPLEMENTING NORMATIVE
DOCUMENT**

(Normative document No. and title)

Item No.	Circular Letter No., date of approval	List of amended and introduced paras / chapters / sections



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 314-26-1047c

dated 12.10.2017

Re:

requirements for ships which are periodically grounded in operation (NAABSA ships)

Item of technical supervision:

sea-going ships under construction and in service

Implementation: from the date of signing

Valid: till -

Validity period extended till -

Cancels / amends / supplements Circular Letter No. - - dated -

Number of pages: 1+14

Appendices: amendments to the Rules for the Classification and Construction of Sea-Going Ships, 2017, ND No. 2-020101-095-E

Director General


K.G. Palnikov

Amends Rules for the Classification and Construction of Sea-Going Ships, 2017, ND No. 2-020101-095-E

We hereby inform that Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Sea-Going Ships, 2017, ND No. 2-020101-095-E will be amended with the requirements for ships which are periodically grounded in operation (**NAABSA** ships).

It is necessary to do the following:

- 1) Familiarize the surveyors of the RS Branch Offices and interested organizations in the area of the RS Branch Offices' activity with the content of the Circular Letter.
- 2) Apply provisions of the Circular Letter during the RS practical activity.

Person in charge: D.A. Aleksashin
17-264639 dated
"Thesis" System: 03.10.2017

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PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

New **Section 11** shall be introduced reading as follows:

11 REQUIREMENTS FOR SHIPS NOT ALWAYS AFLOAT BUT SAFELY AGROUND (NAABSA SHIPS)

11.1 GENERAL

11.1.1 Application.

11.1.1.1 The requirements of this Section apply to NAABSA ships (Not Always Afloat But Safely Aground) which may lie aground in safety with partial or full hull baring in places fit for grounding the ships.

11.1.1.2 At the shipowner's request, one of the following distinguishing marks may be added to the character of classification of a ship complying with the requirements of this Section:

.1 NAABSA1 – partial or full ship hull baring is permitted on plane homogeneous sand-and-shingle or sand-and-mud sea beds with no motion in calm water as harbours or sheltered areas.

.2 NAABSA2 – in addition to NAABSA1 notation specified, motion and ship bow impact contact with sea bed at defined wave parameters are permitted.

.3 NAABSA3 – in addition to NAABSA2 notation, hull baring of moored ship is permitted at specified distance from seashore line in rolling conditions with impact contact against the seabed in any point of the seabed.

11.2 REQUIREMENTS FOR HULL STRUCTURE

11.2.1 Requirements for hull structures specified in this Section are in addition to the requirements of Part II "Hull".

11.2.2 Symbols.

The following symbols have been adopted in this Chapter:

Δ_N = design displacement of NAABSA ship equal to the maximum value at the beginning of baring or upon emersion from the ground, but in all cases not more than summer load line displacement, in t;

L_{BN} = design length of ship's bottom along the keel line, in m;

L_N = design length of bottom, in m, considering the bow (1) and stern (2) external structural strengthening of hull (refer to Fig. 11.2.2.1);

Δd = change of midship mean draft relative to level d_N corresponding to design displacement Δ_N , in m;

ψ_0 = design trim angle of the ship, in deg. (positive nose-up trim);
 ψ_N = design sea bed slope angle along the ship, in deg.;
 ψ_S = operating trim angle of the ship, in deg.;
 ψ_{ON} = ship trim angle due to grounding on the move, in deg.;
 R_{ON} = initial bow response to ship grounding on the move, in kN;
 R_N^m = static end (local) response for the ship, in kN;
 R_N^n = static nominal (distributed) response for the ship, in kN;
 M_N = ship hull bending moment considering the sea bed response, in kN·m;
 N_N = ship hull shear force considering the sea bed response, in kN;
 B_N = width of flat horizontal section of the bottom, in m;
 β_k = deadrise angle, in deg.;
 h_k = design height of external structural protection below the keel line, in m;
 v_N = design forward speed of ship upon grounding, in knots;
 h_N = design (allowable) wave height for NAABSA conditions, in m.

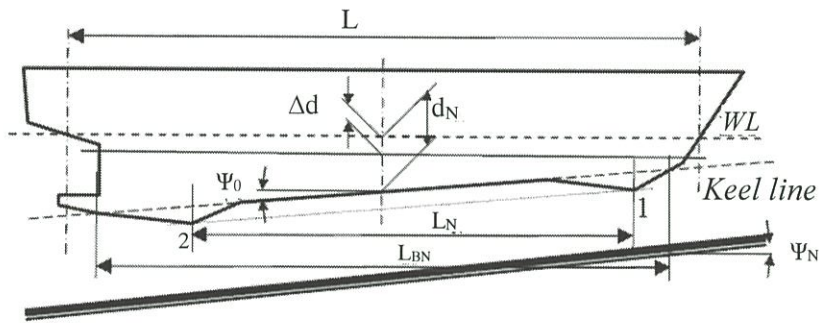


Fig. 11.2.2.1

In Fig. 11.2.2.1, the draft corresponding to design displacement is shown with a dotted line and the draft at hull baring is shown with a solid line.

11.2.3 Requirements for hull shape.

11.2.3.1 For typical transverse sections of NAABSA ships are specified in Fig. 11.2.3.1. In the area of impact contact with sea bed it is recommended to reduce the width of the flat horizontal part of the bottom and to increase the deadrise angle.

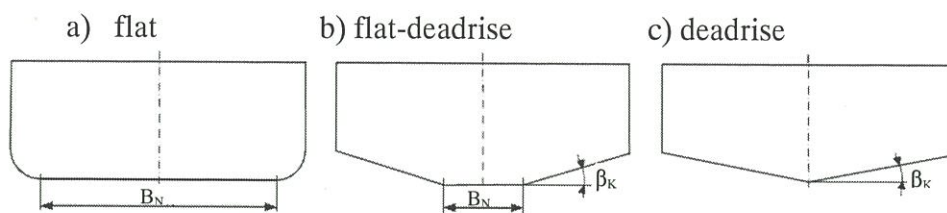


Fig.11.2.3.1

11.2.4 Strengthened areas.

11.2.4.1 The strengthened bottom area over the hull length of **NAABSA** ships is divided into the following:

fore area – A ;

midship area – B ; and

aft area – C .

11.2.4.2 The length of strengthened bottom areas of **NAABSA** ships is defined according to Fig. 11.2.4.2

The aft boundary of the fore area is located at a distance L_A , in m, from the fore perpendicular equal to:

$$L_A = 0,3L(1 + 0.175\psi_0) - 20h_k \geq 2L_3, \text{ but not more than } 0,3L \quad (11.2.4.2-1)$$

where L_3 = distance between point 3 (refer to Fig. 11.2.4.2) and fore perpendicular, in m;

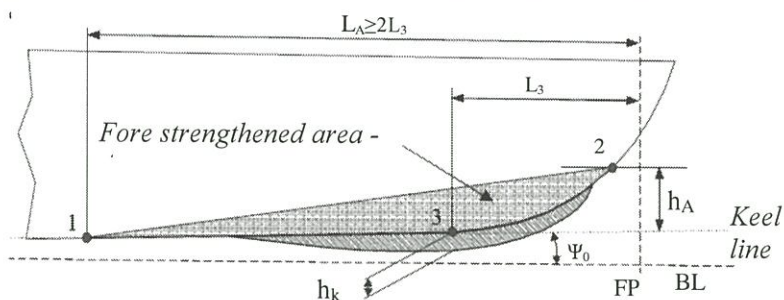
h_k = design height of external structural protection below the keel line, in m.

The forward boundary of the aft area is located at a distance L_C , in m, from the aft perpendicular equal to:

$$L_C = 0,3L(1 - 0.175\psi_0) - 20h_k \geq 0.05L, \text{ but not more than } 0,3L \quad (11.2.4.2-2)$$

If the engine room is located in the aft of the ship, such an engine room shall be attributed to the strengthened area C .

The midship strengthened area B is located between fore and aft areas.



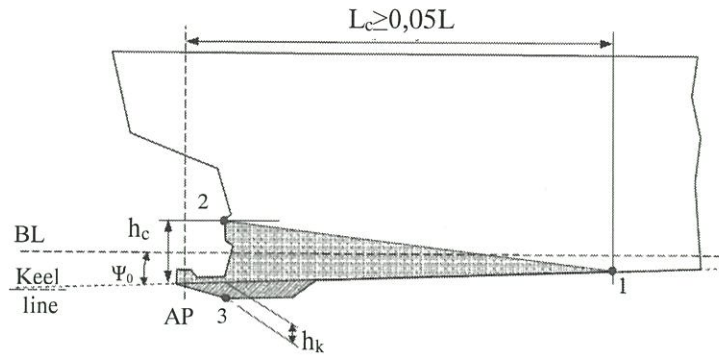


Fig. 11.2.4.2

1 – point of distance from perpendicular; 2 – upper boundary;

3 – point to determine the height of external structural protection

A distance between the upper boundary of the fore strengthened area and the keel line (refer to point 2 in Fig. 11.2.4.2) h_A , in m, is determined by the following formula:

$$h_A = 0,1\psi L - h_K \quad (11.2.4.2-3)$$

where ψ = design trim angle at rolling in the place of grounding, in rad; if no exact data is available, ψ is determined by Formula (1.3.3.1-4), Part II "Hull" as for a ship operating in restricted area of navigation **R3**.

A distance between the upper boundary of the aft strengthened area and the keel line (refer to point 2 in Fig. 11.2.4.2) h_C , in m, is determined by the following formula:

$$h_C = \frac{0,2\psi L}{3} - h_K \quad (11.2.4.2-4)$$

A distance between the upper boundary of the midship strengthened area and the keel line h_B , in m, is determined by the formula:

$$h_C = (0,5B - B_K) \cdot \tan \theta - h_K \leq h_{AN} \quad (11.2.4.2-5)$$

where B_K = distance from CL to the nearest false keel side, in m;

h_{AN} = height to top of floors in case of curved lines and up to the lift point of bottom in case of simplified lines, in m;

θ = design heel angle at rolling in the place of grounding, in rad; if no exact data is available, θ is determined by Formula (1.3.3.1-5), Part II "Hull" as for a ship operating in restricted area of navigation **R3** at $\varphi_r = \varphi$.

11.2.5 Design.

11.2.5.1 For ships with the distinguishing mark **NAABSA2**, the double bottom is required to be fitted in the fore strengthened area. For ships with the distinguishing mark **NAABSA3**, the double bottom is required to be fitted extending along the entire length of the ship – from forepeak to afterpeak bulkhead.

11.2.5.2 For transverse framing system, the flooring shall be installed on each frame. For longitudinal framing system of bottom on ships with **NAABSA2** and **NAABSA3** marks, the flooring shall be installed at two frame spacing intervals.

11.2.5.3 A distance a_{BS} , in m, between bottom stringers, stringer and keel shall not exceed

$$a_{BS} = 1,4 + \frac{2,5L}{100} - \left(\frac{L}{100}\right)^2, \quad (11.2.5.3)$$

but not more than:

1,1 m – in strengthened area *A* for ships with the distinguishing mark **NAABSA2** and strengthened areas *A* and *C* for ships with the distinguishing mark **NAABSA3**;

2,2 m – in strengthened area *B* for ships with the distinguishing mark **NAABSA3**.

11.2.5.4 For the upper deck of **NAABSA** ships over 50 m long, the longitudinal framing system in the midship hull area is recommended.

11.2.5.5 Web frames and/or double side diaphragms shall be installed at least 4 frame spacing apart.

11.2.5.6 Plane longitudinal and transverse bulkheads shall be reinforced with vertical stiffeners. Corrugations of corrugated bulkheads shall be vertical.

11.2.5.7 False keels with different cross-section shapes arranged in different places under the bottom (refer to Fig. 11.2.5.7) can be used as external structural protection of **NAABSA** ships. Installed false keels shall be arranged in the plane of longitudinal bulkheads or bottom stringers. False keels shall be fastened to external shell plating by means of an intermediate member, i.e a flat bar welded to the shell plating with an all-round continuous fillet weld. Connection of false keels to intermediate member shall comply with the requirements of 2.2.5.3, Part II "Hull". False keels shall terminate in the stiffened areas of shell plating and shall be gradually tapered at ends in height and width.

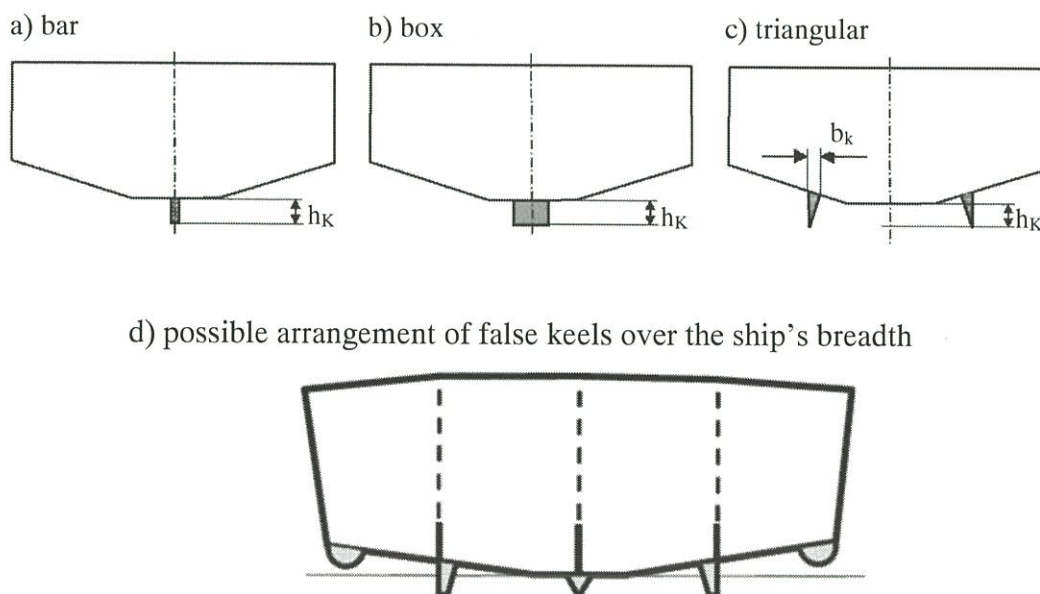


Fig. 11.2.5.7

11.2.5.8 For the longitudinal framing system of bottom on ships with the distinguishing marks **NAABSA2** or **NAABSA3**, the dock and bilge brackets shall be placed at each frame. It is recommended to install lightened dock and bilge brackets between the frames.

11.2.5.9 Support sections of beams.

For designing framing beams by allowable stresses, the support sections and design spans shall be determined according to 1.6.3.1, Part II "Hull".

For designing framing beams by limit state, the support section shall be taken considering availability of brackets and arranged as follows:

at the end of brackets with a free edge stiffened with a face plate;

in the middle of bracket side with unstiffened free edge.

11.2.5.10 Connections of beams shall comply with the requirements of 1.7.2, Part II "Hull". For areas of impact loads on ships with the distinguishing marks **NAABSA2** and **NAABSA3**, it is not recommended to use beam connections with technological gaps.

11.2.5.11 Holes in bottom framing webs.

11.2.5.11.1 Holes in bottom framing webs shall comply with the requirements specified in 2.3.5.2 and 2.4.2.7 of Part II "Hull".

11.2.5.12.2 Holes in primary framing webs for bottom beams in the areas where the bottom contacts the seabed shall be compensated by installation of fixings similar to the intersections specified in Table 3.10.2.4.5 of Part II "Hull". In the areas of impact loads it is recommended to use fixings with edges welded to shell.

11.2.6 Design loads.

11.2.6.1 Design local pressures p_i , in kPa, on the structural members immediately perceiving the seabed are determined by the formula

$$p_i = 10d_N(1 + 4/\sqrt{A_i}) \quad (11.2.6.1)$$

where

d_N = refer to 11.2.2;

A_i = calculated area of the member strain zone, in m^2 .

11.2.6.2 The required total area of contact with the seabed in case of full ship hull baring A_N^{min} , in m^2 , shall be at least

$$A_N^{min} = g\Delta_N/R_0 \quad (11.2.6.2-1)$$

where R_0 = design nominal resistance of ground, in kPa, at least

$$R_0 > 10 \Delta d. \quad (11.2.6.2-2)$$

For **NAABSA** ships, which are loaded/unloaded when grounded in safe mode with use of heavy wheeled and tracked vehicles:

$$R_0 = 100.$$

11.2.6.3 Design static load Q_{OS} , in kN, from the ground to check transverse strength of **NAABSA** ship hull compartment (refer to 11.2.8.11) is determined by the formula

$$Q_{OS} = k_\varphi R_N^n \frac{L_{OS}}{L_{BN}} \quad (11.2.6.3-1)$$

where $k_\varphi = 1,5$ – with no design-based justifications;

L_{OS} = length of ship compartment/hold, in m;

R_N^n = static response in case of ship hull baring, in kN.

For partial baring conditions:

$$R_N^n = g\Delta_N \frac{\Delta d}{d_N} \frac{\alpha}{c_b}. \quad (11.2.6.3-2)$$

For full baring conditions:

$$R_N^n = g\Delta_N \quad (11.2.6.3-3)$$

where α = waterplane area coefficient for summer load waterline.

For the recommended diagrams of design load application to ship compartments are specified in Fig. 11.2.6.3.

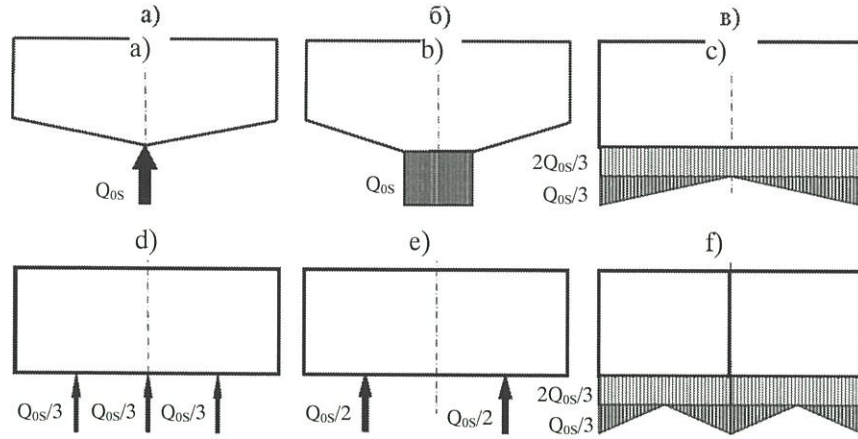


Fig. 11.2.6.3:

a – deadrise; *b* – flat-deadrise; *c* – flat; *d* – with three false keels;

e – with two false keels; *f* – flat with one longitudinal bulkhead at *CL*

If no calculations of ship baring and emersion processes are available, static end response of the ground R_N^m to ship hull, in kN, is determined by the following formula:

$$R_N^m = g\Delta_N \left[\frac{tg(\psi_N - \psi_0 - \psi_S - \psi_{ON})}{6} \frac{L}{d_N} \right] + R_{ON} \quad (11.2.6.3-4)$$

For **NAABSA1** ships $R_{ON} = 0$ and $\psi_{ON} = 0$ shall be taken.

In any case for full hull baring conditions the value of static end response of the ground R_N^m , in kN, shall be at least

$R_N^m = 3g\Delta_N/12$ – for ship with the distinguishing mark **NAABSA1**;

$R_N^m = 4g\Delta_N/12$ – for ships with the distinguishing mark **NAABSA2**;

$R_N^m = 5g\Delta_N/12$ – for ships with the distinguishing mark **NAABSA3**.

11.2.6.4 Bending moments and shear forces for hull.

11.2.6.4.1 Bending moments and shear forces for hull of a ship which is periodically grounded in operation shall be determined for ships with the distinguishing mark **NAABSA1** and length over 50 m and for ships with the distinguishing mark **NAABSA2** and **NAABSA3** irrespective of the ship's length.

11.2.6.4.2 The values of maximum bending moments, in kNm, and shear forces, in kN, can be determined by approximation formulae specified in 11.2.6.4.3 – 11.2.6.4.6.

11.2.6.4.3 For full hull baring when aground and hull hogging of **NAABSA** ships of all levels:

$$M_N = 0,315\Delta_N L; \quad (11.2.6.4.3-1)$$

$$N_N = -1,03\Delta_N \quad (11.2.6.4.3-2)$$

For partial hull baring of **NAABSA1** ships, the obtained values can be reduced by replacing Δ_N with the nominal response of the ground R_N^n , but not more than twice.

11.2.6.4.4 In case of action of end force and hull sagging of ships with the distinguishing mark **NAABSA1**:

$$M_N = -0,363\Delta_N L; \quad (11.2.6.4.4-1)$$

$$N_N = 2,45\Delta_N. \quad (11.2.6.4.4-2)$$

11.2.6.4.5 In case of action of end force, including bow impact of ships with the distinguishing mark **NAABSA2**:

$$M_N = -0,629\Delta_N L; \quad (11.2.6.4.5-1)$$

$$N_N = 3,27\Delta_N. \quad (11.2.6.4.5-2)$$

11.2.6.4.6 In case of action of end force, including bow or stern impact of ships with the distinguishing mark **NAABSA3**:

$$M_N = -0,921\Delta_N L; \quad (11.2.6.4.6-1)$$

$$N_N = 4,09\Delta_N. \quad (11.2.6.4.6-2)$$

11.2.6.4.7 The formulae specified in 11.2.6.4.3 – 11.2.6.4.6 determine maximum values of bending moments in the midship area of the hull and shear forces on the bow and stern. In case of sagging due to end forces, including impacts forces, the obtained values shall be summed up algebraically with design bending moments for the ship in still water.

11.2.7 Ultimate section modulus of a ship's hull cross section.

Ultimate section modulus of hull cross section for **NAABSA** ships by the end of service life shall be not less than permissible residual ultimate section modulus of hull cross section $W_{LM(bot)}$, in cm^3 , determined by the formula:

$$W_{LM(bot)} = 1,1 \cdot \frac{|0,92M_N + M_{SW}|}{R_{eH}} \cdot 10^3 \quad (11.2.7)$$

where M_N = design bending moment according to 11.2.6.4, in kNm ;

M_{SW} = design bending moment in case of ship sagging in still water, in kNm ;

R_{eH} = upper yield stress of deck (bottom) material.

When determining ultimate section modulus of hull cross section of **NAABSA** ships by the end of service life, the following shall be taken into account:

wear of structural members is 30 %;

deformations of bottom structures breadthwise in design section are 50 % of the permissible values;
compressed flexible braces of the deck and upper part of sides are not allowed;
tension braces of the bottom with deformations are not allowed.

11.2.8 Dimensions of structural members.

11.2.8.1 Thickness of the bottom and bilge plating s , in mm, in the strengthened bottom area of NAABSA ships shall be at least:

$$s = 15,8ak_{\alpha}\sqrt{\frac{k_p p}{k_{\sigma} R_{eH}}} \cdot m_n^{-1} \quad (11.2.8.1)$$

where a = dimension of the smaller side of the panel, in m;

b = dimension of the larger side of the panel, in m;

$$k_{\alpha} = \frac{1-\alpha+\frac{\pi\alpha}{6}}{1-\alpha+\frac{\pi\alpha}{2}} - \text{ratio of panel sides};$$

$$\alpha = \frac{a}{b};$$

k_p – safety factor taken equal to:

$k_p = 1,5$ in case of no external structural protection in the area concerned;

$k_p = 1,0$ if external structural protection is available in the area concerned;

p – design pressure of seabed, in kPa, according to 11.2.6.1 at $A_i = a \times b$;

k_{σ} – factor of allowable stresses taken equal to:

$k_{\sigma} = 0,95 - \frac{0,42L}{100}$ in case of transverse framing system in the midship strengthened area;

$k_{\sigma} = 0,9$ – in other cases;

R_{eH} = upper yield stress, in MPa;

m_n = coefficient taken equal to:

$m_n = 0,75$ – in case of no external structural protection in the area concerned;

$m_n = 0,65$ – if external structural protection is available in the concerned area.

11.2.8.2 In the area of impact loads with no external structural protection in the area concerned the thickness of the bottom and bilge plating of ships with the distinguishing marks **NAABSA2** and **NAABSA3** shall be at least:

$$s = \frac{10,6}{R_{eH}} \cdot p \cdot b \quad (11.2.8.2)$$

where R_{eH} = upper yield stress, in MPa;

p = design pressure of seabed, in kPa, according to 11.2.6.1 at $A_i = a \times b$;

b = dimension of the larger side of the panel, in m.

11.2.8.3 In all cases the thickness of the bottom and bilge plating shall be not less than that specified in 2.2.4.8, Part II "Hull".

11.2.8.4 Ultimate section modulus W_0 , in cm^3 , of cross section of primary members in the strengthened bottom area of **NAABSA** ships shall be at least:

$$W_0 = \frac{1000k_p p a l^2}{m k_\sigma R_{eH}} \cdot k_\alpha \cdot k_k \cdot m_n^{-1} \quad (11.2.8.4)$$

where a = distance between primary members;

l = span length, in m;

$$k_\alpha = 1 - \frac{\alpha^2}{2} + \frac{\alpha^3}{8};$$

$$\alpha = \frac{a}{l};$$

p = design pressure of seabed, in kPa, according to 11.2.6.1 at $A_i = 2a \times l$;

$k_k = 0,914$ – load distribution coefficient;

$m_n = 0,75$ – in case of no external structural protection in the area concerned;

$m_n = 0,65$ – if external structural protection is available in the area concerned;

$m = 12$ – bending moment coefficient;

$k_\sigma = 0,95 - \frac{0,42L}{100}$ – for bottom longitudinal girders in the midship strengthened area;

$k_\sigma = 0,9$ – in other cases;

R_{eH} – upper yield stress, in MPa;

$k_p = 1,35$ in case of no external structural protection in the area concerned;

$k_p = 1,0$ if external structural protection is available in the area concerned;

11.2.8.5 Actual section modulus of girder section is determined according to 3.10.4.2.6, Part II "Hull".

11.2.8.6 The beam web area in the strengthened bottom area of **NAABSA** ships f_c , in cm^2 , shall be not less than the value determined by the formula

$$f_c = \frac{5k_p p a l \left(1 - \frac{\alpha}{2}\right)}{0,57m_n k_\sigma R_{eH}} \quad (11.2.8.6)$$

where $k_p = 1,35$ in case of no external structural protection in the area concerned;

$k_p = 1,0$ if external structural protection is available in the area concerned;

a = distance between primary members;

l – span length, in m;

$$\alpha = \frac{a}{l};$$

p = design pressure of seabed, in kPa, according to 11.2.6.1 at $A_i = 2a \times l$;

$k_k = 0,914$ – load distribution coefficient;

$m_n = 0,75$ – in case of no external structural protection in the area concerned;

$m_n = 0,65$ – if external structural protection is available in the area concerned;

$k_\sigma = 0,95 - \frac{0,42L}{100}$ for longitudinal beams of bottom framing in the midship strengthened area;

$k_\sigma = 0,9$ – in other cases;

R_{eH} – upper yield stress, in MPa.

11.2.8.7 Actual area of web is determined according to 3.10.4.2.5, Part II "Hull".

11.2.8.8 Scantlings of floors, centre girder and bottom stringers shall be selected proceeding from the calculation of bottom grillage, using beam model. Design static loads on bottom grillage are determined according to 11.2.6.3. It is recommended to take into account the effect of brackets. If pillars are available, the interaction of bottom grillage with superstructures shall be considered.

Reduced stresses (by von Mises criterion) obtained by results of calculation shall not exceed:

$0,75 \cdot \left(0,95 - \frac{0,42L}{100}\right) \cdot R_{eH}$ – for longitudinal framing in the strengthened area B ;

$0,68 \cdot R_{eH}$ – in all other cases.

11.2.8.9 Dimensions of pillars and struts shall be not less than the those specified in 2.9, Part II "Hull". Compression loads shall be determined by calculation using beam model.

11.2.8.10 The web thickness of floors, bottom stringers, centre girder, bilge brackets and plates of transverse and longitudinal bulkheads adjoining the shell in the strengthened bottom area of **NAABSA** ships shall be not less than that specified in 2.2.4.9, Part II "Hull" where external structural protection is available in the area concerned and 2.4.4.3.2, Part II "Hull" where there is no external structural protection.

11.2.8.11 The webs of floors, bottom stringers, centre girder, bilge brackets and plates of transverse and longitudinal bulkheads adjoining the shell in strengthened bottom area of **NAABSA** ships shall be reinforced with stiffeners. The distance between stiffeners shall not exceed the distance between the bottom longitudinals in the area concerned. Stability of stiffeners shall be ensured in worn-out state at the end of structure service life.

11.2.8.12 The web thickness of floors, bottom stringers, centre girder, as well as bilge brackets and plates of transverse and longitudinal bulkheads adjoining the shell in strengthened bottom area of **NAABSA** ships shall be not less than that specified in 3.10.4.9.2, Part II "Hull". Design pressures shall be not less than those determined by the formula

$$p = 10d_N \cdot \left(1 + 4/\sqrt{A_i}\right) \cdot k_p$$

where d_N = refer to 11.2.2;

A_i = calculated area of the member strain zone, in m^2 ;

$k_p = 1,5$ – safety factor;

11.2.8.13 Stems.

11.2.8.13.1 Stem construction shall comply with the requirements of 2.9, Part II "Hull".

11.2.8.13.2 The lower part of the stem on **NAABSA** ships at the transition area to keel shall protrude beyond the shell surface or shall be made as an outboard bar.

11.2.8.13.3 The approved cross section dimensions of the stem shall be checked based on the calculation of the curvilinear variable section beam, which rests on decks, platforms and transverse bulkheads. Design load shall be not less than the response of the seabed R_N^m according to 11.2.6 distributed as a triangle along the length L_3 (refer to 11.2.4.2); coefficient of allowable stresses shall be taken equal to $k_\sigma = 0,68$.

11.2.8.13.4 The lower part of the sternframe on **NAABSA** ships at the transition area to keel shall protrude beyond the shell surface or shall be made as an outboard bar.

11.2.8.13.5 The approved dimensions of sternframe members shall be checked based on the direct strength calculation taking the coefficient of allowable stresses $k_\sigma = 0,68$ and design end loads according to 11.2.6. If the solepiece is lifted in the stern direction at an angle of not less than 6° for ships with the distinguishing mark **NAABSA1**, 8° for ships with the distinguishing mark **NAABSA2** and 10° for ships with the distinguishing mark **NAABSA3**, the load is considered distributed in the form of a triangle, in other cases the load is evenly distributed.

11.3 EQUIPMENT, ARRANGEMENTS AND OUTFIT

The **NAABSA** ships shall have at least one embarkation ladder on each side. The length of such embarkation ladders shall equal the distance from the upper deck to the seabed to provide safe transfer of the crew. The design of embarkation ladders shall comply with the requirements of 6.20.7, Part II "Life-Saving Appliances" of the Rules for the Equipment of Sea-Going Ships.

11.4 STABILITY AND SUBDIVISION

11.4.1 The requirements of this Section are in addition to the requirements of Part IV "Stability" and Part V "Subdivision".

11.4.2 For the purpose of this Chapter the following symbols have been adopted:

L_l – ship's length as determined in the Load Line Rules for Sea-Going Ships;

B – ship's breadth.

11.4.3 The Stability Booklet shall include the following:

.1 it shall be specified that in case of grounding and emersion the ship shall be trimmed in way to have the bottom plane parallel to the ground plane in the place of grounding;

.2 it shall be specified that during loading/unloading operations aground, the changes in ship load shall be strictly weighed. If the exact data on the height of the center of gravity is not available, the height of center of gravity shall be taken equal to the upper dimensional limit;

.3 it shall be specified that prior to emersion, the ship trim and stability afloat shall be estimated to confirm that the ship complies with all applicable requirements for stability and that the load line draught is not exceeded.

11.4.4 Under all loading conditions to be encountered in service (icing disregarded), the trim and stability of an intact ship shall be sufficient to meet the requirements of 3.3 and 3.4, Part V "Subdivision" after obtaining the following bottom damages located anywhere in the ship length:

.1 longitudinal extent – $\frac{1}{3}L_1^{2/3}$ or 14,5 m (whichever is less);

.2 transverse extent – $B/6$ or 10 m (whichever is less);

.3 vertical extent – $B/20$ or 2 m (whichever is less).



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 313-10-1077c

dated 21.12.2017

Re:

amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Ships, 2018, ND No. 2-020101-104-E

Item of technical supervision:

Ships under construction and in service

Implementation: from 1 January 2018

Valid: till ----

Validity period extended till ----

~~Cancels / Amends / Supplements Circular Letter~~
No.

dated ----

Number of pages: 1+6

Appendices: text of amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Ships, 2018, ND No. 2-020101-104-E

Director General

K.G. Palnikov

Amends

Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104-E

We hereby inform that new distinguishing marks and descriptive notations shall be introduced to the Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104-E.

It is necessary to do the following:

1. Familiarize surveyors of the RS Branch Offices and interested organizations in the area of the RS Branch Offices' activity with the content of the Circular Letter..
2. Apply the requirements specified in the Appendix to the Circular Letter to the RS practical activity.

Person in charge: V.K.Shurpyak

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**RULES FOR THE CLASSIFICATION AND CONSTRUCTION
OF SEA-GOING SHIPS, 2018,
ND No. 2-020101-104**

PART I. CLASSIFICATION

2.2. CLASS NOTATION OF A SHIP

The Chapter shall be supplemented by new para **2.2.38** reading as follows:

"2.2.38 Distinguishing mark for ships fitted with boiler plant monitoring system.

If a ship is fitted with a boiler plant monitoring system that allows to carry out internal surveys of steam boilers internal surveys without participation of Register Surveyor, the distinguishing mark **BMS** (Boiler Monitoring System) shall be added to the character of classification".

Paras 2.2.38 and 2.2.39 shall be renumbered as **paras 2.2.39 and 2.2.40** accordingly.

**PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE
CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL
PARTICULARS OF SHIPS**

New **Section 16** shall be introduced reading as follows:

"16 REQUIREMENTS FOR BOILER MONITORING SYSTEMS

16.1 GENERAL PROVISIONS AND APPLICATION

16.1.1 Distinguishing mark **BMS** (Boiler Monitoring System) may be added to the character of classification of ships fitted with boiler plant monitoring system that allows not to carry out internal surveys of steam boilers at the presence of the RS surveyor. This Section specifies technical and organizational requirements for the ships with the distinguishing mark **BMS**, which shall be followed to allow the survey carried out by the chief engineer to be credited by the Register as boiler internal survey. Documentation on the performed internal survey shall be presented to the attending RS surveyor who shall carry out the remaining scope of the boiler survey.

16.1.2 To assign the distinguishing mark **BMS**, the initial survey shall be performed to confirm that the boiler design and technical condition make it possible for the crew to perform the survey, that the ship is fitted with appropriate boiler condition control and

monitoring system, and that the ship's chief engineer is qualified to partially perform the scope of boiler survey.

16.1.3 Distinguishing mark **BMS** may be assigned to auxiliary oil-fired steam boilers and waste-heat boilers with working pressure not exceeding 2,0 MPa.

16.1.4 Distinguishing mark **BMS** may be assigned to both ships with new boilers and boilers in service.

16.1.5 Distinguishing mark **BMS** can be withdrawn at the discretion of the shipowner or proceeding from the results of ship survey carried out by the RS surveyor. After that, the ship's boiler plant shall be submitted to the Register on a common basis.

16.2 TERMS AND DEFINITIONS

In addition to the below mentioned, the definitions specified in Chapter 1.2, Part X "Boilers, Heat Exchangers and Pressure Vessels" and in 1.1.1, Part I "Classification" of the Rules for the Classification and Construction of Sea-Going Ships are applicable to the requirements of this Section.

Monitoring means continuous process of reading and recording item's parameters under control, which are assumed essential for the life duration, and comparing these parameters with specified values.

Boiler water means water inside the boiler and all its components.

Feed water means water supplied by feed water pumps to the steam boiler to generate steam; it is a mixture of condensate and make-up water.

Make-up water means water added to the feed water for replenishing the leaks and condensate losses; it is a mixture of distillate and chemically treated water.

Condensate means water generated in the condensate and feed water system upon the waste steam condensation.

Distillate means water generated in the desalinating plant by evaporation and condensation of sea water.

16.3 TECHNICAL AND OPERATING DOCUMENTATION

16.3.1 For steam boilers, the ship's *Maintenance manual on boiler water monitoring and treatment* shall be developed. This document shall provide recommendations on pre-boiler and in-boiler water treatment and on prevention of scale formation and other factors leading to boiler plant excessive wear. This document shall be developed considering the requirements of instructions developed by boiler firms (manufacturers), standard instructions and applicable industry standards. The content and availability of this document on board the ship shall be checked by the RS surveyor during the initial survey for assigning the distinguishing mark **BMS** to the ship.

16.3.2 Maintenance manual on boiler water monitoring and treatment shall contain:

- .1 specification and brief description of water preparation process and equipment applied;
- .2 schedule, scope and methods of water quality control;
- .3 list and diagram of the sampling points;
- .4 make-up, feed, boiler water and condensate quality standards;
- .5 list of reagents necessary for water treatment and for ship's water laboratory;
- .6 data on filter regeneration (if applicable);
- .7 recommendations on boiler conservation for the period when they are not in operation.

16.3.3 The ship shall be provided with ship's boiler monitoring log-book. The following shall be recorded in the log-book:

data on boiler maintenance in accordance with the manufacturer's recommendations and boiler survey results;
results of water chemical analyses;
measures taken to provide the feed and boiler water quality standards;
measures taken for burner units maintenance in accordance with the manufacturer's recommendations;
periodic testing of automatic burner unit interlocking and protecting devices as specified in Chapter 5.3, Part X "Boilers, Heat Exchangers and Pressure Vessels".

16.4 ADDITIONAL REQUIREMENTS FOR THE SHIPS WITH THE DISTINGUISHING MARK BMS.

16.4.1 Additional requirements for boiler plants of ships with distinguishing mark BMS.

16.4.1.1 Special devices shall be provided for metering the chemicals and adding them to boiler and feed water.

16.4.1.2 Regular facilities shall be provided for collecting representative samples from boiler and feed water at safe temperature (e.g. by installing a sample cooler).

16.4.1.3 Facilities shall be provided for continuous early detection of excessive salinity, which shall immediately alarm when salt water is detected in the system.

16.4.1.4 Facilities shall be provided in condensate and feed water system for continuous early detection of oil products or transported goods in the boiler and feed water.

16.4.1.5 To remove oxygen, the feed water shall be kept in an open tank (e.g. in observation tank, hot well or a special deaerator) at temperature of at least 80°C.

16.4.1.6 Regular facilities shall be provided for monitoring pressure difference before and after exhaust boilers.

16.4.2 Boiler, feed and make-up water quality monitoring.

16.4.2.1 Feed water shall contain minimum dissolved salts, gases, organics and insoluble suspended solids. The main water quality indicators to be controlled within the monitoring process are total hardness, chloride, oxygen and oil products content.

16.4.2.2 Boiler water quality shall be maintained and documented in accordance with recommended limiting values of boiler and feed water quality indicators as specified by the boiler manufacturer. Where there are no any special instructions from the boiler manufacturer, the boiler and feed water quality requirements specified in Table 16.4.2 for steam boilers with working pressure not exceeding 2 MPa shall be followed.

16.4.2.3 Water quality shall be regularly checked using regular facilities and periodical water analysis in land-based laboratories. Boiler and feed water shall be monitored with the use of on-board regular facilities at least every 24 h. Boiler and feed water analysis results shall be recorded in a ship's log book.

16.4.2.4 Boiler water analysis in land-based laboratories shall be carried out at least once a month, and results shall be kept on board the ship.

16.4.2.5 In any cases, deviation of boiler water quality from the prescribed standards shall be immediately corrected. Acceptable methods of maintaining water quality are maximum condensate return, surface and bottom blowdown, pre-boiler chemical treatment of the feed and make-up water, in-boiler chemical water treatment. Another method to ensure water quality may be adopted instead of chemical treatment, provided that its equivalence is substantiated.

16.4.2.6 Boiler water quality shall be annually analyzed by the shipowner and corrected, if necessary. Measures to improve the boiler water quality shall be developed to prevent hard deposit formation and corrosion damages; these measures shall be based on analyses (examinations) of hard deposits found in boiler and corrosion damages.

Table 16.4.2

Recommended boiler and feed water quality standards

Water type	Quality indicator	Measurement unit	Gas-tube boilers	Water-tube and composite boilers
Feed water	Total hardness	mg-eq/l	not more than 0,5	not more than 0,3
	Oil and oil products	mg/l	not more than 3	not more than 3
	Oxygen	mg/l	not more than 0,1	not more than 0,1
	Chlorides	mg/l	not more than 50	not more than 15
Condensate	Chlorides	mg/l	not more than 50	not more than 15

Distillate ³	Total hardness	mg-eq/l	–	not more than 0,05
Make-up water ³	Total hardness	mg-eq/L	not more than 8	not more than 5
Boiler water	Chlorides	mg/L	not more than 8000	not more than 1200
	Base number	mg/L	150 to 200	150 to 200
	Residual hardness	mg-eq/L	not more than 0,4	not more than 0,2
	Total salinity	mg/L	not more than 13000	not more than 3000
	Phosphate number ¹	mg/L	30 to 60	30 to 60
	Nitrate number ¹	mg/L	75 to 100 ²	75 to 100 ²
Notes: 1. To be monitored for boilers with phosphate/nitrate water treatment mode. 2. The nitrate number shall be 50 % of the actual base number. 3. To be monitored during make-up water preparation.				

16.5 SURVEYS

16.5.1 Initial survey.

16.5.1.1 Initial survey for assigning the distinguishing mark **BMS** to the ship shall be carried out by the RS surveyor in the scope of special survey, including internal survey and furnace inspection.

16.5.1.2 During initial survey for assigning the distinguishing mark **BMS** to the ship, the RS surveyor shall check boiler's overall technical condition in accordance with 16.4.1, compliance with the requirements of 16.4.2 and availability of the log-books required.

16.5.1.3 The boiler shall comply with strength and design requirements of the RS rules as specified in Part X "Boilers, Heat Exchangers and Pressure Vessels". The boiler shall not have indications of any damages, which were not documented and agreed with the Register during the last repair. Plugged tubes are not allowed. The boiler heating surfaces shall be free of soot, sludge, ripple or metal overheat marks. The boiler components shall not have any visible deformations or damages.

16.5.2 Periodical surveys.

16.5.2.1 Periodical internal surveys of boiler's water/steam and furnace/fire sides for ships with boiler plant monitoring system and distinguishing mark **BMS** shall be performed by

the crew against requirements of 2.9.3, Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service without participation of the RS surveyor. The Report on Survey supplemented with photos of the boiler's components subject to internal survey shall be signed by the chief engineer.

16.5.2.2 Internal surveys of boiler's water/steam side shall be performed by the crew at least once a year but not more than 30 days before annual ship survey. If the boiler has components not accessible for internal survey, the internal survey shall be followed by hydraulic tests with test pressure equal to 1,25 working pressure in accordance with 2.9.2.3, Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service; the testing shall be reflected in the Report on Survey signed by the chief engineer.

16.5.2.3 Internal survey of boiler's furnace/fire side shall be performed by the ship crew at least twice a year.

16.5.2.4 During annual survey, the documentation on performed internal surveys and photos of boiler's components subject to internal survey shall be submitted to the RS surveyor, who reviews the submitted materials and performs the boiler external examination in accordance with 2.9.1, Part II "Survey Schedule and Scope" of the Rules for the Classification Surveys of Ships in Service. If the boiler internal survey (internal examination) documents are drawn up improperly or there are reasonable doubts regarding reliability of the photos submitted, the RS surveyor is entitled to require repeated boiler internal survey in his presence.

16.5.2.5 During annual survey of the ship, the documentation on boiler and feed water monitoring along with results of annual boiler water analysis shall be submitted to the RS surveyor in accordance with 16.4.2.6."



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 313-08-1083c

dated 28.12.2017

Re:

amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Ships, 2018, ND No. 2-020101-104-E

Item of technical supervision:

ships under construction

Implementation 01.01.2018

Valid: till ----

Validity period extended till ----

~~Cancels / Amends / Supplements~~ Circular Letter ----
No.

dated ----

Number of pages: 1+2

Appendices: text of amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Ships, 2018, ND No. 2-020101-104-E

Director General

K.G. Palnikov

Amends

Rules for the Classification and Construction of Sea-Going Ships, 2018,
ND No. 2-020101-104-E

We hereby inform that due to entering into force on 01.01.2018 of the IACS Unified Interpretation (UI) GF3 (Dec 2017), GF4 (Dec 2017), GF5 (Dec 2017), GF6 (Dec 2017) GF7 (Dec 2017), GF8 (Dec 2017), GF9 (Dec 2017), GF 10 (Dec 2017), GF 11 (Dec 2017) and GF12 (Dec 2017) Section 9, Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Ships, 2018, ND No. 2-020101-104-E shall be amended as specified in the Appendix to the Circular Letter. The original texts of the above UI in English are published on the RS internal website in the Section "External Normative Documents/02 IACS Documents/ 0234 GF.

It is necessary to do the following:

1. Follow the provisions of the Circular Letter during the review and approval of the ships' technical documentation.
2. Bring the content of the Circular Letter to the notice of the RS surveyors, interested organizations and persons in the area of the RS Branch Offices' activity.

Person in charge: V.K.Shurpyak

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"Thesis" System: 17-348449

**RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS,
2018, ND No. 2-020101-104-E**

**PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE
CLASS NOTATION DEFINING STRUCTURAL AND OPERATIONAL PARTICULARS
OF SHIPS**

Section 9. Requirements for ships equipped for using gases or low-flashpoint fuels

Para 9.1.3 shall be amended to read:

“Tank connection space is a space surrounding all tank connections and tank valves that is required for tanks with such connections in enclosed spaces.”.

Para 9.2.4.11 shall be amended to read:

“In this case:

.1 Fuel preparation rooms, regardless of location, shall be arranged to safely contain cryogenic leakages.

.2 The material of the boundaries of the fuel preparation room shall have a design temperature corresponding with the lowest temperature it can be subjected to in a probable maximum leakage scenario unless the boundaries of the space, i.e. bulkheads and decks, are provided with suitable thermal protection.

.3 The fuel preparation room shall be arranged to prevent surrounding hull structure from being exposed to unacceptable cooling, in case of leakage of cryogenic liquids.

.4 The fuel preparation room shall be designed to withstand the maximum pressure build up during such a leakage. Alternatively, pressure relief venting to a safe location (mast) can be provided.”.

Para 9.3.1.4 shall be amended to read:

“A tank connection space may be required also for tanks on open deck. This may apply for ships where restriction of hazardous areas is safety critical. A tank connection space may also be necessary in order to provide environmental protection for essential safety equipment related to the gas fuel system like tank valves, safety valves and instrumentation. A tank connection space may also contain equipment such as vaporizers or heat exchangers. Such equipment is considered to only contain potential sources of release, but not sources of ignition. In this case, such tank connection space is not regarded as a fuel preparation room.”.

Para 9.3.2.2 shall be amended to read:

“All liquefied gas fuel tanks shall be fitted with safety valves in compliance with the requirements of 3.19.1, Part VI “Systems and Piping” of the Rules for the Classification and Construction of Ships Carrying Liquefied Gases in Bulk. “.

Para 9.4.2 shall be amended to read:

"Liquefied gas fuel tanks' pressure and temperature shall be controlled and maintained within the design range at all times including after activation of the safety system required in 9.10.4 for a period of minimum 15 days. The activation of the safety system alone is not deemed as an emergency situation."

Para 9.5.2.1 shall be amended to read:

"The special consideration shall as a minimum include, but not be restricted to, the following design features:

- .1 segregation towards other areas on the ship;
- .2 hazardous area plans for the ship;
- .3 requirements for forced ventilation;
- .4 requirements for leakage detection (e.g. gas detection and low temperature detection);
- .5 safety actions related to leakage detection (e.g. gas detection and low temperature detection);
- .6 access to bunkering station from non-hazardous areas through airlocks;
- .7 monitoring of bunkering station by direct line of sight or by CCTV."

Para 9.6.1 shall be supplemented by subparagraph 9.6.1.8 reading as following:

"9.6.1.8 Premixed engines using fuel gas mixed with air before the turbocharger shall be located in ESD protected machinery spaces."

Para 9.8.3.1 shall be amended to read:

"Spaces enclosed in the boundaries of machinery spaces (such as purifier's room, engine-room workshops and stores) are considered an integral part of machinery spaces containing gas-fuelled consumers and, therefore, their ventilation system does not need to be independent of the one of machinery spaces."

Para 9.8.6.2 shall be amended to read:

"Double piping and gas valve unit spaces in gas safe engine-rooms are considered an integral part of the fuel supply systems and, therefore, their ventilation system does not need to be independent of other fuel supply ventilation systems provided such fuel supply systems contain only gaseous fuel."

Para 9.8.6.3 shall be amended to read:

"The ventilation inlet for the double wall piping or duct shall always be located in a non-hazardous area in open air away from ignition sources. The inlet openings shall be fitted with suitable wire mesh guards and protected from ingress of water."



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 312-11-1090c

18.01.2018

Re:

amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104E by requirements to indoor climate in living and working spaces

Item of supervision:

Ships under construction and in service

Implementation from the date of publication

Valid: till -

Validity period extended till -

~~Cancels / amends / adds circular letter No.~~

Number of pages: 1 + 3

Appendices: amendments to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104E

Director General  Konstantin G. Palnikov

Amends Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104E

We hereby inform that new Section 17 has been introduced to Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" related to the additional voluntary requirements for indoor climate in ship's spaces.

It is necessary to do the following:

1. Familiarize surveyors of the RS Branch offices and interested organizations in the area of the RS Branch Offices' activity with the content of the Circular letter.
2. Apply the above requirements in the RS practical activity.

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"Thesis" System No. 17-348454

RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA- GOING SHIPS, 2018, ND No. 2-020101-104-E

Part I. CLASSIFICATION

2.2. CLASS NOTATION OF A SHIP

The Chapter shall be supplemented with new para **2.2.39** reading as follows:

"2.2.39. Indoor hygiene and sanitary conditions

Ships complying with the indoor climate requirements specified in Section 17 of Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" are assigned the distinguishing mark **COMF(C)** added to the character of classification."

Paras **2.2.39** and **2.2.40** shall be renumbered as paras **2.2.40** and **2.2.41** accordingly.

Part XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

New Section 17 shall be introduced reading as follows:

"17 INDOOR HYGIENE AND SANITARY CONDITIONS

17.1 INDOOR CLIMATE

17.1.1 General.

Ships complying with the indoor climate requirements of this Chapter may be assigned the distinguishing mark **COMF(C)** added to the character of classification.

17.1.2 Definitions.

Air supply quantity means total amount of supplied air to any given space, which may consist of a percentage re-circulated return air in addition to the fresh air supply quantity.

Air velocity means measured mean absolute velocity of air mass in motion.

Fresh air supply quantity means quantity of fresh/outside air per person supplied to a space, expressed in l/s or m³/h.

Indoor climate means indoor ambient temperature, temperature gradient, air velocity, humidity and carbon dioxide concentration used as parameters for indoor climate.

Relative humidity means ratio of the partial pressure of water vapor in air to the equilibrium pressure of saturated vapors at a specified temperature.

Vertical gradient means vertical air temperature difference.

17.1.3 Documentation.

In addition to documentation specified in Section 3, Part I "Classification" the following documentation shall be submitted (A – for approval, FI – for information):

- .1 heat balance calculation (FI);
- .2 program of mooring and sea trials (A);
- .3 measurement report (FI).

17.1.4 Requirements for on board climate.

17.1.4.1 Measurements.

.1 for ships with less than 100 cabins and the accommodation restricted to a separate section in the aft-ship, midship or in the fore-ship a full set of measurements applicable to climate parameters shall be taken in the following minimum number of cabins (n = number of cabins):

- for $n < 10$ – measurements in all cabins;
- for $10 \leq n \leq 40$ – measurements in at least 10 cabins;
- for $n \geq 41$ – measurements in at least 25 % of all cabins.

The cabins to be measured shall be evenly distributed amongst the cabins on each deck or in each respective fire zone.

.2 for ships with more than 100 cabins distributed over a major portion of the ship, e.g. passenger ships, a full set of measurements shall be taken in at least 10 % of the cabins in each fire zone containing cabins on each deck. The cabins to be measured shall be evenly distributed amongst the cabins on each deck or in each respective fire zone;

.3 climate parameters shall be measured in a representative number of public spaces on board. The measuring positions shall be selected such as to give a representative description of the climate in the public spaces on board the ship.

17.1.4.2 Air temperature.

.1 band width between 20°C to 24°C at outside temperature ≤ 15 °C and between 24 °C to 28 °C at outside temperature ≥ 40 °C shall be provided;

.2 air temperature in a designated space shall be measured at the geometrical centre of the location. For larger spaces the temperature shall be measured in a representative number of positions in the occupancy zone;

.3 individual space temperature control is required.

17.1.4.3 Relative humidity.

.1 Heating, Ventilation and Air Conditioning (HVAC) system shall provide and maintain a relative humidity within a range from at least 20 % to 60 % maximum;

.2 air relative humidity value is determined based on documentation and shall not be generally verified through measurements.

17.1.4.4 Enclosed space vertical gradient.

.1 vertical gradient shall be maintained within 3 °C;

.2 vertical temperature difference in all designated spaces shall be measured in the geometric centre of the occupancy zone at the following distances above the floor: 0,2 m, 1,0 m and 1,8 m. For larger spaces, measurements shall be taken in representative positions.

17.1.4.5 Air velocity.

.1 mean air velocities shall not exceed 0.35 m/s at the measurement position in the space;

.2 mean air velocity shall be measured at the geometric centre of the space. However, the surveyor may request alterations of the measurement position based on survey results. Typical alteration may be to carry out the measurement at the most commonly occupied position in the space in question.

17.1.4.6 Air exchange rate.

.1 air exchange rate for cabins, public spaces, wheelhouse and control stations shall be at least 6 complete air changes per hour.

17.1.5 Requirements for HVAC system.

17.1.5.1 General.

.1 individual space temperature control is required;

.2 in case of system failure, a controlled climate in cabins, hospitals and messrooms shall be restored after maximum 12 h. If different failures, not related to each other, occur simultaneously, the required restoring time shall be increased by 12 h;

.3 minimum level of ventilation in hospitals and machinery control rooms shall be provided during a system failure by means of separate forced ventilation. Regulation of the fans shall be located in the respective spaces. This ventilation shall maintain the temperature below 35 °C and above 15 °C;

.4 it shall be possible to examine, clean or replace air ducts, central air handling units, air filters, dust collectors, heat exchangers, re-heaters and air terminals at regular work intervals."



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 314-08-1112c

dated

26.03.2018

Re:

implementation of IMO Resolution MSC.415(97) provisions in the Rules for Classification and Construction of Sea-Going Ships, 2018, No. 2-020101-104-E

Item(s) of supervision:

tugs, escort tugs, anchor-handling ships, floating cranes and crane ships

Implementation:

from the date of publication

Valid till:

31.12.2018

Validity period extended till: -

Cancels / amends / adds Circular Letter No. -

dated -

Number of pages:

1+16

Appendix(ces):

text of amendments to Part IV "Stability" and Part XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships"

Director General

Konstantin G. Palnikov

Text of CL:

We hereby inform that in connection with the adoption of IMO Resolution MSC.415(97) "Amendments to Part B of the International Code on Intact Stability, 2008" Rules for Classification and Construction of Sea-Going Ships shall be amended as specified in the Appendix to the Circular Letter.

The above amendments will be introduced into the Rules at their re-publication.

It is necessary to do the following:

1. Familiarize the RS surveyors and interested organizations in the area of the RS Branch Offices' activity with the content of the Circular Letter.
2. Apply the provisions of the Circular Letter in the RS practical activity.

List of ND amended and introduced paras/chapters/sections (to specify in the List of Circular Letters (form 8.3.36)):

Part IV: paras 3.7.1.3, 3.7.3.5, 4.1.1.5 and Appendix 3

Part XVII: para 2.2.2.1.6

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**RULES FOR CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS,
2018,
ND-2-020101-104-E**

PART IV. STABILITY

3 ADDITIONAL REQUIREMENTS FOR STABILITY

A new **para 3.7.1.3** shall be introduced reading as follows:

«**3.7.1.3** For the confirmation of sufficient stability of tugs intended for inner and outer road operations and ocean towage, checking may be done in compliance with the requirements specified in Section 2, Appendix 3 to the present Part.».

A new **para 3.7.3.5** shall be introduced reading as follows:

«**3.7.3.5** For the confirmation of the sufficient stability of ships engaged in anchor handling, checking may be done in compliance with the requirements specified in Section 1 Appendix 3 to the present Part.».

**4 REQUIREMENTS FOR THE STABILITY OF FLOATING CRANES, CRANE SHIPS,
TRANSPORT PONTOONS, DOCKS AND BERTH-CONNECTED SHIPS**

A new **para 4.1.1.5** shall be introduced reading as follows:

«**4.1.1.5** For the confirmation of the sufficient stability of ships covered by the provisions of the present Chapter, checking may be done in compliance with the requirements specified in Section 1, Appendix 3 to the present Part.».

The Part shall be supplemented with a new **Appendix 3** reading as follows:

IMO RESOLUTION MSC.415 (97) REQUIREMENTS FOR THE STABILITY OF SHIPS ENGAGED IN ANCHOR HANDLING, TUGS, ESCORT TUGS, FLOATING CRANES AND CRANE SHIPS

Prior to coming into force of IMO Resolution MSC.415(97) the requirements specified in the present Appendix may be used for stability checking of ships engaged in anchor handling, tugs, escort tugs, floating cranes and crane ships.

1 SHIPS ENGAGED IN ANCHOR HANDLING

1.1 Heeling lever.

1.1.1 A heeling lever, $HL\varphi$, in m, generated by the tension applied to the towing line should be calculated as:

$$HL\varphi = (M_{AH}/\Delta_2)\cos\theta$$

where $M_{AH} = F_p(h \cdot \sin\alpha \cdot \cos\beta + y \cdot \sin\beta)$;

$$F_v = F_p \cdot \sin\beta;$$

F_p – permissible towing line tension, in tm, which can be applied to the ship during operation while working through specified towing pins. F_p shall in no circumstance be taken as greater than F_d ;

F_d – design maximum towing line tension, in tm, the maximum winch towing line pull or maximum static winch brake holding force, whichever is greater;

β – the vertical angle, in deg., between the waterline and the vector at which the towing line tension is applied determined at the maximum heeling moment angle and calculated as $\arctg(y/(h \cdot \sin\alpha))$. β shall be taken not less than $\arccos(1,5B_p/(F_p \cdot \cos\alpha))$;

B_p – maximum continuous pull (the Bollard pull), in tm;

h – the vertical distance, in m, from the centre the propulsive force acts on the ship to either:

the uppermost part at the towing pin, or

a point on a line defined between the highest point of the winch pay-out and the top of the stern or any physical restriction of towing line transverse movement;

α – the horizontal angle, in deg., between the centreline and the vector at which the towing line tension is applied to the ship in the upright position;

y – the transverse distance, in m, from the centreline to the outboard point at which the towing line tension is applied to the ship, calculated as $y_0 + x \cdot \tan\alpha$. y shall be taken not greater than $B/2$;

y_0 – the transverse distance, in m, between the ship centreline to the inner part of the towing pin or any physical restriction of the transverse towing line movement;

x – the longitudinal distance, in m, between the stern and the towing pin or any physical restriction of the transverse towing line movement.

B – breadth of the ship, in m;

Δ_2 – displacement of a ship, including action of the vertical loads added (F_v), at the centreline in the stern of the ship;

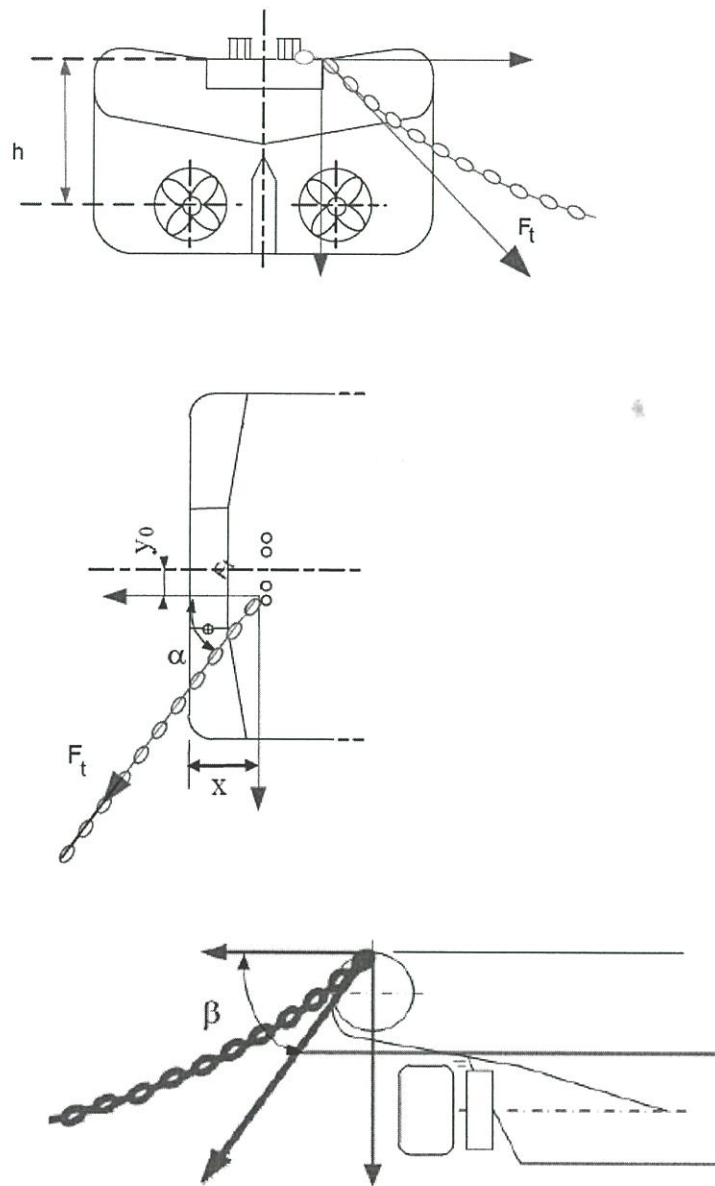


Рис. 1.1.1 Diagram showing the positions of angles α and β and distances h , x and y .
 F_t shows the vector of the applied towing line tension

1.2 Permissible towing line tension.

1.2.1 3 The calculated permissible towing line tension shall not be greater than the value specified in 1.2.2.

1.2.2 Permissible towing line tension as function of α determined in accordance with 1.1. can be calculated by direct stability calculations, provided that the following conditions are met:

- .1 the heeling lever is calculated as defined in 1.1 for each α ;
- .2 all the stability criteria specified in 1.3 are met;

.3 α shall not be taken less than 5° , except the case specified in 1.2.3;

.4 intervals of α shall be not be more than 5° , except the cases where permissible towing line tension does not exceed values calculated for more unfavourable values of α ;

1.2.3 For operations to retrieve a stuck anchor, in which the ship is on station above the anchor and the ship has low or no speed, α may be taken as less than 5° .

1.3 Stability criteria.

1.3.1 Stability of a ship during operations of anchor handling shall comply with the criteria specified in this Chapter. In other conditions the ship's stability shall comply with the criteria specified in Section 2 or other applicable criteria.

1.3.2 The area between the righting lever curve and the heeling lever curve calculated in accordance with 1.1.1 and determined from the first intersection of the two curves, to the angle of the second intersection or the angle of down-flooding, whichever is less, shall not be less than 0,070 mrad.

1.3.3 The maximum righting lever between the righting lever curve and the heeling lever curve calculated in accordance with 1.1.1 shall be at least 0,2 m.

1.3.4 The static angle at the first intersection between the righting lever curve and the heeling lever curve calculated in accordance 1.1.1 shall not be greater than:

.1 the angle at which the righting lever equals half of the maximum righting lever;

.2 the deck edge immersion angle;

.3 15° , whichever is less.

1.3.5 A minimum freeboard at stern, on centreline, of at least $0,005L$ shall be maintained in all loading conditions, including vertical loads added, (as per the definition of displacement Δ_2 given in 1.1.1). In the event of the anchor retrieval operation specified in 1.2.3, a lower minimum freeboard may be accepted provided that due precautions are indicated in the operation plan.

1.4 Stability of ships engaged in anchor handling shall be checked in the following loading conditions in addition to those specified in 1.4.8.2:

.1 loading condition at the maximum draught at which anchor handling operations may occur, with 67 % of stores;

.2 loading condition at the minimum draught at which anchor handling operations may occur, with 10 % of stores.

1.5 Stability of ships engaged in anchor handling shall be checked for all towing pins with relevant maximum towing line tension, and other structural elements limiting the towing line movement.

1.6 For ships engaged in anchor handling in loading conditions specified in 1.4 when applying the design tension F_d , for the towing pin nearest to centerline, stability criteria specified in 1.2.2 shall be met as a minimum, for α equal to 5° .

1.7 Stability instrument.

1.7.1 A stability instrument may be used for determining the permissible towing line tension and checking compliance with relevant stability criteria. Two types of stability instrument may be used on board:

.1 software checking the permissible tension on the basis of the permissible tension curves;

.2 software performing direct stability calculations to check compliance with the relevant criteria, for a given loading condition (before application of the towing line tension force), a given tension and a given towing line position (defined by angles α and β).

2 TUGS AND ESCORT TUGS

2.1 Heeling lever.

2.1.1 The heeling lever, in m, occurring during towing operations is calculated as follows:

.1 a transverse heeling moment is generated by the maximum transverse thrust exerted by the ship's propulsion and steering systems and the corresponding opposing towing line pull.

.2 the heeling lever HL_φ , in (m), as a function of the heeling angle φ , should be calculated according to the following formula:

$$HL_\varphi = \frac{BP \cdot C_T \cdot (h \cdot \cos\varphi - r \cdot \sin\varphi)}{g \cdot \Delta}$$

where BP – maximum continuous pull (bollard pull), in kN;

$C_T = 0,5$, for ships with non-azimuth propulsion units;

$0,9/(1+L/L)$, for ships with azimuth propulsion units installed at a single point along the length. C_T shall not be less than 0,7 for ships with azimuth stern drive towing over the stern or tractor tugs towing over the bow, and not less than 0,5 for ships with azimuth stern drive towing over the bow or tractor tugs towing over the stern.

For ships with other propulsion and towing arrangements, the value of C_T shall be determined in accordance with the procedure approved by the Register.

Δ – displacement, in t;

l – longitudinal distance, in m, between the towing point and the vertical centreline of the propulsion unit;

h – vertical distance, in m, between the towing point and the horizontal centreline of the propulsion unit;

g – gravitational acceleration, in m/s^2 , to be taken as 9,81;

r – the transverse distance, in m, between the centreline and the towing point;

L – length of the ship, in m.

The towing point (being the location where the towing line force is applied to the ship) may be a towing hook, staple, fairlead or equivalent fitting serving for fastening or limiting the movement of the towing line.

2.1.2 The heeling lever HL_φ , in m, occurring due to towing line jerk effect, is calculated according to the following formula::

$$HL_\varphi = C_1 \cdot C_2 \cdot \gamma \cdot V^2 \cdot A_p \cdot (h \cdot \cos\varphi - r \cdot \sin\varphi + C_3 \cdot d) / (2 \cdot g \cdot \Delta)$$

where $C_1 = 2,8 \left(\frac{L_S}{L_{pp}} - 0,1 \right)$ $0,1 \leq C_1 \leq 1,00$

$C_2 = \left(\frac{\theta}{3\theta_D} + 0,5 \right)$ $C_2 \leq 1,00$;

θ_D – the deck edge immersion angle, in deg., calculated according to the formula $\theta_D = \arctg\left(\frac{2f}{B}\right)$

C_3 – distance from the centre of lateral projected area of the underwater hull A_P to the waterline as fraction of the draught related to the heeling angle, in m.

$C_3 = \left(\frac{\theta}{\theta_D} \right) \cdot 0,26 + 0,30$ $0,50 \leq C_3 \leq 0,83$;

γ – specific gravity of water, in t/m³;

V – lateral velocity, in m/s, to be taken as 2,57 (5 knots);

A_p – lateral projected area of the underwater hull on the centerline, in m²;

r – the transverse distance between the centreline and the towing point, in m;

L_S – the longitudinal distance, in m, from the aft perpendicular to the towing point;

d – draught of the ship, in m.

The towing point (being the location where the towline force is applied to the ship) may be a towing hook, staple, fairlead or equivalent fitting serving for fastening or limiting the movement of the towing line.

2.2 Heeling lever for escort operations.

2.2.1 For the evaluation of the stability particulars during escort operations the ship is considered to be in an equilibrium position determined by the combined action of the hydrodynamic forces acting on hull and appendages, the thrust force and the towing line force as shown in Fig. 2.2.1.

2.2.2 At the design stage steering force, breaking force, heel angle and heeling lever may be determined by model tests or calculation. On the completion of the ship's construction, the values of maximum steering force and maximum heel angle of the tug are specified by full scale tests or numerical simulations in accordance with a procedure approved by the Register

2.2.3 For each loading condition the evaluation of the equilibrium positions shall be performed over the applicable escort speed range, whereby the speed of the assisted ship through the water is to be considered (the typical escort speed range is 6 - 10 knots).

2.2.4 For each relevant combination of loading condition and escort speed, the maximum heeling lever shall be used for the evaluation of the stability particulars.

2.2.5 For the purpose of stability calculations the heeling lever shall be taken as constant.

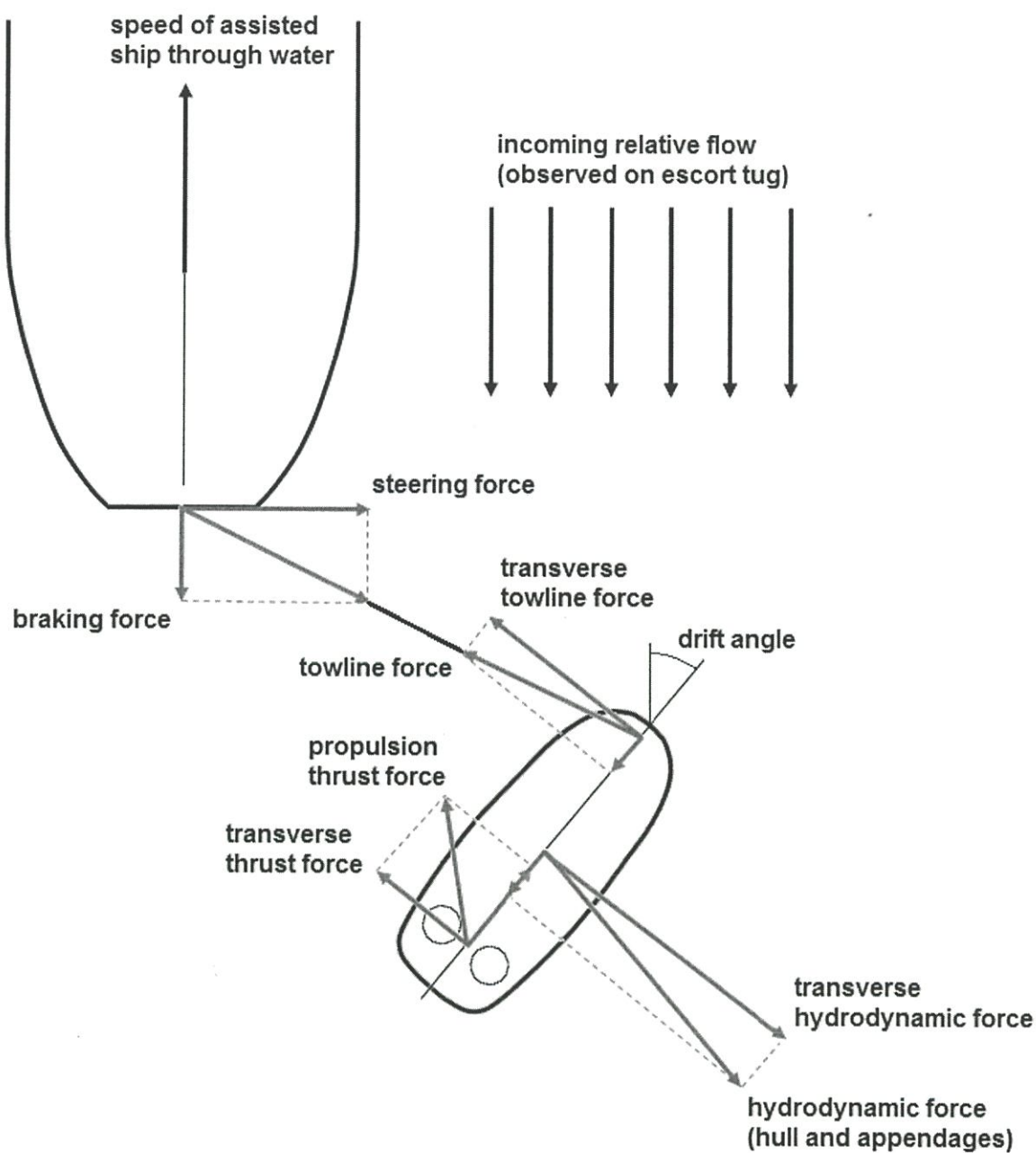


Fig. 2.2.1

2.3 Stability criteria.

2.3.1 Stability of ships during inner and outer road operations and ocean towage shall comply with the criteria specified in this Chapter in addition to those indicated in Section 2 and other applicable criteria.

2.3.2 For ships engaged in inner and outer road operations and ocean towage the area A contained between the righting lever curve and the heeling lever curve occurring during towing calculated in accordance with 2.1.1, measured from the heel angle θ_e to the angle of the second intersection θ_c , or the angle of down-flooding θ_f , whichever is less, shall be greater than the area B contained between the heeling lever curve and the righting lever curve, measured from the heel angle $\theta=0$ to the heel angle θ_e .

θ_e – heel angle, in deg., at first intersection between the heeling lever and righting lever curves;

θ_f – angle of down-flooding, in deg. In stability calculations openings fitted with weathertight closing devices, which may be required to keep open for operational reasons (doors leading to machinery and boiler trunks or to upper deck superstructures, as well as the doors to all companionways of spaces located below the upper deck) shall be taken into account;

θ_c – heel angle, in deg., at second intersection between the heeling lever and righting lever curves.

2.3.3 For ships engaged in inner and outer road operations and ocean towage the first intersection between the righting lever curve and the heeling lever curve occurring due to towing line jerk calculated in accordance with 2.1.2 shall occur at an angle of heel less than the angle of down-flooding, θ_f .

2.3.4 For escort tugs, the maximum heeling lever determined in accordance with paragraph 2.2 shall comply with the following criteria:

.1 $A \geq 1,25 \cdot B$;

.2 $C \geq 1,40 \cdot D$;

.3 $\theta_e \leq 15^\circ$,

where A – righting lever curve area measured from the heel angle θ_e to a heel angle of 20° (refer to Fig. 2.3.4-1);

B – heeling lever curve area measured from the heel angle θ_e to a heel angle of 20° (refer to Fig. 2.3.4-1);

C – righting lever curve area measured from the zero heel to the heel angle θ_d (refer to Fig. 2.3.4-2);

D – heeling lever curve area measured from zero heel to the heel angle θ_d (refer to Fig. 2.3.4-2);

θ_e – heel angle, in deg., corresponding to the first intersection between heeling lever curve and the righting lever;

θ_d – the heel angle, in deg., corresponding to the second intersection between heeling lever curve and the righting lever curve or the angle of down-flooding, whichever is less.

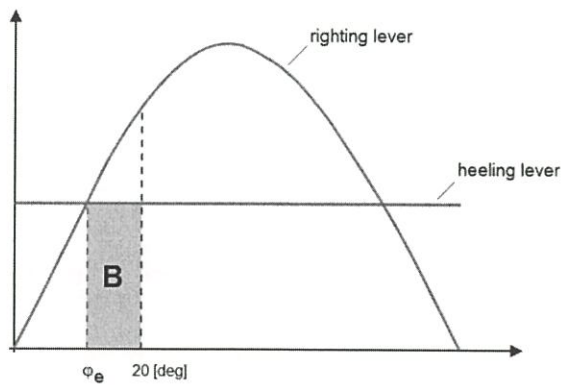
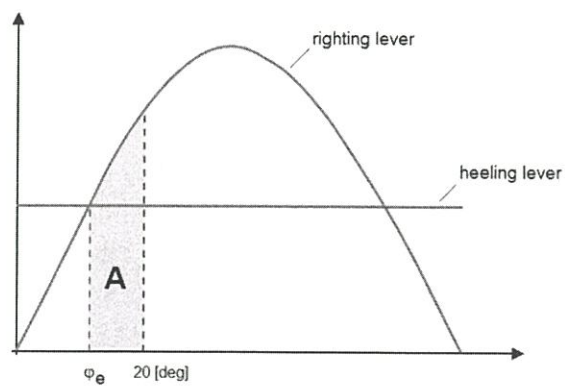


Fig. 2.3.4-1

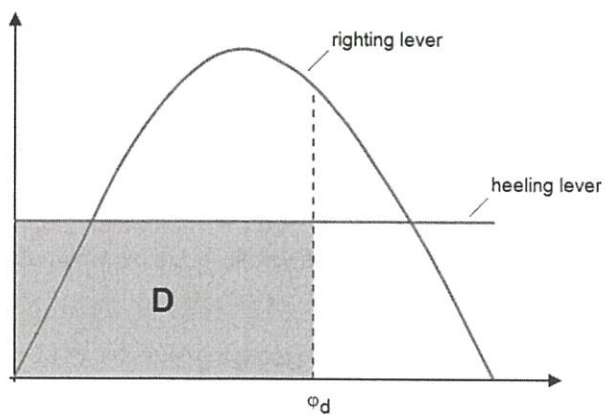
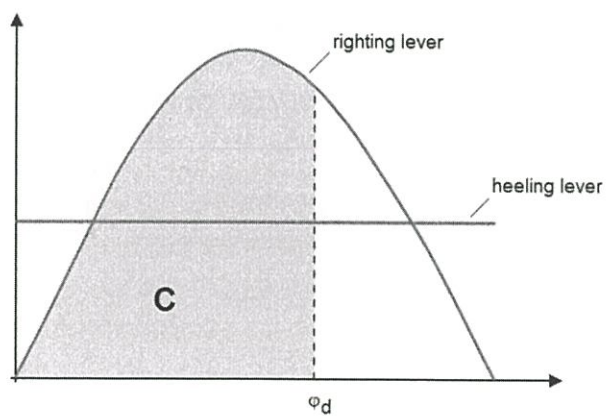


Fig. 2.3.4-2

2.3.5 A minimum freeboard at stern, of at least $0,005L$, measured on centerline, shall be maintained in all loading conditions.

2.4 Stability of tugs engaged in inner and outer road operations and ocean towage and escorting operations shall be checked in the following loading conditions in addition to those specified in 1.4.8.2:

.1 maximum operational draught at which towing or escorting operations may be carried out, with 100 % of stores;

.2 minimum operational draught at which towing or escorting operations may be carried out, with 10 % of stores;

.3 intermediate condition with 50 % of stores.

2.5 For ships engaged in inner and outer road operations, ocean towage, anchor handling, floating cranes/crane ships allowance shall be made for the weight of cargo, chains, spare towing lines and towing lines for towing winches.

3 FLOATING CRANES/CRANE SHIPS

3.1 Application.

3.1.1 The provisions of the present Chapter shall apply to ships engaged in lifting operations, including those involving lifting of the ship's own structures or lifting of cargoes, in which the maximum heeling moment due to the lift is greater than that calculated by the following formula:

$$M_L = 0,67 \cdot \Delta \cdot GM \cdot \left(\frac{f}{B}\right)$$

where M_L – value for the heeling moment, in tm, induced by the load in the cargo handling gear;

GM – metacentric height, in m, with free surface correction, including the effect of the load in the cargo handling gear;

f – the minimum freeboard, in m, measured from the upper side of the weather deck to the waterline;

B – breadth of the ship, in m;

Δ – the displacement of the ship, including the lift load, in t.

The provisions of this Chapter shall also apply to ships which are engaged in lifting operations where the increase of the ship's vertical centre of gravity (VCG) due to the lifted weight is greater than 1 %.

The calculations shall be done for the most unfavourable loading condition, for which the use of cargo handling gear is possible.

3.1.2 For the purpose of this Section, waters that are not exposed are those where the environmental impact on the lifting operation is negligible. Otherwise, waters are to be considered exposed. In general, waters that are not exposed are calm stretches of water, i.e. estuaries, roadsteads, bays, lagoons; where the wind fetch *(a space with no physical obstacles, where wind can pass along the water in straight direction) is 6 miles or less.

3.2 Load and vertical centre of gravity for different types of lifting operations.

3.2.1 In the calculations of stability during lifting operations involving cargo handling gear consisting of a crane, derrick, sheerlegs, a-frame or similar:

.1 the magnitude of the vertical load P_L should be the maximum allowed static load at a given outreach of the cargo handling gear;

.2 the transverse distance y is the transverse distance between the point at which the vertical load is applied to the cargo handling gear and the ship centreline in the upright position;

.3 the vertical height of the load KG_{load} is taken as the vertical distance from the point at which the vertical load is applied to the cargo handling gear to the baseline in the upright position;

.4 the change of centre of gravity of the cargo handling gear shall be taken into account in calculations.

3.2.2 In the calculations of stability during lifting operations not involving cargo handling gear consisting of a crane, derrick, sheerlegs, a-frame or similar, which involve lifting of fully or partially submerged objects over rollers or strong points at or near a deck level:

.1 the magnitude of the vertical load P_L should be the winch brake holding load;

.2 the transverse distance y is the transverse distance between the point at which the vertical load is applied to the cargo handling gear and the ship's centreline in the upright position;

.3 the vertical height of the load KG_{load} is taken as the vertical distance from the point at which the vertical load is applied to the cargo handling gear to the baseline in the upright position.

3.3 Stability criteria.

3.3.1 The stability criteria specified in this Chapter, as well as the criteria stipulated in 3.4 - 3.5 and 3.7, as applicable, shall be fulfilled for all loading conditions where lifting operations are possible, with the cargo handling gear and its load at the most unfavourable positions, as regards stability. For the purpose of this Chapter and 3.4, the displacement and centre of gravity of the ship shall be calculated taking into account the weight and the centre of gravity (COG) of the cargo handling gear and its load.

3.3.2 Stability of ships during the lifting operations specified in 3.1.1 shall comply with the following stability criteria in addition to those stipulated in Section 2:

.1 the equilibrium heel angle shall not be greater than the maximum static heeling angle at which the reliable operation of the cargo handling gear is ensured;

.2 during lifting operations in non-exposed waters, the minimum distance between the water level and the highest continuous deck taking into account trim and heel at any position along the length of the ship, shall not be less than 0,5 m;

.3 during lifting operations in exposed waters, the minimum distance between the waterline and the highest continuous deck taking into account trim and heel at any

position along the length of the ship shall not be less than 1 m or the highest significant wave height ($0,75 \cdot h_{3\%}$), m, at which the operation is possible, whichever is greater.

3.4 Lifting operations conducted under environmental and operational limitations.

3.4.1 For stability checking during lifting operations carried out within clearly defined limitations specified in 3.4.1.1, instead of the criteria indicated in 3.3, the criteria stipulated in 3.4.1.2 may be applied:

.1 the limits of the environmental conditions shall include at least the following:

the maximum height of the wave of 3 % probability of exceeding level height, $h_{3\%}$;

the maximum wind speed (1 minute sustained at 10 m above sea level);

the limits of the operational conditions shall include at least the following:

the maximum duration of the lift;

limitations in ship speed;

limitations in traffic/traffic control.

.2 stability of the ship shall be checked at the most unfavourable position of the cargo handling gear and its load, as regards stability, for compliance with the following criteria:

.1 the corner of the highest continuous deck shall not be submerged;

.2 $A_{RL} \geq 1,40 \cdot A_{HL}$

where A_{RL} – the area under the net righting lever curve, corrected for crane heeling moment and for the righting moment provided by the counter ballast if applicable, extending from the equilibrium heeling angle θ_1 to the angle of down flooding θ_f or the angle of vanishing stability θ_R or the second intersection of the righting lever curve with the wind heeling lever curve, whichever is less (refer to Fig. 3.4.1.2);

A_{HL} – the area below the wind heeling lever curve due to the wind force applied to the ship and the lift at the maximum wind speed specified in 3.4.1.1 (refer to Fig. 3.4.1.2);

.3 the area under the net righting lever curve from the equilibrium heel angle θ_1 to the down flooding angle θ_f or 20° , whichever is less, shall be at least 0,03 mrad.

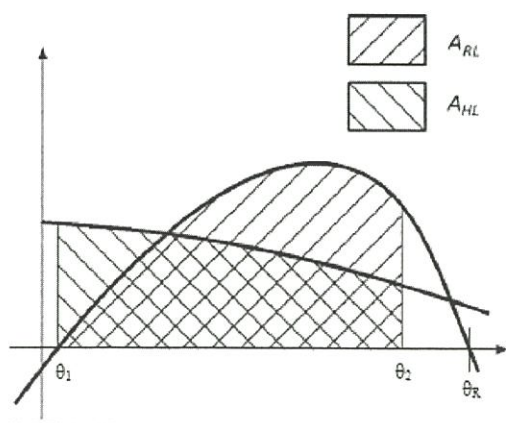


Fig. 3.4.1.2

3.5 Sudden loss of hook load.

3.5.1 Stability of a ship engaged in a lifting operation shall be sufficient to withstand the sudden loss of the hook load, considering the most unfavourable, as regards stability, point at which the hook load may be applied to the ship. To ensure the sufficient stability, the area on the side of the ship opposite to the lift (Area 2) shall be greater than the residual area on the side of the lift (Area 1), as shown in Fig. 3.5.1, by an amount given by the following:

$Area\ 2 \geq 1,40 \cdot Area\ 1$, for lifting operations in waters that are exposed;

$Area\ 2 \geq 1,00 \cdot Area\ 1$, for lifting operations in waters that are not exposed,

where GZ_1 – net righting lever (GZ) curve for the condition before loss of crane load, corrected for crane heeling moment and for the righting moment provided by the counter ballast if applicable;

GZ_2 – net righting lever (GZ) curve for the condition after loss of crane load, corrected for the transverse moment provided by the counter ballast if applicable;

θ_{e2} – the angle of static equilibrium after loss of crane load, in deg.;

θ_f – the angle of down-flooding, in deg., or the heel angle corresponding to the second intersection between heeling and righting arm curves, whichever is less.

The calculation of the GZ curve shall include the ship's true transverse centre of gravity as function of the angle.

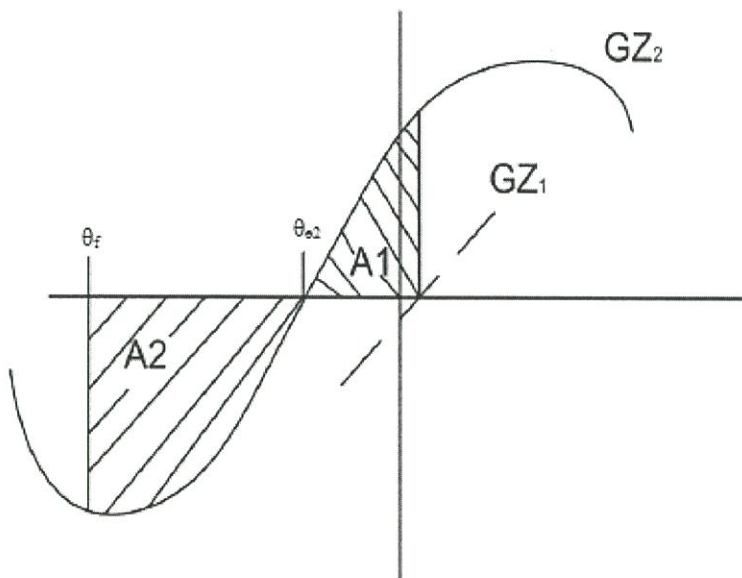


Fig. 3.5.1

3.6 Alternative method of stability calculation.

3.6.1 The criteria specified in 3.6 may be applied to ships engaged in a lifting operation, determined in 3.1.1 as an alternative to the criteria in 3.3 - 3.5, as applicable. For the purpose of this Chapter and 3.7, the lifted load which causes the ship to heel is translated

for the purpose of stability calculation to a heeling moment/heeling lever which is applied on the righting lever curve of the ship.

3.6.2 The heeling moment applied to the ship due to a lift and the associated heeling lever are calculated using the following formulae:

$$HM_{\theta} = P_L \cdot y \cdot \cos\theta$$

$$HL_{\theta} = HM_{\theta} \div \Delta$$

where HM_{θ} – the heeling moment, in tm, due to the lift at θ ;

P_L – the vertical load of the lift, in t, as defined in 3.2.1.1;

y – the transverse distance of the lift, in m, as defined in 3.2.1.2;

θ – the angle of heel, in deg.;

HL_{θ} – the heeling lever, in m, due to the lift at θ ;

Δ – the displacement of the ship, in t, with the load of the lift.

3.6.3 For application of the criterion specified in 3.7 involving the sudden loss of load of the lift in which counter-ballast is used, the heeling levers are calculated using the following formulae:

$$CHL_1 = \frac{(P_L \cdot y - CBM) \cdot \cos\theta}{\Delta}$$

$$CBHL_2 = \frac{CBM \cdot \cos\theta}{(\Delta - P_L)}$$

where CBM – the heeling moment, in tm, due to the counter-ballast;

CHL_1 – combined heeling lever, in m, due to the load of the lift and the counter-ballast heeling moment at the displacement corresponding to the ship with the load of the lift;

$CBHL_2$ – heeling lever, in m, due to the counter-ballast heeling moment at the displacement corresponding to the ship without the load of the lift.

3.7 Alternative stability criteria.

3.7.1 Stability of a ship during lifting operations specified in 3.1.1 shall comply with the criteria stipulated in this Chapter. In other conditions stability shall comply with the criteria specified in Section 2 or other applicable criteria:

.1 the residual righting area below the righting lever and above the heeling lever curve between θ_e and the lesser of 40° or the angle of the maximum residual righting lever shall not be less than:

0,080 mrad, if lifting operations are performed in waters that are exposed;

0,053 mrad, if lifting operations are performed in waters that are not exposed;

.2 the equilibrium angle shall be limited to the lesser of the following:

.1 10° ;

.2 the angle of immersion of the highest continuous deck;

.3 the allowable value of trim/heel, at which the reliable operation of the crane device is ensured.

3.7.2 Stability of a ship engaged in a lifting operation shall be sufficient to withstand the sudden loss of the hook load, considering the most unfavourable, as regards stability, point at which the hook load may be applied to the ship. To ensure the sufficient stability, the area on the side of the ship opposite from the lift (Area 2) in Fig. 3.7.2 shall be greater than the residual area on the side of the lift (Area 1) in Fig. 3.7.2, by an amount given by the following:

$$\text{Area 2} - \text{Area 1} > K,$$

where $K = 0,037 \text{ mrad}$, for a lifting operation in waters that are exposed;

$K = 0 \text{ mrad}$, for a lifting operation in waters that are not exposed;

$GZ(1)$ – the righting arm curve at the displacement corresponding to the ship without hook load;

$GZ(2)$ – the righting arm curve at the displacement corresponding to the ship with hook load;

Area 2 – residual area between $GZ(1)$ and $CBHL_2$ up to the lesser of the down-flooding angle or the second intersection of $GZ(2)$ and $CBHL_2$;

Area 1 – residual area below $GZ(1)$ and above $CBHL_2$ up to the angle of the first intersection between the righting lever curve and the heeling lever curve θ_e .

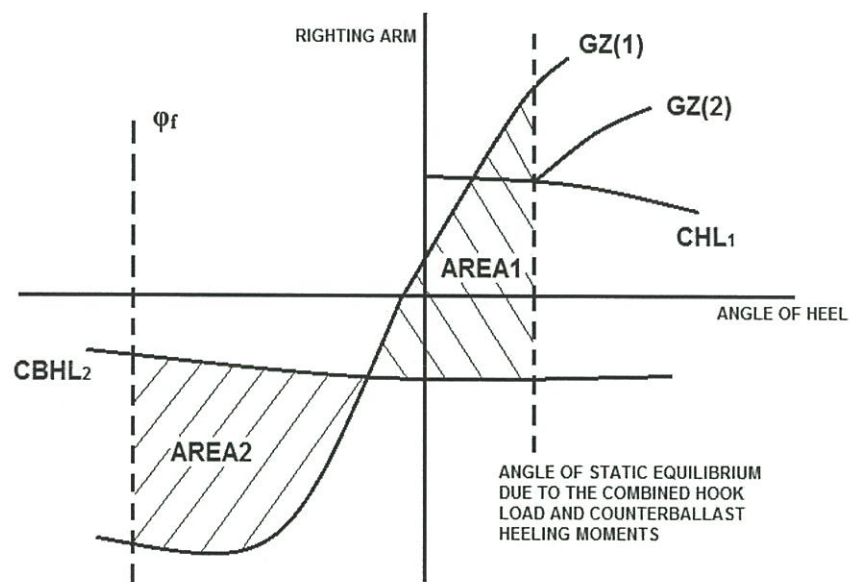


Fig. 3.7.2

3.8 Model tests or direct calculations.

3.8.1 Model tests or direct calculations, performed in accordance with a procedure approved by the Register, which determine stability of a ship sufficient to withstand

sudden loss of hook load, may be allowed as an alternative to the complying with the requirements of 3.5 and 3.7.2, provided that:

.1 the effects of wind and waves are taken into account;

.2 the maximum dynamic roll amplitude of the ship after loss of load will not cause immersion of unprotected openings.

3.9 Stability of ships engaged in lifting operations shall be checked for loading conditions reflecting the operational limitations of the ship. Use of counter ballast, if applicable, shall be considered. The ship's stability in the event of the sudden loss of the hook load shall comply with the requirements specified for such situations.

3.10 The criteria specified in 3.3 – 3.5 and 3.7, as applicable, shall be fulfilled for all loading conditions intended for lifting and with the hook load at the most unfavourable positions, as regards stability. For each loading condition, the weight and centre of gravity of the load being lifted, the cargo handling gear, and counter ballast, if any, shall be taken into account. The most unfavourable position may be chosen at the position where the total of the transverse and vertical moment is the greatest. Stability shall also be checked for loading conditions corresponding to other possible boom positions and counter ballast with different filling level.»

PART XVII. DISTINGUISHING MARKS AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

2 TECHNICAL REQUIREMENTS FOR ESCORT TUGS

A new **para 2.2.2.1.6** shall be introduced reading as follows:

“2.2.2.1.6 For the confirmation of sufficient stability of escort tugs, checking may be done in compliance with the requirements specified in Section 1 Appendix 3 to Part IV “Stability”.”



RUSSIAN MARITIME REGISTER OF SHIPPING

CIRCULAR LETTER

No. 313-08-1163c

dated 24.09.2018

Re:

amendments to the Rules for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104-E

Item(s) of supervision:

ships under construction

Implementation:
from the date of publication

Valid till:

Validity period extended till: ----

Cancels / amends / adds Circular Letter No. ----

dated ----

Number of pages: 1 + 4

Appendix(ces):

amendments to Parts VI "Fire Protection", VII "Machinery Installations", IX "Machinery", X "Boilers, Heat Exchanges and Pressure Vessels" and XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Sea-Going Ships

Director General

Konstantin G. Palnikov

We hereby inform that Parts VI "Fire Protection", VII "Machinery Installations", IX "Machinery", X "Boilers, Heat Exchanges and Pressure Vessels" and XVII "Distinguishing Marks and Descriptive Notations in the Class Notation Specifying Structural and Operational Particulars of Ships" of the Rules for the Classification and Construction of Sea-Going Ships for the Classification and Construction of Sea-Going Ships, 2018, ND No. 2-020101-104-E, shall be amended as specified in the Appendix to the Circular Letter.

Insert text here

It is necessary to do the following:

1. Apply provisions of the Circular Letter during review and approval of technical documentation on ships.
2. Bring the content of the Circular Letter to the notice of the RS surveyors and interested organizations in the area of the RS Branch Offices' activity.

List of ND amended and introduced paras/chapters/sections (to specify in the List of Circular Letters (form 8.3.36)):

Part VI: Table 3.1.2.1, paras 3.2.3.6, 3.12.1;

Part VII: paras 2.1.8, 3.3.1, 4.5.11, 4.5.13.3;

Part IX: paras 9.1.1, 9.5.1;

Part X: Chapter 1.8, para 1.8.2;

Part XVII: paras 3.5.2.2.4, 3.5.3.3.2, 3.5.3.3.3, 3.5.3.3.4, 3.5.3.3.8, 3.6.2.2.1, 3.6.3.3.2, 3.6.3.3.3, 3.6.3.3.8, 3.6.3.6.4

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"Thesis" System No. 18-251114

**RULES FOR THE CLASSIFICATION AND CONSTRUCTION OF SEA-GOING SHIPS,
2018, ND No. 2-020101-104-E**

PART VI. FIRE PROTECTION

Table 3.1.2.1. Footnote 15 shall be supplemented by the following text:

"This requirement does not apply to fishing vessels of less than 500 gross tonnage."

Para 3.2.3.6 shall be amended in the Russian version only.

Para 3.12.1 shall be supplemented by the following text:

"The provisions of this Chapter do not apply to fishing vessels."

PART VII. MACHINERY INSTALLATIONS

Para 2.1.8 shall be supplemented by a new paragraph reading as follows:

"Another speed may be set for the ships intended for navigation in geographically restricted areas while providing sufficient speed to maintain the ship's handling capability in load condition."

Para 3.3.1 shall be amended in the Russian version only.

Para 4.5.11 shall be amended to read:

"**4.5.11** In fishing vessels of more than 1000 gross tonnage one means of escape from machinery spaces of category A may be provided on the condition that it leads directly onto the open deck, the spaces are entered only periodically and the maximum travel distance to the door (hatch) leading directly onto open deck from the control stations of the equipment located in the space is 5 m or less. In cargo ships of less than 1000 gross tonnage, the Register may dispense with one of the means of escape from machinery spaces of category A, due regard being paid to the dimension and disposition of the upper part of the space. In addition, the means of escape in these ships need not comply with the requirements for an enclosure listed in paragraph 4.5.10.1."

Para 4.5.13.3 shall be amended to read:

".3 escape routes that pass only through stairways and/or corridors are considered as providing "direct access to the open deck" if outside the steering gear spaces they have continuous fire shelter equivalent to steering gear spaces or stairways and corridors, whichever is greater."

PART IX. MACHINERY

Para 9.1.1 shall be supplemented by the following text:

"The requirements of 9.2.2, 9.2.3 are applicable to engines operating on gas with a maximum working gas pressure of more than 1,0 MPa."

Para 9.5.1 shall be supplemented by the following text:

"For engines operating on gas with a maximum working gas pressure of not more than 1,0 MPa, the use of other design solutions is allowed provided that proving calculations or experimental data are provided."

PART X. BOILERS, HEAT EXCHANGERS AND PRESSURE VESSELS

Chapter 1.8 shall be renamed reading as follows:

"1.8 BOILER ROOMS".

Para 1.8.2 shall be deleted.

PART XVII. DISTINGUISHING MARKD AND DESCRIPTIVE NOTATIONS IN THE CLASS NOTATION SPECIFYING STRUCTURAL AND OPERATIONAL PARTICULARS OF SHIPS

Para 3.5.2.2.4 shall be amended to read:

"3.5.2.2.4 Where NO_x-reducing device is used, it shall be considered as the engine component. When for NO_x reduction a selective catalytic reduction (SCR) system is used, the requirements of IMO resolution MEPC.291(71) shall be complied with."

Para 3.5.3.3.2 shall be amended to read:

"3.5.3.3.2 To keep cargo spills within the cargo area, provision shall be made for a permanent continuous coaming on the cargo deck extending from side to side and from a point 0,2L forward of amidships to the aft end of the cargo deck with height dimensions given in Table 3.5.3.3.2."

Table 3.5.3.3.2. The column heading "Minimum heights of continuous coaming" shall be replaced by:

"Height dimensions of continuous coamings";

in the last column the values of aft ends of cargo deck for ships of 100000 t deadweight and above shall be replaced by "0,30 m".

Para 3.5.3.3.3 shall be amended to read:

"3.5.3.3.3 To collect possible oil spills during cargo operations the main deck in the cargo area shall be fitted with a system for collection of the spilled cargo with its accumulation in a holding tank or a slop tank.

Collection of the spilled cargo may be performed using particular pump and pipes located in the cargo area or by gravity drainage through specially provided pipes. The system shall be provided with means for removal of cargo residues from the pipes, when the collection of the spilled cargo is over.

Automatic gravity drainage shall be used during cargo operations where cargo spills may occur, and shall not be used under normal conditions when at sea. For gravity drainage, each pipe of deck system shall be arranged with a manually operated valve opened only during cargo operations and an automatic scupper."

Para 3.5.3.3.4 shall be amended to read:

"3.5.3.3.4 On oil tankers, chemical tankers and NLS tankers, the points where cargo hoses are connected to cargo manifolds shall be fitted with pipes for drainage of leaks to a holding tank or a slop tank.

The trays shall have the following minimum dimension:

tray length shall be so that the cargo manifold doesn't extend beyond forward and aft ends of the tray;

width — at least 1,8 m, at that the spill tray extends at least 1,2 m outboard of the end of the manifold flange;

minimum depth — 0,3 m".

Para 3.5.3.3.8. In the first paragraph the word "pipes" shall be replaced by the word "manifolds";

the second paragraph shall be introduced reading as follows:

"These requirements shall not be applied to locations of receiving fuel and lubricating oil manifolds provided on general location area together with cargo manifolds, the locations of which shall be fitted with trays according to 3.5.3.3.4."

Para 3.6.2.2.1 shall be amended to read:

"Compliance with the requirements shall be confirmed in accordance with 3.5.2.2.1 — 3.5.2.2.5 and 3.5.2.2.9 — 3.5.2.2.10."

Paras 3.6.2.2.1 — 3.6.2.2.4 shall be deleted.

Para 3.6.3.3.2. The words "deck scupper" shall be deleted.

Para 3.6.3.3.3 shall be amended to read:

"3.6.3.3.3 On oil tankers, chemical tankers and NLS tankers where cargo hoses are connected to cargo manifolds, the provision shall be made for spill trays with dimensions and pipes according to 3.5.3.3.4."

Para 3.6.3.3.8 shall be amended to read:

"In addition to the requirements specified in 3.5.3.3.8, locations on the open deck in the areas of receiving fuel and lubricating oil manifolds shall be fitted with a system for collection of the spilled cargo with its accumulation in a holding tank or a slop tank.

Collection of the spilled cargo may be performed using particular pump and pipes located in the areas of receiving fuel and lubricating oil manifolds or by gravity drainage through specially provided pipes. Automatic gravity drainage shall be used during bunkering operation where fuel and oil spills may occur. For gravity drainage, each pipe of deck system shall be arranged with a manually operated valve opened only during bunkering operation and an automatic scupper."

Para 3.6.3.6.4. The second sentence shall be amended to read:

"When the ship is operated in special areas defined in compliance with the amendments to Annex IV to MARPOL 73/78 in IMO resolution MEPC.200(62), the above plant shall have a Certificate of type approval for sewage treatment plants in compliance with IMO resolution MEPC.227(64), including provisions specified in 4.2 of the resolution."

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Часть XVII
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определяющие конструктивные
или эксплуатационные особенности судна

Russian Maritime Register of Shipping
Rules for the Classification and Construction of Sea-Going Ships
Part XVII
Distinguishing Marks and Descriptive Notations
in the Class Notation Specifying Structural and Operational Particulars of Ships

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